



Global Companies LLC., 800 South Street, P.O. Box 9161, Waltham, MA 02454-9161 ph: 781-894-8800

May 9, 2022

Via E-Mail Delivery (Christopher.Lang@dec.ny.gov)

Chris Lang, Environmental Analyst
New York State Department of
Environmental Conservation
Division of Environmental Permits, Region 3
21 South Putt Corners Road
New Paltz, NY 12561-1620

RE: Climate Leadership and Community Protection Act (CLCPA) Analysis
Global Companies LLC, Cargo Terminal
Air Title V Permit Application
DEC Application ID 3-3348-00082/00010
Town of New Windsor, Orange County

Dear Mr. Lang:

Global Companies LLC (Global or Applicant) is submitting this letter to document the analysis of the above-referenced application in regards to the requirements and goals of the 2019 Climate Leadership and Community Protection Act (CLCPA). This analysis incorporates submittals sent to NYSDEC on April 14, 2021, March 10, 2022, April 6, 2022, and April 14, 2022.

On August 28, 2020, Global submitted an application for renewal and modification of its Cargo Terminal Title V permit. The application included provisions to modify the allowable throughputs of gasoline and distillate products while maintaining the same overall facility throughput and to install a new Vapor Recovery Unit (VRU) to treat vapors from the existing truck loading rack.

Global is asking to increase the throughput cap at Cargo to create redundancy with the Newburgh Terminal and operational flexibility across the Terminals. The increase in throughput at Cargo does not change the market demand for gasoline in the Newburgh area, and there is not expected to be a net increase in gasoline throughput across all of the Global Newburgh Terminals. Because loading can be done more efficiently at Cargo, Global plans to divert loading from Newburgh to Cargo. The increase in the Cargo cap allows Global the flexibility to make this change, as the Cargo Terminal is currently operating close to its throughput cap. Although the Newburgh Terminal has a higher gasoline throughput, it often has a bottleneck due to loading inefficiencies associated with the layout of the Terminal. In addition, traffic can build up from the Newburgh Terminal onto River Road and often needs to be diverted to Cargo, which has more room for trucks. After the improvements proposed at Cargo—most notably, installation of the VRU—loading emissions at the Terminal will decrease, benefitting the community. Moreover, the VRU will emit no GHGs. By increasing the cap at Cargo, the Terminals will have similar limits

and Global will have the flexibility to switch demand between the two Terminals. In addition, if one of the Terminals is shut down for any period of time, Global will still be able to meet the market demand in the area by using the other Terminal.

As further detailed in this letter, Global believes that the modification (or Project) is consistent with the CLCPA as it will result in a reduction in allowable facility greenhouse gas (GHG) emissions from 3255.6 to 418.1 tpy CO₂e¹, an 87 percent decrease. This is accomplished largely by replacing the existing flares at the facility with the VRU which captures and recycles the vapors rather than combusting them.

Details of the pre and post project GHG emissions, pre and post project combustion and non-combustion HAP emissions, and the upstream GHG analysis are included in the following sections. The calculations include emissions from on site emissions.

Allowable GHG Emissions Before and After the Project

To determine the GHG emission impacts of the Project, Global has quantified allowable GHG emissions both in actual terms and on a CO₂e basis before and after the Project. These emissions include GHG emissions associated with day-to-day operation of the Terminal, in particular, CO₂ and other GHG emissions associated with existing on-site fuel handling and related operations.

The regulations recently adopted by DEC setting statewide GHG emission limits under the CLCPA contain a list of pollutants regulated by New York State as GHGs and assigns each GHG a CO₂ equivalent. *See* 6 NYCRR § 496.5. The Facility emits only CO₂, methane, and nitrous oxide from the State's list of GHGs. Accordingly, these are the only GHGs addressed in the analysis.

Total GHG emissions from the Terminal are relatively low. These emissions originate almost exclusively from two sources—operation of the Terminal's existing open flares, which are used to control emissions of VOCs associated with the Terminal's gasoline loading activities and—to a much lesser extent—miscellaneous exempt combustion equipment (e.g., emergency gas-fired generators and a boiler used to heat the building). Going forward, the Project calls for replacing the existing flares with a VRU permitted at 2 mg/l (except for limited circumstances where the flares will be used as a backup with an allowable gasoline throughput limit of 5,000,000 gallons per year at 80 mg/L without the operation of the vac assist system). There will also be a change to the product throughput subcaps at the truck loading rack. While the overall Terminal throughput will not increase, allowable gasoline throughput will increase from 236 to 550 million gallons and the allowable distillate loading will decrease from 1.419 to 1.1 billion gallons.

The allowable emissions before and after the Project are set forth below. All emissions are measured in tons per year. Information about how the emissions below were calculated can be found in Attachment A, which includes the Potential to Emit (PTE) for the Terminal's combustion sources.

¹ tpy CO₂e = tons per year carbon dioxide equivalent

Current Potential Emissions (based on allowable throughputs):

CO₂: 3,225.55 tpy
Methane: 0.07 tpy
Nitrous Oxide: 0.01 tpy
Total CO₂e: 3,234.01 tpy

Future Potential Emissions (based on proposed allowable throughputs):

CO₂: 415.99 tpy
Methane: 0.01 tpy
Nitrous Oxide: 0.003 tpy
Total CO₂e: 418.13 tpy

As set forth above and in Attachment A, the Project will reduce allowable GHG emissions by approximately 2,815.88 tpy relative to current allowable emissions, an 87 percent decrease.

Combustion HAP Emissions Before and After the Project

As outlined in the attached combustion potential to emit (PTE) (Attachment A), hazardous air pollutant (HAP) emissions associated with combustion sources and generators are as follows:

Pollutant	lb/yr	ton/yr
Benzene	6.11E-03	3.06E-06
Ethylbenzene	1.82E-03	9.08E-07
Toluene	1.77E-01	8.85E-05
Xylenes	3.11E-03	1.56E-06
Formaldehyde	9.42E-01	4.71E-04
Naphthalene	3.23E-02	1.61E-05
Total HAPs	1.16E+00	5.81E-04

Emission factors used to calculate the HAPs associated with combustion sources are from AP-42 Table 1.3-9. The sources contributing to these HAP emissions, as outlined in the attached PTE, are two diesel generators and a distillate furnace. There are no changes to the operations of these sources as a result of the project and, therefore, the combustion HAP emissions before and after the project will not change.

Non-combustion HAP Emissions Before and After the Project

Non-combustion HAP emissions before and after the project are summarized in the following table, with detailed calculations provided in the PTE in Attachment B and the previously submitted PTE for the project. Calculations before the project assumed annual throughputs of 236,000,000 gallons of gasoline and 1,419,100,000 gallons of distillate. The proposed project includes an increase to the annual gasoline throughput to 550,000,000 gallons and a decrease in annual distillate throughput to 1,100,000,000 gallons. However, a Vapor Recovery Unit (VRU) will be installed, which will operate at 2 mg/l with a vacuum assist system to capture fugitive emissions and significantly lower emissions. The throughput to the flares, which operate at an emission limit of 80 mg/l without vacuum assist, would be limited to 5,000,000 gallons per year.

Therefore, as is illustrated in the table below, overall HAP emissions at the facility will decrease as a result of the project. Air dispersion modeling efforts for the facility are ongoing. A protocol has been submitted and modeling will be completed in accordance with the approved protocol and submitted to NYSDEC.

Pollutant	Total PTE (TPY), Before Project	Total PTE (TPY), After Project
Total HAP	4.23	2.39
hexane	0.60	0.26
benzene	0.69	0.31
2,2,4 TMP	0.76	0.34
toluene	1.04	0.59
ethylbenzene	0.12	0.10
xylenes	1.01	0.78
naphthalene	6.63E-03	6.83E-03
cumene	5.85E-03	1.83E-03

Upstream GHG Analysis

An analysis of the impact of the proposed project on upstream GHG emissions was conducted. The proposed modification would decrease upstream GHG emissions associated with combustion at the terminal, due to the decreased propane usage to operate the flares. The upstream calculations associated with current and proposed propane usage are provided as Attachment C and are summarized below. Emission factors are from “Appendix A Emission Factors for Use by State Agencies and Applicants” provided by NYSDEC.

Current Potential Upstream Emissions (based on current maximum allowable throughput to estimate propane usage for flare):

CO₂: 30.49 tpy
Methane: 0.213 tpy
Nitrous Oxide: 0.0005 tpy
Total CO₂e: 48.535 tpy

Future Potential Upstream Emissions (based on proposed maximum allowable throughput to estimate propane usage for flare):

CO₂: 0.867 tpy
Methane: 0.006 tpy
Nitrous Oxide: 0.00001 tpy
Total CO₂e: 1.381 tpy

As previously noted, operation of the other small combustion sources at the terminal will not change as a result of the project. Accordingly, as set forth above and in Attachment C, the

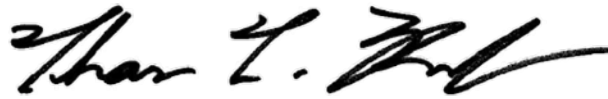
project will reduce upstream GHG emissions by approximately 47.154 tpy relative to current upstream calculations, a 97 percent decrease.

Conclusion

Based on the reduction in GHGs presented above the Project is consistent with the goals of the CLCPA. If there are any questions or concerns regarding the CLCPA consistency analysis, please contact me via e mail at tkeefe@globalp.com.

Many thanks for your attention to this matter. I look forward to hearing from you.

Very truly yours,

A handwritten signature in black ink, appearing to read "Tom Keefe", with a stylized flourish at the end.

Tom Keefe
Vice President, EHS

Attachment A

Potential To Emit for Combustion Sources

Fuel Consumption

Exempt Combustion Sources:

Product	Unit	Gal/yr (Liquid)	SCF/yr (Gas)	Year (Gas)	MMBTU/yr*
Distillate	Furnace	2,155			297
Propane	Flares	17,575			1,599

* MMBTU/yr based on default high heat values from 40 CFR 98 Subpart C Table C-1.

Distillate Combustion Emissions:

Pollutant	Combustion Emissions									
	PM 2.5	PM 10	SOx	NOx	VOC	CO	CH4	N2O	CO2	GHG**
Emission Factor *	2.00	2.00	0.21	20.00	0.20	5.00	0.01	0.0013	163.05	(CH4*84)+(N2O*264)+(CO2*1)
lb/yr	4.31	4.31	0.46	43.10	0.43	10.78	1.97	0.39	48490.10	48,759.17
tons/yr	0.002	0.002	0.00	0.02	0.0002	0.005	0.001	0.000	24.245	24.380

* PM, NOx, CO, VOC, and SOx Emission factors used to estimate emissions are from AP-42, Compilation of Air Pollutant Emission Factors, Fifth Edition, Volume I and are in units of lb/1000 gallons. SOx, NOx, CO, and PM

Emission Factors are from Table 1.3-1. VOC Emission Factors are from Table 1.3-3. CO2 emission factor is from 40 CFR 98 Subpart C Table C-1 for Distillate Fuel Oil 2, converted to lb/MMBTU. CH4 and N2O

** GHG Emission calculated by using the CO2 Equivalency Factor for CO2 (1), CH4 (84) and N2O (264).

Example calculation (using SOx):

= gal/yr / 1000 gal * emission factor
 = 2155 gal/yr / 1000 gal * 0.21 lb/1000 gal (SOx)
 = 0.46 lb/yr

Propane Combustion Emissions

Propane Vapor Service

Pollutant	Combustion Emissions									
	PM2.5	PM10	SOx	NOx	VOC	CO	CH4	N2O	CO2	GHG**
Emission Factor *	0.7	0.7	0.00015	13	NA	7.5	0.01	0.0013	139	(CH4*84)+(N2O*264)+(CO2*1)
lb/yr	12.303	12.303	0.003	228.475	NA	131.813	10.578	2.116	221,671.566	223,118.58
tons/yr	0.006	0.006	0.000	0.114	NA	0.066	0.005	0.001	110.836	111.559

* Emission factors used to estimate emissions for PM, SOx, NOx, VOC and CO are from AP-42, Compilation of Air Pollutant Emission Factors, Fifth Edition, Volume 1 Table 1.5-1, in units of lb/1000 gallons. CO2 emission factor is from 40 CFR 98 Subpart C Table C-1 for Propane, converted to lb/MMBTU. CH4 and N2O emission factors are from 40 CFR 98 Subpart C Table C-2 for Petroleum Products, converted to

** GHG Emission calculated by using the CO2 Equivalency Factor for CO2 (1), CH4 (84) and N2O (264).

Vapor Combustion Emissions from Flare Loading

Based on Flare Loading before throughput modification 236000000 gal/yr

(Emissions from Combustion of Petroleum Product Loaded)

Petroleum Vapor Combusted (lbs), based on loading to flare

2,247,394 Total
 2,247,394 Uncontrolled VOC emissions at 1-RACK1, Emission Point U0001 (Truck Loading Rack Flares)

Uncontrolled VOC emissions = Annual loading volume (1000 gallons) * Loading Emission factor (lbs/1000 gallons)

Emission factor = 12.46 SPM/T = 9.52 lb/1000 gallons

S = 1.00 (dimensionless)

Vapor Pressure = 5.93 psia (average over year for gasoline)

Molecular weight = 66.00 lb/lbmol

Temperature = 512.24 degrees R, same as used for loading, average for year

Conversion from Petroleum Vapor Combusted in lbs to MMSCF (as Natural Gas Equivalent):

MMSCF (as Natural Gas) = Petroleum Vapor Combusted (lbs) * (21,000 BTUs / lb gasoline (high avg. for C4-C8 gases) / (1,000,000 BTUs/SCF)) / (1,000,000)

MMSCF (as Natural Gas) combusted at U0001 = 47.195

MMBTU for Flare Combustion = (21,000 BTUs / lb gasoline (high avg. for C4-C8 gases))/1,000,000 = 47195.27931

Truck Rack Flare Emissions from Gasoline Loading (Emission Unit U0001)

Pollutant	Combustion Emissions									
	PM2.5	PM10	SOx	NOx	VOC*	CO	CH4	N2O	CO2	GHG**
Emission Factor**	274	274	0.60	0.068	NA	0.31	0.002	0.0002	117	(CH4*84)+(N2O*264)+(CO2*1)
lb/yr	0.04	0.04	28.32	3,209.28	NA	14,630.54	104.05	10.40	5,520,718.58	5,532,205.34
tons/yr	0.00	0.00	0.01	1.60	NA	7.32	0.052	0.005	2760.359	2766.10

*These emissions are from gasoline vapor combustion and pilot light gas. Gasoline VOCs are already accounted for in the VCU emissions.

** NOx emissions factor is from Table 13.5-1, in units of lb/MMBTU. CO emission factor is from Table 13.5-2 in units of lb/MMBTU. The PM emission factors were conservatively assumed based on values for soot in Table 13.5-1, in units of ug/l. The SOx emission factor is from AP-42 Table 1.4-2, in units of lb/MMSCF. CH4 and N2O emission factors are from 40 CFR 98 Subpart C Table C-2 converted to units of lb/MMBTU. CO2 emission factor is from 40 CFR 98 Subpart C Table C-1 converted to units of lb/MMBTU.

Total of Combustion Sources

Pollutant	PM 2.5	PM 10	SOx	NOx	VOC	CO	CH4	N2O	CO2	GHG**
lb/yr	16.65	16.65	28.78	3,480.85	0.43	14,773.12	116.59	12.91	5,790,880.24	5,804,083.09
tons/yr	0.01	0.01	0.01	1.74	0.00	7.39	0.06	0.006	2,895.44	2,902.04

HAP Speciation from Fuel Oil Combustion Sources

Pollutant	Emission Factor (lb/1000 gallons)	lb/yr	ton/yr
Benzene	2.14E-04	4.61E-04	2.31E-07
Ethylbenzene	6.36E-05	0.000137058	6.85E-08
Toluene	6.20E-03	0.013361	6.68E-06
Xylenes	1.09E-04	0.000234895	1.17E-07
Formaldehyde	3.30E-02	0.071115	3.56E-05
Naphthalene	1.13E-03	0.00243515	1.22E-06

Emission Factors for HAPs are from AP-42 Table 1.3-9

Combustion Calculations

Fuel Consumption

Exempt Combustion Sources:

Product	Unit	Gal/yr (Liquid)	SCF/yr (Gas)	lb/year (Gas)	MMBTU/yr*
Distillate	Furnace	2,155			297
Propane	Flares	500			46

* MMBTU/yr based on default high heat values from 40 CFR 98 Subpart C Table C-1.

Distillate Combustion Emissions:

Pollutant	Combustion Emissions									
	PM 2.5	PM 10	SOx	NOx	VOC	CO	CH4	N2O	CO2	GHG**
Emission Factor *	2.00	2.00	0.21	20.00	0.20	5.00	0.01	0.0013	163.05	4*84)+(N2O*264)+(CO2*1)
lb/yr	4.31	4.31	0.46	43.10	0.43	10.78	1.97	0.39	48490.10	48,759.17
tons/yr	0.002	0.002	0.00	0.02	0.0002	0.005	0.001	0.000	24.245	24.380

* PM, NOx, CO, VOC, and SOx Emission factors used to estimate emissions are from AP-42, Compilation of Air Pollutant Emission Factors, Fifth Edition, Volume I and are in units of lb/1000 gallons. SOx, NOx, CO, and PM Emission Factors are from Table 1.3-1. VOC Emission Factors are from Table 1.3-3. CO2 emission factor is from 40 CFR 98 Subpart C Table C-1 for Distillate Fuel Oil 2, converted to lb/MMBTU. CH4 and N2O emission factors are from 40 CFR 98 Subpart C Table C-2 for Petroleum Products, converted to lb/MMBTU.

** GHG Emission calculated by using the CO2 Equivalency Factor for CO2 (1), CH4 (84) and N2O (264).

Example calculation (using SOx):
 = gal/yr / 1000 gal * emission factor
 = 2155 gal/yr / 1000 gal * 0.21 lb/1000 gal (SOx)
 = 0.46 lb/yr

Propane Combustion Emissions

Propane Vapor Service

Pollutant	PM2.5	PM10	SOx	NOx	VOC	CO	CH4	N2O	CO2	GHG**
	Emission Factor *	0.7	0.7	0.00015	13	NA	7.5	0.01	0.0013	138.60
lb/yr	0.350	0.350	0.000	6.500	NA	3.750	0.301	0.060	6,306.446	6,347.61
tons/yr	0.000	0.000	0.000	0.003	NA	0.002	0.000	0.000	3.153	3.174

* Emission factors used to estimate emissions for PM, SOx, NOx, VOC and CO are from AP-42, Compilation of Air Pollutant Emission Factors, Fifth Edition, Volume 1 Table 1.5-1, in units of lb/1000 gallons. CO2 emission factor is from 40 CFR 98 Subpart C Table C-1 for Propane, converted to lb/MMBTU. CH4 and N2O emission factors are from 40 CFR 98 Subpart C Table C-2 for Petroleum

** GHG Emission calculated by using the CO2 Equivalency Factor for CO2 (1), CH4 (84) and N2O (264).

Vapor Combustion Emissions from Flare Loading

Based on Flare Loading after throughput modification 5000000 gal/yr

(Emissions from Combustion of Petroleum Product Loaded)

Petroleum Vapor Combusted (lbs), based on loading to flare

47,614 Total
 47,614 Uncontrolled VOC emissions at 1-RACK1, Emission Point U0001 (Truck Loading Rack Flares)

Uncontrolled VOC emissions = Annual loading volume (1000 gallons) * Loading Emission factor (lbs/1000 gallons)

Emission factor = 12.46 SPM/T = 9.52 lb/1000 gallons

S = 1.00 (dimensionless)

Vapor Pressure = 5.93 psia (average over year for gasoline)

Molecular weight = 66.00 lb/lbmol

Temperature = 512.24 degrees R, same as used for loading, average for year

Conversion from Petroleum Vapor Combusted in lbs to MMSCF (as Natural Gas Equivalent):

MMSCF (as Natural Gas) = Petroleum Vapor Combusted (lbs) * (21,000 BTUs / lb gasoline (high avg. for C4-C8 gases) / (1,000 BTU/SCF) / (1,000,000)

MMSCF (as Natural Gas) combusted at U0001 = 1.000

MMBTU for Flare Combustion = (21,000 BTUs / lb gasoline (high avg. for C4-C8 gases))/1,000,000 = 999.8999854

Truck Rack Flare Emissions from Gasoline Loading (Emission Unit U0001)

Pollutant	Combustion Emissions									
	PM2.5	PM10	SOx	NOx	VOC*	CO	CH4	N2O	CO2	GHG**
Emission Factor**	274	274	0.60	0.068	NA	0.31	0.002	0.0002	117	4*84)+(N2O*264)+(CO2*1)
lb/yr	0.00	0.00	0.60	67.99	NA	309.97	2.204	0.2204	116,964.38	117,207.74
tons/yr	0.00	0.00	0.00	0.03	NA	0.15	0.001	0.000	58.482	58.60

*These emissions are from gasoline vapor combustion and pilot light gas. Gasoline VOCs are already accounted for in the VCU emissions.

** NOx emissions factor is from Table 13.5-1, in units of lb/MMBTU. CO emission factor is from Table 13.5-2 in units of lb/MMBTU. The PM emission factors were conservatively assumed based on values for soot in Table 13.5-1, in units of ug/l. The SOx emission factor is from AP-42 Table 1.4-2, in units of lb/MMSCF. CH4 and N2O emission factors are from 40 CFR 98 Subpart C Table C-2 converted to units of lb/MMBTU. CO2 emission factor is from 40 CFR 98 Subpart C Table C-1 converted to units of lb/MMBTU.

Total of Combustion Sources

Pollutant	PM 2.5	PM 10	SOx	NOx	VOC	CO	CH4	N2O	CO2	GHG**
lb/yr	4.66	4.66	1.06	117.59	0.43	324.49	4.47	0.67	171,760.92	172,314.52
tons/yr	0.00	0.00	0.00	0.06	0.00	0.16	0.002	0.0003	85.88	86.16

HAP Speciation from Fuel Oil Combustion Sources

Pollutant	Emission Factor (lb/1000 gallons)	lb/yr	ton/yr
Benzene	2.14E-04	4.61E-04	2.31E-07
Ethylbenzene	6.36E-05	0.000137058	6.85E-08
Toluene	6.20E-03	0.013361	6.68E-06
Xylenes	1.09E-04	0.000234895	1.17E-07
Formaldehyde	3.30E-02	0.071115	3.56E-05
Naphthalene	1.13E-03	0.00243515	1.22E-06
Total HAPs		8.77E-02	4.39E-05

Emission Factors for HAPs are from AP-42 Table 1.3-9

Emergency Generators (Exempt)

Emergency Generator Sources:

Fuel Type	Source	Gal/hr (Liquid)	SCF/hr (Gas)	Gal/hr (Gas)	MMBTU/hr*
Diesel	North Generator - 400 kW	21.3			2.94
Diesel	South Generator - 600 kW	31.5			4.35
Propane	100 kW				0.96

* MMBTU/hr for diesel generators calculated based on high heat value in 40 CFR 98 Subpart C Table C-1. MMBTU/hr for propane generator is based on the spec sheet from the manufacturer.

Distillate Fired Engine Emissions:

Pollutant	PM2.5	PM10	SOx	NOx	VOC	CO	CH4	N2O	CO2	GHG**
Emission Factor *	2.00	2.00	0.21	20.00	0.20	5.00	0.01	0.001	163.05	CH4*84)+(N2O*264)+(CO2*1)
lb/yr	52.80	52.80	5.62	528.00	5.28	132.00	24.10	4.82	594,031.83	597,328.08
tons/yr	0.03	0.03	0.00	0.26	0.00	0.07	0.01	0.00	297.02	298.66

* PM, SOx, NOx, VOC and CO Emission factors used to estimate emissions are from AP-42, Compilation of Air Pollutant Emission Factors, Fifth Edition, Volume I in units of lb/1000 gallon. SOx, NOx, CO, and PM Emission Factors are from Table 1.3-1. VOC Emission Factor is from Table 1.3-3. CO2 emission factor is from 40 CFR 98 Subpart C Table C-1 for Distillate Fuel Oil 2, converted to lb/MMBTU. CH4 and N2O emission factors are from 40 CFR 98 Subpart C Table C-2 for Petroleum Products, converted to lb/MMBTU.

** GHG Emission calculated by using the CO2 Equivalency Factors for CH4 (84), N2O (264) and CO2 (1).

Example calculation:

= gal/yr / 1000 gal * emission factor

Natural Gas & Propane Fired Engine Emissions:

Pollutant	PM2.5	PM10	SOx	NOx	VOC	CO	CH4	N2O	CO2	GHG**
Emission Factor* - lb/MMBtu	0.0099	0.0099	0.0006	2.270	0.0296	3.720	0.007	0.0013	138.603	CH4*84)+(N2O*264)+(CO2*1)
lb/yr	4.73	4.73	0.28	1,083.93	14.13	1,776.30	3.16	0.63	66,183.03	66,615.06
tons/yr	0.00	0.00	0.00	0.54	0.01	0.89	0.00	0.00	33.09	33.31

* PM, SOx, NOx, VOC and CO Emission factors used to estimate emissions are from AP-42 Table 3.2-3. CO2 emission factor is from 40 CFR 98 Subpart C Table C-1 for Propane. CH4 and N2O emission factors are from 40 CFR 98 Subpart C Table C-2 for Petroleum Products.

** GHG Emission calculated by using the CO2 Equivalency Factors for CH4 (84), N2O (264) and CO2 (1).

MMBTU/yr Calculation = 0.96 MM BTU/hr * 500 hrs = 478 MMBTU/yr Assumes 500 hours/yr

Total of Generator Sources

Pollutant	PM2.5	PM10	SOx	NOx	VOC	CO	CH4	N2O	CO2	GHG
lb/yr	57.53	57.53	5.90	1,611.93	19.41	1,908.30	27.25	5.45	660,214.86	663,943.14
tons/yr	0.03	0.03	0.00	0.81	0.01	0.95	0.01	0.003	330.11	331.97

HAP Speciation from Diesel Generators

Pollutant	Emission Factor (lb/1000 gallons)	lb/yr	ton/yr
Benzene	2.14E-04	5.65E-03	2.82E-06
Ethylbenzene	6.36E-05	0.00167904	8.40E-07
Toluene	6.20E-03	0.16368	8.18E-05
Xylenes	1.09E-04	0.0028776	1.44E-06
Formaldehyde	3.30E-02	0.8712	4.36E-04
Naphthalene	1.13E-03	0.029832	1.49E-05
Total HAPs		1.07E+00	5.37E-04

Emission Factors for HAPs are from AP-42 Table 1.3-9. Calculations are based on 500 hours/yr of operation.

Attachment B
Pre-Project Potential To Emit

Total Facility PTE Pre-Project Summary

Pollutant	Tank Emissions (TPY)	Loading Emissions (TPY)	Equipment Fugitive Emissions (TPY)	Total (TPY)
VOC	45.74	94.91	0.27	140.92
Total HAP	1.64	2.57	0.03	4.23
hexane	0.22	0.37	0.001	0.60
benzene	0.26	0.43	0.002	0.69
2,2,4 TMP	0.29	0.46	0.005	0.76
toluene	0.38	0.64	0.009	1.04
ethylbenzene	0.07	0.05	0.002	0.12
xylene	0.41	0.60	0.009	1.01
naphthalene	0.003	0.00	0.001	6.63E-03
cumene	0.001	0.00	0.001	5.85E-03

* = includes VOCs from Combustion and Emergency Generators

Total Emissions from Combustion Sources and Emergency Generators

Pollutant	Combustion Sources (TPY)	Generators (TPY)	Total (TPY)
PM 2.5	0.00	0.03	0.03
PM 10	0.00	0.03	0.03
SOx	0.01	0.00	0.02
NOx	1.63	0.81	2.44
VOC	0.00	0.01	0.01
CO	7.32	0.95	8.28
CH4	0.05	0.01	0.07
N2O	0.01	0.00	0.01
CO2	2787.76	330.11	3117.86
GHG	2,793.66	331.97	3125.63

SUMMARY OF TANK HAP EMISSIONS									
Tank ID	Total HAPS	hexane	benzene	2,2,4 TMP	toluene	ethylbenzene	xylenes	naphthalene	cumene
	lb/yr	lb/yr	lb/yr	lb/yr	lb/yr	lb/yr	lb/yr	lb/yr	lb/yr
ROUTINE EMISSIONS									
IFR Tanks									
17414	269.59	51.27	57.07	66.10	66.74	4.92	22.13	0.34	1.02
30531	63.84	10.87	12.35	15.03	16.28	1.53	7.15	0.22	0.40
30532	77.80	12.84	14.69	18.11	20.00	1.98	9.32	0.32	0.53
30534	290.82	53.93	60.31	70.63	72.51	5.71	25.93	0.52	1.26
30533	63.02	11.14	12.57	15.04	15.92	1.39	6.44	0.17	0.34
30535	290.53	53.92	60.29	70.58	72.43	5.69	25.85	0.51	1.26
SubTotal	1055.59	193.98	217.30	255.50	263.89	21.23	96.82	2.08	4.80
VFR Tanks									
17413	491.82	2.35	14.38	0.00	130.62	16.73	325.43	2.32	0.00
17415	174.39	0.83	5.10	0.00	46.31	5.93	115.39	0.82	0.00
SubTotal	666.22	3.18	19.48	0.00	176.93	22.67	440.82	3.14	0.00
Horizontal Tanks									
10454A	33.12	0.00	0.00	0.00	0.00	9.65	23.46	0.00	0.00
10455A	33.12	0.00	0.00	0.00	0.00	9.65	23.46	0.00	0.00
13061A	33.12	0.00	0.00	0.00	0.00	9.65	23.46	0.00	0.00
13316A	33.12	0.00	0.00	0.00	0.00	9.65	23.46	0.00	0.00
10456	0.01	0.00	0.00	0.00	0.00	0.00	0.01	0.00	0.00
10457	32.99	0.00	0.00	0.00	0.00	9.62	23.37	0.00	0.00
10458	32.97	0.00	0.00	0.00	0.00	9.61	23.36	0.00	0.00
10459B	1.25	0.00	0.00	0.00	0.00	0.37	0.89	0.00	0.00
10460	0.01	0.00	0.00	0.00	0.00	0.00	0.01	0.00	0.00
10470	33.39	0.00	0.00	0.00	0.00	9.71	23.67	0.00	0.00
10480	19.31	0.00	0.00	0.00	0.00	5.62	13.69	0.00	0.00
SubTotal	252.40	0.00	0.00	0.00	0.01	73.53	178.85	0.00	0.00
TOTAL ROUTINE	1974.21	197.16	236.78	255.50	440.82	117.43	716.49	5.22	4.80
LANDING PTE EMISSIONS (LB/YR) ^{1/}									
Tank ID	Total HAPS	hexane	benzene	2,2,4 TMP	toluene	ethylbenzene	xylenes	naphthalene	cumene
IFR Tanks									
17414	266.86	50.91	57.68	66.44	67.01	4.47	19.55	0.04	0.77
30531	95.52	18.22	20.65	23.78	23.98	1.60	7.00	0.01	0.28
30532	194.95	37.19	42.14	48.54	48.95	3.26	14.28	0.03	0.56
30534	350.05	66.78	75.66	87.15	87.89	5.86	25.64	0.05	1.01
30533	48.74	9.30	10.53	12.13	12.24	0.82	3.57	0.01	0.14
30535	350.05	66.78	75.66	87.15	87.89	5.86	25.64	0.05	1.01
SubTotal	1306.17	249.19	282.33	325.20	327.96	21.86	95.68	0.18	3.76
TOTAL TANK PTE									
Total HAPS	hexane	benzene	2,2,4 TMP	toluene	ethylbenzene	xylenes	naphthalene	cumene	
Total (lb/yr)	3,280	446	519	581	769	139	812	5	9
Total (tpy)	1.64	0.22	0.26	0.29	0.38	0.07	0.41	0.00	0.00
Total (lb/hr)	0.37	0.05	0.06	0.07	0.09	0.02	0.09	0.00	0.00

SUMMARY OF PTE ROUTINE TANK EMISSIONS

SUMMARY OF VOC EMISSIONS				SUMMARY PER MONTH											
Tank ID				January	February	March	April	May	June	July	August	September	October	November	December
ROUTINE	lb/yr	tpy	lb/hr	lb/month	lb/month	lb/month	lb/month	lb/month	lb/month	lb/month	lb/month	lb/month	lb/month	lb/month	lb/month
IFR Tanks															
17414															
<i>Total</i>	11,595	5.80	1.32	677.96	714.60	853.66	984.77	775.47	986.47	1,123.20	1,095.26	1,523.78	1,111.10	983.70	765.24
<i>Standing</i>	11,521	5.76	1.32	671.77	708.41	847.46	978.58	769.28	980.27	1,117.01	1,089.07	1,517.59	1,104.91	977.51	759.05
<i>Working</i>	74	0.04	0.01	6.19	6.19	6.19	6.19	6.19	6.19	6.19	6.19	6.19	6.19	6.19	6.19
30531															
<i>Total</i>	2,411	1.21	0.28	141.88	149.37	177.83	204.67	161.83	205.02	233.00	227.28	314.98	230.52	204.45	159.74
<i>Standing</i>	2,358	1.18	0.27	137.49	144.98	173.44	200.28	157.44	200.63	228.61	222.89	310.59	226.13	200.06	155.35
<i>Working</i>	53	0.03	0.01	4.39	4.39	4.39	4.39	4.39	4.39	4.39	4.39	4.39	4.39	4.39	4.39
30532															
<i>Total</i>	2,831	1.42	0.32	166.96	175.73	208.99	240.35	190.29	240.76	273.46	266.78	369.28	270.57	240.09	187.84
<i>Standing</i>	2,756	1.38	0.31	160.68	169.45	202.71	234.07	184.01	234.47	267.18	260.50	363.00	264.29	233.81	181.56
<i>Working</i>	75	0.04	0.01	6.28	6.28	6.28	6.28	6.28	6.28	6.28	6.28	6.28	6.28	6.28	6.28
30534															
<i>Total</i>	12,147	6.07	1.39	711.22	749.47	894.65	1,031.55	813.02	1,033.32	1,176.08	1,146.91	1,594.32	1,163.45	1,030.43	802.34
<i>Standing</i>	12,029	6.01	1.37	701.39	739.64	884.82	1,021.72	803.19	1,023.49	1,166.25	1,137.08	1,584.49	1,153.62	1,020.60	792.51
<i>Working</i>	118	0.06	0.01	9.83	9.83	9.83	9.83	9.83	9.83	9.83	9.83	9.83	9.83	9.83	9.83
30533															
<i>Total</i>	2,489	1.24	0.28	146.14	153.92	183.47	211.33	166.86	211.69	240.75	234.81	325.88	238.18	211.11	164.68
<i>Standing</i>	2,448	1.22	0.28	142.75	150.54	180.09	207.95	163.47	208.31	237.37	231.43	322.49	234.80	207.72	161.30
<i>Working</i>	41	0.02	0.00	3.38	3.38	3.38	3.38	3.38	3.38	3.38	3.38	3.38	3.38	3.38	3.38
30535															
<i>Total</i>	12,146	6.07	1.39	711.12	749.37	894.55	1,031.45	812.92	1,033.22	1,175.98	1,146.81	1,594.22	1,163.35	1,030.33	802.24
<i>Standing</i>	12,029	6.01	1.37	701.39	739.64	884.82	1,021.72	803.19	1,023.49	1,166.25	1,137.08	1,584.49	1,153.62	1,020.60	792.51
<i>Working</i>	117	0.06	0.01	9.73	9.73	9.73	9.73	9.73	9.73	9.73	9.73	9.73	9.73	9.73	9.73
SubTotal	43,618	21.81	4.98												
FRT Tanks															
17413															
<i>Total</i>	5,561	2.78	0.63	192.30	201.87	268.94	381.90	530.19	711.09	840.62	810.76	636.86	443.69	315.75	227.22
<i>Standing</i>	353	0.18	0.04	9.14	10.15	16.51	25.72	38.70	50.01	59.20	53.08	38.53	26.01	15.17	10.32
<i>Working</i>	5,209	2.60	0.59	183.17	191.72	252.43	356.18	491.50	661.08	781.43	757.68	598.32	417.68	300.57	216.91
17415															
<i>Total</i>	1,972	0.99	0.23	68.18	71.58	95.35	135.41	187.99	252.15	298.08	287.48	225.82	157.32	111.96	80.56
<i>Standing</i>	125	0.06	0.01	3.24	3.60	5.85	9.12	13.72	17.74	21.01	18.84	13.67	9.22	5.38	3.65
<i>Working</i>	1,847	0.92	0.21	64.94	67.99	89.50	126.29	174.27	234.41	277.07	268.65	212.16	148.10	106.58	76.91
SubTotal	7,533	3.77	0.86												
Horizontal Tanks															
10454A															
<i>Total</i>	33	0.02	0.00	0.95	1.05	1.50	2.29	3.33	4.52	5.35	5.00	3.80	2.53	1.66	1.13
<i>Standing</i>	12	0.01	0.00	0.27	0.31	0.53	0.86	1.34	1.76	2.10	1.86	1.32	0.86	0.47	0.31
<i>Working</i>	21	0.01	0.00	0.68	0.74	0.97	1.43	1.99	2.76	3.25	3.15	2.48	1.67	1.19	0.82
10455A															
<i>Total</i>	33	0.02	0.00	0.95	1.05	1.50	2.29	3.33	4.52	5.35	5.00	3.80	2.53	1.66	1.13
<i>Standing</i>	12	0.01	0.00	0.27	0.31	0.53	0.86	1.34	1.76	2.10	1.86	1.32	0.86	0.47	0.31
<i>Working</i>	21	0.01	0.00	0.68	0.74	0.97	1.43	1.99	2.76	3.25	3.15	2.48	1.67	1.19	0.82

Floating Roof

Material: Gasoline
Permitted Material Throughput: 259,600,000 gallons/yr (includes 10% for tank-to-tank transfers)

ID	Type	Shell Capacity (gal)	Calculated Throughput (gal/yr)	Diameter	Tank Height or Length
17414	IFR	2,356,148	40,548,985	117	36
30531	IFR	1,136,066	19,551,541	70	48
30532	IFR	2,321,969	39,960,769	100	48
30534	IFR	4,351,191	74,883,403	134	48
30533	IFR	612,766	10,545,619	50	48
30535	IFR	4,306,233	74,109,682	134	48

Total = 15,084,373

Fixed Roof

Material: Distillate
Permitted Material Throughput: 1,561,010,000 gallons/yr (includes 10% for tank-to-tank transfers)

ID	Type	Shell Capacity (gal)	Calculated Throughput (gal/yr)	Diameter	Tank Height or Length
17413	FRT	2,512,053	1,151,804,368	117	36
17415	FRT	892,466	409,205,632	78	29

Total = 3,404,519

Horizontal Tank

Material: NA
Permitted Material Throughput: NA gallons/yr

ID	Type	Max Shell Capacity (gal)	Calculated Throughput * (gal/yr)	Diameter	Tank Height or Length
10454A	HT	6,400	76,800	10	14.0
10455A	HT	6,400	76,800	10	14.0
13061A	HT	6,400	76,800	10	14.0
13316A	HT	6,400	76,800	10	14.0
10456	HT	410	4,920	4	6.0
10457	HT	6,450	77,400	8	21.3
10458	HT	6,450	77,400	8	21.3
10459B	HT	250	3,000	3.166667	5.0
10460	HT	410	4,920	5.5	4.0
10470	HT	1,250	15,000	15	5.0
10480	HT	800	9,600	13.5	3.5

Total = 41,620

*assume 12 turnovers per year.

TANK LANDINGS

Tank No.	17,414	30,531	30,532	30,534	30,533	30,535
Tank Diam	117	70	100	134	50	134
Heel Height	4.0	4.0	4.0	4.0	4.0	4.0
Volume ft3	43,005	15,394	31,416	56,410	7,854	56,410
Vol bbl	7,660	2,742	5,596	10,048	1,399	10,048
Volume gal	321,722.09	115,161	235,022	422,006	58,756	422,006
Vol liters	1,217,718	435,884	889,560	1,597,293	222,390	1,597,293
Avg Temp F	60.65	60.65	60.65	60.65	60.65	60.65
Avg Temp K	289.07	289.07	289.07	289.07	289.07	289.07
temp corr	0.9449	0.9449	0.9449	0.9449	0.9449	0.9449
moles	51,369.098	18,388	37,526	67,381	9,381	67,381
VP of VOC(psia)	7.55	7.55	7.55	7.55	7.55	7.55
VOC theo fraction	0.51	0.51	0.51	0.51	0.51	0.51
Sat Factor	0.60	0.60	0.60	0.60	0.60	0.60
moles VOC	15,823	5,664	11,559	20,756	2,890	20,756
mol weight g/g-mole	60.00	60.00	60.00	60.00	60.00	60.00
VOC grams/landing	949,402	339,840	693,551	1,245,340	173,388	1,245,340
VOC lbs/landing	2,093.04	749.21	1,528.99	2,745.46	382.25	2,745.46
VOC tons/landing	1.05	0.37	0.76	1.37	0.19	1.37
land/yr	3	3	3	3	3	3
average days per landing	2.0	2.0	2.0	2.0	2.0	2.0
VOC lb filling	6,279	2,248	4,587	8,236	1,147	8,236
VOC lb standing	1,909	683	1,394	2,504	349	2,504
VOC lb/hr when landing	57	20	42	75	10	75
VOC lb/day when landing	4,094	1,465	2,991	5,370	748	5,370
Total VOC lbs	8,188	2,931	5,981	10,740	1,495	10,740
Total VOC tons	4.09	1.47	2.99	5.37	0.75	5.37

July Vapor Fraction Speciation for Landings

	Gasoline Vapor Wt%
hexane	0.622%
benzene	0.704%
2,2,4 TMP	0.811%
toluene	0.818%
ethylbenzene	0.055%
xylenes	0.239%
naphthalene	0.0004%
cumene	0.009%

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Fugitive Emissions for PTE

Fugitive Equipment	Number of units			Emission Factor lb/hour			Light Devices (lb/yr)	Heavy Devices (lb/yr)	Gas Devices (lb/yr)	Total VOC Emission (lb/yr)
	Light Devices	Heavy Device	Gas Devices	Light Devices	Heavy Device	Gas Devices				
Flanges	504	472	54	0.000017	0.000017	0.00009	75.05568	70.29024	42.5736	187.91952
Loading Arm Valve	12	12	0	0.000095	0.000095	0.000029	9.9864	9.9864	0	19.9728
Other	0	0	0	0.000287	0.000287	0.000265	0	0	0	0
Pumps	5	5	0	0.00117	0.00117	0.000143	51.246	51.246	0	102.492
Valves	135	126	15	0.000095	0.000095	0.000029	112.347	104.8572	3.8106	221.0148
						Total	248.63508	236.37984	46.3842	531.399

HAP Speciation

HAP	Light Service Liquid Weight Percent	Heavy Service Liquid Weight Percent	Vapor Weight Percent (for gas service)	lb/year	tpy	lb/hr
hexane	1.00	0.0001	0.43	2.685209	0.001342604	0.000306531
benzene	1.80	0.001	0.47	4.696042	0.002348021	0.000536078
2,2,4 TMP	4.00	0	0.53	10.192019	0.005096009	0.001163472
toluene	7.00	0.032	0.52	17.719350	0.008859675	0.002022757
ethylbenzene	1.40	0.013	0.03	3.526598	0.001763299	0.00040258
xylenes	7.00	0.29	0.14	18.155204	0.009077602	0.002072512
naphthalene	0.42	0.07565	0.00	1.210761	0.00060538	0.000138215
cumene	0.50	0	0.00	1.243175	0.000621588	0.000141915

Total 0.029092591 tpy

MONTHLY IFR TANK VOC AND HAP ESTIMATIONS

INPUT DATA				MONTH January				MONTH February				MONTH March			
Symbol	Units	Symbol	Units	Symbol	Units	Symbol	Units	Symbol	Units	Symbol	Units	Symbol	Units		
Tank No.	17414														
Nearest US Location	Bridgeport, CT														
Product Information				Product Type				Product Type				Product Type			
Absolute Pressure	P _A	14.69	psi	Monthly Throughput (only change if actual is known)	Q _{month}	80,454.34	barrels/month	Monthly Throughput (only change if actual is known)	Q _{month}	80,454.34	barrels/month	Monthly Throughput (only change if actual is known)	Q _{month}	80,454.34	barrels/month
Average organic liquid density	W _L	5.60	lb/gal	Vapor Molecular weight	M _v	60.15		Vapor Molecular weight	M _v	60.15		Vapor Molecular weight	M _v	60.15	
Average Reid Vapor Pressure	RVP	13.00		Vapor Pressure Equation Constant A	A	11.60		Vapor Pressure Equation Constant A	A	11.60		Vapor Pressure Equation Constant A	A	11.60	
Product factor; 0.4 for crude oils or 1 for other organic liquids	K _c	1.00		Vapor Pressure Equation Constant B	B	4937.93	°R	Vapor Pressure Equation Constant B	B	4937.93	°R	Vapor Pressure Equation Constant B	B	4937.93	°R
Tank design data				Average Daily Ambient Temperature Eq. 1-30				Average Daily Ambient Temperature Eq. 1-30				Average Daily Ambient Temperature Eq. 1-30			
Tank design factor		0		Daily total solar insolation on a horizontal surface	I	560.0	Btu/ft ² -day	Daily total solar insolation on a horizontal surface	I	847.0	Btu/ft ² -day	Daily total solar insolation on a horizontal surface	I	1156.0	Btu/ft ² -day
Shell height	H _s	36.00	ft	TAA = ((TAX+TAN)/2)				TAA = ((TAX+TAN)/2)				TAA = ((TAX+TAN)/2)			
Diameter	D	117.00	ft	Average daily maximum ambient temperature, Table 7.1-7				Average daily maximum ambient temperature, Table 7.1-7				Average daily maximum ambient temperature, Table 7.1-7			
Throughput	Q	3,379,082	gal/month	Average daily minimum ambient temperature, Table 7.1-7				Average daily minimum ambient temperature, Table 7.1-7				Average daily minimum ambient temperature, Table 7.1-7			
Maximum Filling Height (use Hs-1 if unknown)	H _{LQ}	35.00	ft	Liquid Bulk Temperature Eq. 1-31:				Liquid Bulk Temperature Eq. 1-31:				Liquid Bulk Temperature Eq. 1-31:			
Minimum Filling Height (use 1 if unknown)	H _{Lm}	1.00	ft	TB = TAA + 0.003 as I				TB = TAA + 0.003 as I				TB = TAA + 0.003 as I			
Liquid height (assume 1/2 Hs)	H _L	18.00	ft	Average Daily Liquid Surface Temperature Eq. 2-6				Average Daily Liquid Surface Temperature Eq. 1-28				Average Daily Liquid Surface Temperature Eq. 1-28			
Tank Construction (pick from drop down list)		Riveted		TLA = 0.3*TAA + 0.7*TB + 0.004*α ¹				TLA = 0.3*TAA + 0.7*TB + 0.004*α ¹				TLA = 0.3*TAA + 0.7*TB + 0.004*α ¹			
Tank Color (pick from drop down list)		White		True Vapor Pressure Eq. 1-25:				True Vapor Pressure Eq. 1-25:				True Vapor Pressure Eq. 1-25:			
Tank Shell Condition (pick from drop down list)		Average		P _{VA} = exp(A-(B/TLA))				P _{VA} = exp(A-(B/TLA))				P _{VA} = exp(A-(B/TLA))			
Tank Interior Condition (pick from drop down list)		Light Rust		Vapor pressure function Eq. 2-4:				Vapor pressure function Eq. 2-4:				Vapor pressure function Eq. 2-4:			
Tank paint solar absorptance, dimensionless, Table 7.1-6	α	0.25		P* = P _{VA} / (P _A / (1 + (1 - (P _{VA} / P _A)) ^{0.5})) ²				P* = P _{VA} / (P _A / (1 + (1 - (P _{VA} / P _A)) ^{0.5})) ²				P* = P _{VA} / (P _A / (1 + (1 - (P _{VA} / P _A)) ^{0.5})) ²			
Internal floating roof design data				Rim Seal Losses Eq. 2-3:				Rim Seal Losses Eq. 2-3:				Rim Seal Losses Eq. 2-3:			
Rim Seal Type:		Vapor-mounted seal	Rim-mounted secondary	L _R = ((K _{RA} + K _{RB} √V) DP* M _v K _c) / 12 months				L _R = ((K _{RA} + K _{RB} √V) DP* M _v K _c) / 12 months				L _R = ((K _{RA} + K _{RB} √V) DP* M _v K _c) / 12 months			
Rim Seal Fit (Average or Tight fitting)		Average		Withdrawal losses Eq. 2-19:				Withdrawal losses Eq. 2-19:				Withdrawal losses Eq. 2-19:			
Number of fixed roof support columns	N _c	16.00	NA	L _W = (((0.943)QC _s W _L) / D) * [1 + (N _c F _r /D)]				L _W = (((0.943)QC _s W _L) / D) * [1 + (N _c F _r /D)]				L _W = (((0.943)QC _s W _L) / D) * [1 + (N _c F _r /D)]			
Effective column diameter (1.1 for 9x7 in. built up columns; 0.7 for 8 in. pipe columns; 1.0 for 6 in. pipe columns)	F _c	1.00	ft	Deck Fitting Losses Eq. 2-13:				Deck Fitting Losses Eq. 2-13:				Deck Fitting Losses Eq. 2-13:			
Deck seam loss per unit seam length factor; 0.0 or 0.14	KD	0.14	lb-mole/ft-yr	L _F = F _r P* M _v K _c				L _F = F _r P* M _v K _c				L _F = F _r P* M _v K _c			
Zero wind speed LR factor; see Table 7.1-8	KR _a	2.2	lb-mole/ft-yr	Deck Seam Losses Eq. 2-18:				Deck Seam Losses Eq. 2-18:				Deck Seam Losses Eq. 2-18:			
Wind speed dependent LR factor; see Table 7.1-8	KR _b	0.0	lb-mole/(mph) ^{1.75} /yr	L _D = K _D S _D D ² P* M _v K _c / 12 months				L _D = K _D S _D D ² P* M _v K _c / 12 months				L _D = K _D S _D D ² P* M _v K _c / 12 months			
Average ambient wind speed at tank site; for IFR use Zero	v	0.0	mph	HAPS Speciation				HAPS Speciation				HAPS Speciation			
Seal-related wind speed exponent; see Table 7.1-8	n	4.3	NA	Product - select from list				Product - same as January				Product - same as January			
Shell cladding factor; see Table 7.1-10	C _s	0.0015	bb/1,000 ft ²	Total HAP Monthly Emissions				Total HAP Monthly Emissions				Total HAP Monthly Emissions			
Deck Design Data				Individual HAP Monthly Emissions Eq. 40-2 L_{T1} = Z_{vi}(L_R + L_F + L_D) + Z_LL_W				Individual HAP Monthly Emissions Eq. 40-2 L_{T1} = Z_{vi}(L_R + L_F + L_D) + Z_LL_W				Individual HAP Monthly Emissions Eq. 40-2 L_{T1} = Z_{vi}(L_R + L_F + L_D) + Z_LL_W			
Deck Seam (choose Welded or Bolted)		Bolted		hexane				hexane				hexane			
Select Deck Construction Type		Continuous sheet		benzene				benzene				benzene			
If bolted continuous sheet or panel, enter width		5	ft	Toluene				Toluene				Toluene			
If bolted panel, also enter length		0	ft	ethylbenzene				ethylbenzene				ethylbenzene			
Deck seam length factor; Length of Seam / Area of Deck	SD	0.20	ft/ft ²	xylene				xylene				xylene			
Deck Fitting Data				cumene				cumene				cumene			
Access Hatch Bolted cover, gasketed	2	1.6		Vapor Weight Concentrations Eq. 40-6 Z _{vi} = y _i M _i / M _v				Vapor Weight Concentrations Eq. 40-6 Z _{vi} = y _i M _i / M _v				Vapor Weight Concentrations Eq. 40-6 Z _{vi} = y _i M _i / M _v			
Column Well Built-up column, gasketed sliding cover	16	33.0		hexane				hexane				hexane			
Unslotted Guidepole and Well Gasketed sliding cover w/pole sleeve	0	8.6		benzene				benzene				benzene			
Slotted guidepole/sample well Gasketed sliding cover, with pole sleeve	0	11.0		toluene				toluene				toluene			
Gauge-float well (automatic g) Bolted cover, gasketed	0	2.8		ethylbenzene				ethylbenzene				ethylbenzene			
Gauge-hatch/sample port Slit fabric seal, 10% open area	2	12.0		xylene				xylene				xylene			
Vacuum Breaker Weighted mechanical actuation, gasketed	1	6.2		naphthalene				naphthalene				naphthalene			
Deck drain Stub drain (1-inch diameter)	110	1.2		cumene				cumene				cumene			
Legs (IFR type) IFR type, Adjustable	0	7.9		Vapor Mole Fraction Eq. 40-5 y _i = P _i / P _{VA}				Vapor Mole Fraction Eq. 40-5 y _i = P _i / P _{VA}				Vapor Mole Fraction Eq. 40-5 y _i = P _i / P _{VA}			
Rim Vent Weighted mechanical actuation, gasketed	0	0.7		hexane				hexane				hexane			
Ladder Sliding cover, gasketed	1	56.0		benzene				benzene				benzene			
Ladder / Guide-Pole Combinat Ladder sleeve, gasketed sliding cover	0	60.0		toluene				toluene				toluene			
Monthly deck fitting loss factor				ethylbenzene				ethylbenzene				ethylbenzene			
	F _r	62.45	per month	xylene				xylene				xylene			
				naphthalene				naphthalene				naphthalene			
				cumene				cumene				cumene			
Liquid Mole Fraction Eq. 40-4 x_i = (Z_{vi}M_i) / M_v				Liquid Mole Fraction Eq. 40-4 x_i = (Z_{vi}M_i) / M_v				Liquid Mole Fraction Eq. 40-4 x_i = (Z_{vi}M_i) / M_v				Liquid Mole Fraction Eq. 40-4 x_i = (Z_{vi}M_i) / M_v			
				hexane				hexane				hexane			
				benzene				benzene				benzene			
				toluene				toluene				toluene			
				ethylbenzene				ethylbenzene				ethylbenzene			
				xylene				xylene				xylene			
				naphthalene				naphthalene				naphthalene			
				cumene				cumene				cumene			
Component Vapor pressure P_{VA} = (0.019337)10⁴(A-(B/(TLA+C)))				Component Vapor pressure P_{VA} = (0.019337)10⁴(A-(B/(TLA+C)))				Component Vapor pressure P_{VA} = (0.019337)10⁴(A-(B/(TLA+C)))				Component Vapor pressure P_{VA} = (0.019337)10⁴(A-(B/(TLA+C)))			
				hexane				hexane				hexane			
				benzene				benzene				benzene			
				toluene				toluene				toluene			
				ethylbenzene				ethylbenzene				ethylbenzene			
				xylene				xylene				xylene			
				naphthalene				naphthalene				naphthalene			
				cumene				cumene				cumene			

¹ Deck legs determined from AP-42 Table 7.1-15. Stub drains determined from AP-42 7.1-15. All other fitting data taken from assumptions provided in Global IFR roof summary table

MONTH April				MONTH May				MONTH June			
ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units
Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D$)				Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D$)				Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D$)			
		LT	984.77 lb/month			LT	775.47 lb/month			LT	986.47 lb/month
			0.49 tons/month				0.39 tons/month				0.49 tons/month
Product Type Gasoline - RVP 13.5				Product Type Gasoline - RVP 9				Product Type Gasoline - RVP 9			
Monthly Throughput (only change if actual is known)				Monthly Throughput (only change if actual is known)				Monthly Throughput (only change if actual is known)			
		Q_{month}	80,454.34 barrels/month			Q_{month}	80,454.34 barrels/month			Q_{month}	80,454.34 barrels/month
Vapor Molecular weight				Vapor Molecular weight				Vapor Molecular weight			
		M_v	62.00			M_v	68.00			M_v	68.00
Vapor Pressure Equation Constant A				Vapor Pressure Equation Constant A				Vapor Pressure Equation Constant A			
		A	11.63			A	11.76			A	11.76
Vapor Pressure Equation Constant B				Vapor Pressure Equation Constant B				Vapor Pressure Equation Constant B			
		B	5015.72			B	5315.06			B	5315.06
Daily total solar insolation on a horizontal surface				Daily total solar insolation on a horizontal surface				Daily total solar insolation on a horizontal surface			
		I	1490.0 Btu/ft ² -day			I	1750.0 Btu/ft ² -day			I	1862.0 Btu/ft ² -day
Average Daily Ambient Temperature Eq. 1-30				Average Daily Ambient Temperature Eq. 1-30				Average Daily Ambient Temperature Eq. 1-30			
		$T_{AA} = ((TAX+TAN)/2)$	T_{AA}			$T_{AA} = ((TAX+TAN)/2)$	T_{AA}			$T_{AA} = ((TAX+TAN)/2)$	T_{AA}
		Average daily maximum ambient temperature, Table 7.1	509.15 °R			Average daily maximum ambient temperature, Table 7.1-7	518.65 °R			Average daily maximum ambient temperature, Table 7.1-7	528.60 °R
		Average daily minimum ambient temperature, Table 7.1	516.80 °R			Average daily minimum ambient temperature, Table 7.1-7	526.50 °R			Average daily minimum ambient temperature, Table 7.1-7	536.10 °R
Liquid Bulk Temperature Eq. 1-31:				Liquid Bulk Temperature Eq. 1-31:				Liquid Bulk Temperature Eq. 1-31:			
		$T_B = TAA + 0.003 \text{ as I}$	T_B			$T_B = TAA + 0.003 \text{ as I}$	T_B			$T_B = TAA + 0.003 \text{ as I}$	T_B
		Average Daily Liquid Surface Temperature Eq. 1-28	510.27			Average Daily Liquid Surface Temperature Eq. 1-28	519.96			Average Daily Liquid Surface Temperature Eq. 1-28	530.00
		$TLA = 0.3 \cdot TAA + 0.7 \cdot TB + 0.004 \cdot \alpha \cdot I$	T_{LA}			$TLA = 0.3 \cdot TAA + 0.7 \cdot TB + 0.004 \cdot \alpha \cdot I$	T_{LA}			$TLA = 0.3 \cdot TAA + 0.7 \cdot TB + 0.004 \cdot \alpha \cdot I$	T_{LA}
		True Vapor Pressure Eq. 1-25:	511.42 °R			True Vapor Pressure Eq. 1-25:	521.32 °R			True Vapor Pressure Eq. 1-25:	531.44 °R
		$PvA = \exp(A - (B/TLA))$	P_{vA}			$PvA = \exp(A - (B/TLA))$	P_{vA}			$PvA = \exp(A - (B/TLA))$	P_{vA}
		Vapor pressure function Eq. 2-4:	6.201 psia			Vapor pressure function Eq. 2-4:	4.763 psia			Vapor pressure function Eq. 2-4:	5.783 psia
		$P^* = P_{vA} / (P_{vA} + (1 - (P_{vA}/P_{atm}))^{0.5})^2$	P^*			$P^* = P_{vA} / (P_{vA} + (1 - (P_{vA}/P_{atm}))^{0.5})^2$	P^*			$P^* = P_{vA} / (P_{vA} + (1 - (P_{vA}/P_{atm}))^{0.5})^2$	P^*
		Rim Seal Losses Eq. 2-3:	0.136 NA			Rim Seal Losses Eq. 2-3:	0.098 NA			Rim Seal Losses Eq. 2-3:	0.124 NA
		$L_R = ((K_{sa} + K_{sb} \cdot V) / DP) \cdot M_v \cdot K_v / 12 \text{ months}$	L_R			$L_R = ((K_{sa} + K_{sb} \cdot V) / DP) \cdot M_v \cdot K_v / 12 \text{ months}$	L_R			$L_R = ((K_{sa} + K_{sb} \cdot V) / DP) \cdot M_v \cdot K_v / 12 \text{ months}$	L_R
		Withdrawal losses Eq. 2-19:	181.20 lb/month			Withdrawal losses Eq. 2-19:	142.45 lb/month			Withdrawal losses Eq. 2-19:	181.52 lb/month
		$L_W = (((0.943) \cdot QCsW_v) / D) \cdot [1 + (N_v \cdot F_v / D)]$	L_W			$L_W = (((0.943) \cdot QCsW_v) / D) \cdot [1 + (N_v \cdot F_v / D)]$	L_W			$L_W = (((0.943) \cdot QCsW_v) / D) \cdot [1 + (N_v \cdot F_v / D)]$	L_W
Deck Fitting Losses Eq. 2-13:				Deck Fitting Losses Eq. 2-13:				Deck Fitting Losses Eq. 2-13:			
		$L_F = F_f \cdot P^* \cdot M_v \cdot K_v$	527.55 lb/month			$L_F = F_f \cdot P^* \cdot M_v \cdot K_v$	414.72 lb/month			$L_F = F_f \cdot P^* \cdot M_v \cdot K_v$	528.47 lb/month
Deck Seam Losses Eq. 2-18:				Deck Seam Losses Eq. 2-18:				Deck Seam Losses Eq. 2-18:			
		$L_D = K_D \cdot S_D \cdot D^2 \cdot P^* \cdot M_v \cdot K_v / 12 \text{ months}$	269.83 lb/month			$L_D = K_D \cdot S_D \cdot D^2 \cdot P^* \cdot M_v \cdot K_v / 12 \text{ months}$	212.11 lb/month			$L_D = K_D \cdot S_D \cdot D^2 \cdot P^* \cdot M_v \cdot K_v / 12 \text{ months}$	270.29 lb/month
HAPS Speciation				HAPS Speciation				HAPS Speciation			
Product - same as January Gasoline				Product - same as January Gasoline				Product - same as January Gasoline			
Total HAP Monthly Emissions				Total HAP Monthly Emissions				Total HAP Monthly Emissions			
			18.897 lb/month				23.265 lb/month				31.927 lb/month
Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{vi}L_W$				Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{vi}L_W$				Individual HAP Monthly Emission Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{vi}L_W$			
		L_{Ti}				L_{Ti}				L_{Ti}	
		hexane	3.6600 lb/month			hexane	4.4240 lb/month			hexane	5.9722 lb/month
		benzene	4.0201 lb/month			benzene	4.9320 lb/month			benzene	6.7518 lb/month
		2,2,4 TMP	4.6301 lb/month			2,2,4 TMP	5.7117 lb/month			2,2,4 TMP	7.8549 lb/month
		toluene	4.6125 lb/month			toluene	5.7626 lb/month			toluene	8.0186 lb/month
		ethylbenzene	0.3402 lb/month			ethylbenzene	0.4227 lb/month			ethylbenzene	0.5830 lb/month
		xylenes	1.5351 lb/month			xylenes	1.8976 lb/month			xylenes	2.6021 lb/month
		naphthalene	0.0273 lb/month			naphthalene	0.0280 lb/month			naphthalene	0.0295 lb/month
		cumene	0.0718 lb/month			cumene	0.0866 lb/month			cumene	0.1152 lb/month
Vapor Weight Concentrations Eq. 40-4 $Z_{vi} = y_i M_i / M_v$				Vapor Weight Concentrations Eq. 40-4 $Z_{vi} = y_i M_i / M_v$				Vapor Weight Concentrations Eq. 40-4 $Z_{vi} = y_i M_i / M_v$			
		Z_{vi}				Z_{vi}				Z_{vi}	
		hexane	0.00368			hexane	0.00567			hexane	0.00603
		benzene	0.00399			benzene	0.00627			benzene	0.00677
		2,2,4 TMP	0.00448			2,2,4 TMP	0.00710			2,2,4 TMP	0.00776
		toluene	0.00427			toluene	0.00693			toluene	0.00774
		ethylbenzene	0.00026			ethylbenzene	0.00044			ethylbenzene	0.00051
		xylenes	0.00113			xylenes	0.00190			xylenes	0.00221
		naphthalene	0.00000			naphthalene	0.00000			naphthalene	0.00000
		cumene	0.00004			cumene	0.00007			cumene	0.00009
Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{vA}$				Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{vA}$				Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{vA}$			
		y_i				y_i				y_i	
		hexane	0.00265			hexane	0.00447			hexane	0.00476
		benzene	0.00317			benzene	0.00546			benzene	0.00590
		2,2,4 TMP	0.00243			2,2,4 TMP	0.00423			2,2,4 TMP	0.00462
		toluene	0.00287			toluene	0.00511			toluene	0.00571
		ethylbenzene	0.00015			ethylbenzene	0.00028			ethylbenzene	0.00032
		xylenes	0.00066			xylenes	0.00122			xylenes	0.00142
		naphthalene	0.00000			naphthalene	0.00000			naphthalene	0.00002
		cumene	0.00002			cumene	0.00004			cumene	0.00005
Liquid Mole Fraction Eq. 40-4 $X_i = (Z_{vi} M_i) / M_l$				Liquid Mole Fraction Eq. 40-4 $X_i = (Z_{vi} M_i) / M_l$				Liquid Mole Fraction Eq. 40-4 $X_i = (Z_{vi} M_i) / M_l$			
		X_i				X_i				X_i	
		hexane	0.01068			hexane	0.01068			hexane	0.01068
		benzene	0.02120			benzene	0.02120			benzene	0.02120
		2,2,4 TMP	0.03222			2,2,4 TMP	0.03222			2,2,4 TMP	0.03222
		toluene	0.06989			toluene	0.06989			toluene	0.06989
		ethylbenzene	0.01213			ethylbenzene	0.01213			ethylbenzene	0.01213
		xylenes	0.06066			xylenes	0.06066			xylenes	0.06066
		naphthalene	0.00298			naphthalene	0.00298			naphthalene	0.00298
		cumene	0.00383			cumene	0.00383			cumene	0.00383
Component Vapor pressure $P_{vA} = (0.019337)10^*(A - (B/(TLA+C)))$				Component Vapor pressure $P_{vA} = (0.019337)10^*(A - (B/(TLA+C)))$				Component Vapor pressure $P_{vA} = (0.019337)10^*(A - (B/(TLA+C)))$			
		A	B			A	B			A	B
		hexane	1171.5			hexane	1171.5			hexane	1171.5
		benzene	1211			benzene	1211			benzene	1211
		2,2,4 TMP	1257.8			2,2,4 TMP	1257.8			2,2,4 TMP	1257.8
		toluene	1377.6			toluene	1377.6			toluene	1377.6
		ethylbenzene	1419.3			ethylbenzene	1419.3			ethylbenzene	1419.3
		xylenes	1462.3			xylenes	1462.3			xylenes	1462.3
		naphthalene	1831.6			naphthalene	1831.6			naphthalene	1831.6
		cumene	207.2			cumene	207.2			cumene	207.2

MONTH July				MONTH August				MONTH September						
ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units			
Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D + L_{LF}$)		LT	1,123.20	lb/month	Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D + L_{LF}$)		LT	1,095.26	lb/month	Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D + L_{LF}$)		LT	1,523.78	lb/month
			0.56	tons/month				0.55	tons/month				0.76	tons/month
Product Type			Gasoline - RVP 9		Product Type			Gasoline - RVP 9		Product Type			Gasoline - RVP 13.5	
Monthly Throughput (only change if actual is known)		Q_{month}	80,454.34	barrels/month	Monthly Throughput (only change if actual is known)		Q_{month}	80,454.34	barrels/month	Monthly Throughput (only change if actual is known)		Q_{month}	80,454.34	barrels/month
Vapor Molecular weight		M_v	68.00		Vapor Molecular weight		M_v	68.00		Vapor Molecular weight		M_v	62.00	
Vapor Pressure Equation Constant A		A	11.76		Vapor Pressure Equation Constant A		A	11.76		Vapor Pressure Equation Constant A		A	11.63	
Vapor Pressure Equation Constant B		B	5315.06	$^{\circ}R$	Vapor Pressure Equation Constant B		B	5315.06	$^{\circ}R$	Vapor Pressure Equation Constant B		B	5015.72	$^{\circ}R$
Daily total solar insolation on a horizontal surface		I	1904.0	Btu/ft ² -day	Daily total solar insolation on a horizontal surface		I	1685.0	Btu/ft ² -day	Daily total solar insolation on a horizontal surface		I	1320.0	Btu/ft ² -day
Average Daily Ambient Temperature Eq. 1-30					Average Daily Ambient Temperature Eq. 1-30					Average Daily Ambient Temperature Eq. 1-30				
TAA = ((TAX+TAN)/2)		T_{AA}	533.90	$^{\circ}R$	TAA = ((TAX+TAN)/2)		T_{AA}	533.20	$^{\circ}R$	TAA = ((TAX+TAN)/2)		T_{AA}	526.15	$^{\circ}R$
Average daily maximum ambient temperature, Table 7.1-7		T_{AX}	541.10	$^{\circ}R$	Average daily maximum ambient temperature, Table 7.1-7		T_{AX}	540.10	$^{\circ}R$	Average daily maximum ambient temperature, Table 7.1-7		T_{AX}	533.40	$^{\circ}R$
Average daily minimum ambient temperature, Table 7.1-7		T_{AN}	526.70	$^{\circ}R$	Average daily minimum ambient temperature, Table 7.1-7		T_{AN}	526.30	$^{\circ}R$	Average daily minimum ambient temperature, Table 7.1-7		T_{AN}	518.90	$^{\circ}R$
Liquid Bulk Temperature Eq. 1-31:					Liquid Bulk Temperature Eq. 1-31:					Liquid Bulk Temperature Eq. 1-31:				
TB = TAA + 0.003 as I		T_B	535.33		TB = TAA + 0.003 as I		T_B	534.46		TB = TAA + 0.003 as I		T_B	527.14	
Average Daily Liquid Surface Temperature Eq. 1-28					Average Daily Liquid Surface Temperature Eq. 1-28					Average Daily Liquid Surface Temperature Eq. 1-28				
TLA = 0.3*TAA + 0.7*TB + 0.004*alpha		T_{LA}	536.80	$^{\circ}R$	TLA = 0.3*TAA + 0.7*TB + 0.004*alpha		T_{LA}	535.77	$^{\circ}R$	TLA = 0.3*TAA + 0.7*TB + 0.004*alpha		T_{LA}	528.16	$^{\circ}R$
True Vapor Pressure Eq. 1-25:					True Vapor Pressure Eq. 1-25:					True Vapor Pressure Eq. 1-25:				
PVA = exp(A-(B/TLA))		P_{VA}	6.391	psia	PVA = exp(A-(B/TLA))		P_{VA}	6.270	psia	PVA = exp(A-(B/TLA))		P_{VA}	8.462	psia
Vapor pressure function Eq. 2-4:					Vapor pressure function Eq. 2-4:					Vapor pressure function Eq. 2-4:				
$P^* = P_{VA} / P_{VA} / (1 + (1 - (P_{VA} / P_{VA}))^{0.5})^2$		P^*	0.142	NA	$P^* = P_{VA} / P_{VA} / (1 + (1 - (P_{VA} / P_{VA}))^{0.5})^2$		P^*	0.138	NA	$P^* = P_{VA} / P_{VA} / (1 + (1 - (P_{VA} / P_{VA}))^{0.5})^2$		P^*	0.211	NA
Rim Seal Losses Eq. 2-3:					Rim Seal Losses Eq. 2-3:					Rim Seal Losses Eq. 2-3:				
$L_R = ((K_{Ra} + K_{Rb})^2) DP^* M_v K_c / 12 \text{ months}$		L_R	206.83	lb/month	$L_R = ((K_{Ra} + K_{Rb})^2) DP^* M_v K_c / 12 \text{ months}$		L_R	201.66	lb/month	$L_R = ((K_{Ra} + K_{Rb})^2) DP^* M_v K_c / 12 \text{ months}$		L_R	281.01	lb/month
Withdrawal losses Eq. 2-19:					Withdrawal losses Eq. 2-19:					Withdrawal losses Eq. 2-19:				
$L_W = (((0.943)QCsw)/D)^2 [1 + (N_e F_e / D)]$		L_W	6.19	lb/month	$L_W = (((0.943)QCsw)/D)^2 [1 + (N_e F_e / D)]$		L_W	6.19	lb/month	$L_W = (((0.943)QCsw)/D)^2 [1 + (N_e F_e / D)]$		L_W	6.19	lb/month
Deck Fitting Losses Eq. 2-13:					Deck Fitting Losses Eq. 2-13:					Deck Fitting Losses Eq. 2-13:				
$L_F = F_f P^* M_v K_c$		L_F	602.18	lb/month	$L_F = F_f P^* M_v K_c$		L_F	587.12	lb/month	$L_F = F_f P^* M_v K_c$		L_F	818.14	lb/month
Deck Seam Losses Eq. 2-18:					Deck Seam Losses Eq. 2-18:					Deck Seam Losses Eq. 2-18:				
$L_D = K_D S_D P^* M_v K_c / 12 \text{ months}$		L_D	307.99	lb/month	$L_D = K_D S_D P^* M_v K_c / 12 \text{ months}$		L_D	300.29	lb/month	$L_D = K_D S_D P^* M_v K_c / 12 \text{ months}$		L_D	418.45	lb/month
HAPS Speciation					HAPS Speciation					HAPS Speciation				
Product - same as January			Gasoline		Product - same as January			Gasoline		Product - same as January			Gasoline	
Total HAP Monthly Emissions			37.837	lb/month	Total HAP Monthly Emissions			36.613	lb/month	Total HAP Monthly Emissions			33.737	lb/month
Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{vi}L_W$					Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{vi}L_W$					Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{vi}L_W$				
		L_{Ti}					L_{Ti}					L_{Ti}		
hexane			7.0073	lb/month	hexane			6.7941	lb/month	hexane			6.3841	lb/month
benzene			7.9806	lb/month	benzene			7.7268	lb/month	benzene			7.1774	lb/month
2,2,4 TMP			9.3118	lb/month	2,2,4 TMP			9.0104	lb/month	2,2,4 TMP			8.3151	lb/month
toluene			9.5744	lb/month	toluene			9.2513	lb/month	toluene			8.4210	lb/month
ethylbenzene			0.6961	lb/month	ethylbenzene			0.6725	lb/month	ethylbenzene			0.6033	lb/month
xylenes			3.1003	lb/month	xylenes			2.9961	lb/month	xylenes			2.6885	lb/month
naphthalene			0.0306	lb/month	naphthalene			0.0304	lb/month	naphthalene			0.0295	lb/month
cumene			0.1358	lb/month	cumene			0.1315	lb/month	cumene			0.1180	lb/month
Vapor Weight Concentrations Eq. 40-4 $Z_{vi} = y_i M_i / M_v$					Vapor Weight Concentrations Eq. 40-4 $Z_{vi} = y_i M_i / M_v$					Vapor Weight Concentrations Eq. 40-4 $Z_{vi} = y_i M_i / M_v$				
		M_i	M_v	Z_{vi}			M_i	M_v	Z_{vi}			M_i	M_v	Z_{vi}
hexane		86.18	68	0.00622	hexane		86.18	68	0.00618	hexane		86.18	62	0.00417
benzene		78.11	68	0.00704	benzene		78.11	68	0.00699	benzene		78.11	62	0.00466
2,2,4 TMP		114.23	68	0.00811	2,2,4 TMP		114.23	68	0.00805	2,2,4 TMP		114.23	62	0.00532
toluene		92.14	68	0.00818	toluene		92.14	68	0.00810	toluene		92.14	62	0.00526
ethylbenzene		106.17	68	0.00055	ethylbenzene		106.17	68	0.00054	ethylbenzene		106.17	62	0.00034
xylenes		106.17	68	0.00239	xylenes		106.17	68	0.00235	xylenes		106.17	62	0.00149
naphthalene		128.17	68	0.00000	naphthalene		128.17	68	0.00000	naphthalene		128.17	62	0.00000
cumene		120.19	68	0.00009	cumene		120.19	68	0.00009	cumene		120.19	62	0.00006
Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{VA}$					Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{VA}$					Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{VA}$				
		$P_i = P_{VA}(x_i)$	P_{VA}	y_i			$P_i = P_{VA}(x_i)$	P_{VA}	y_i			$P_i = P_{VA}(x_i)$	P_{VA}	y_i
hexane		0.031357	6.391	0.00491	hexane		0.030584	6.270	0.00488	hexane		0.025362	8.462	0.00300
benzene		0.039198	6.391	0.00613	benzene		0.038170	6.270	0.00609	benzene		0.031274	8.462	0.00370
2,2,4 TMP		0.030873	6.391	0.00483	2,2,4 TMP		0.030033	6.270	0.00479	2,2,4 TMP		0.024416	8.462	0.00289
toluene		0.038599	6.391	0.00604	toluene		0.037467	6.270	0.00598	toluene		0.029970	8.462	0.00354
ethylbenzene		0.002233	6.391	0.00035	ethylbenzene		0.002160	6.270	0.00034	ethylbenzene		0.001682	8.462	0.00020
xylenes		0.009773	6.391	0.00153	xylenes		0.009450	6.270	0.00151	xylenes		0.007343	8.462	0.00087
naphthalene		0.000015	6.391	0.00000	naphthalene		0.000014	6.270	0.00000	naphthalene		0.000010	8.462	0.00000
cumene		0.000339	6.391	0.00005	cumene		0.000327	6.270	0.00005	cumene		0.000250	8.462	0.00003
Liquid Mole Fraction Eq. 40-4 $x_i = (Z_{vi} M_i) / M_i$					Liquid Mole Fraction Eq. 40-4 $x_i = (Z_{vi} M_i) / M_i$					Liquid Mole Fraction Eq. 40-4 $x_i = (Z_{vi} M_i) / M_i$				
		Z_{vi}	M_i	x_i			Z_{vi}	M_i	x_i			Z_{vi}	M_i	x_i
hexane		0.01	92	0.01068	hexane		0.01	92	0.01068	hexane		0.01	92	0.01068
benzene		0.018	92	0.02120	benzene		0.018	92	0.02120	benzene		0.018	92	0.02120
2,2,4 TMP		0.04	92	0.03222	2,2,4 TMP		0.04	92	0.03222	2,2,4 TMP		0.04	92	0.03222
toluene		0.07	92	0.06989	toluene		0.07	92	0.06989	toluene		0.07	92	0.06989
ethylbenzene		0.014	92	0.01213	ethylbenzene		0.014	92	0.01213	ethylbenzene		0.014	92	0.01213
xylenes		0.07	92	0.06066	xylenes		0.07	92	0.06066	xylenes		0.07	92	0.06066
naphthalene		0.00415	92	0.00298	naphthalene		0.00415	92	0.00298	naphthalene		0.00415	92	0.00298
cumene		0.005	92	0.00383	cumene		0.005	92	0.00383	cumene		0.005	92	0.00383
Component Vapor pressure $P_{VA} = (0.019337)10^4 (A - (B/(TLA+C)))$					Component Vapor pressure $P_{VA} = (0.019337)10^4 (A - (B/(TLA+C)))$					Component Vapor pressure $P_{VA} = (0.019337)10^4 (A - (B/(TLA+C)))$				
		A	B	C			A	B	C			A	B	C
hexane		6.878	1171.5	224.37	hexane		6.878	1171.5	224.37	hexane		6.878	1171.5	224.37
benzene		6.906	1211	220.79	benzene		6.906	1211	220.79	benzene		6.906	1211	220.79
2,2,4 TMP		6.812	1257.8	220.74	2,2,4 TMP		6.812	1257.8	220.74	2,2,4 TMP		6.812	1257.8	220.74
toluene		7.017	1377.6	222.64	toluene		7.017	1377.6	222.64	toluene		7.017	1377.6	222.64
ethylbenzene		6.95	1419.3	212.61	ethylbenzene		6.95	1419.3	212.61	ethylbenzene		6.95	1419.3	212.61
xylenes		7.009	1462.3	215.11	xylenes		7.009	1462.3	215.11	xylenes		7.009	1462.3	215.11
naphthalene		7.146	1831.6	211.82	naphthalene		7.146	1831.6	211.82	naphthalene		7.146	1831.6	211.82
cumene		6.929	1455.8	207.2	cumene		6.929	1455.8	207.2	cumene		6.929	1455.8	207.2

MONTH October				MONTH November				MONTH December			
ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units
Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_F + L_D$)				Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_F + L_D$)				Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_F + L_D$)			
		LT	1,111.10 lb/month			LT	983.70 lb/month			LT	765.24 lb/month
			0.56 tons/month				0.49 tons/month				0.38 tons/month
Product Type Gasoline - RVP 13.5				Product Type Gasoline - RVP 15				Product Type Gasoline - RVP 15			
Monthly Throughput (only change if actual is known)				Monthly Throughput (only change if actual is known)				Monthly Throughput (only change if actual is known)			
		Q_{month}	80,454.34 barrels/month			Q_{month}	80,454.34 barrels/month			Q_{month}	80,454.34 barrels/month
Vapor Molecular weight		M_v	62.00	Vapor Molecular weight		M_v	60.15	Vapor Molecular weight		M_v	60.15
Vapor Pressure Equation Constant A		A	11.63	Vapor Pressure Equation Constant A		A	11.60	Vapor Pressure Equation Constant A		A	11.60
Vapor Pressure Equation Constant B		B	5015.72	Vapor Pressure Equation Constant B		B	4937.93	Vapor Pressure Equation Constant B		B	4937.93
Daily total solar insolation on a horizontal surface		I	948.0 Btu/ft ² -day	Daily total solar insolation on a horizontal surface		I	621.0 Btu/ft ² -day	Daily total solar insolation on a horizontal surface		I	501.0 Btu/ft ² -day
Average Daily Ambient Temperature Eq. 1-30				Average Daily Ambient Temperature Eq. 1-30				Average Daily Ambient Temperature Eq. 1-30			
TAA = ((TAX+TAN)/2)		T_{AA}	514.75 °R	TAA = ((TAX+TAN)/2)		T_{AA}	505.35 °R	TAA = ((TAX+TAN)/2)		T_{AA}	495.50 °R
Average daily maximum ambient temperature, Table 7.1-7		T_{AX}	522.40 °R	Average daily maximum ambient temperature, Table 7.1-7		T_{AX}	512.10 °R	Average daily maximum ambient temperature, Table 7.1-7		T_{AX}	501.80 °R
Average daily minimum ambient temperature, Table 7.1-7		T_{AN}	507.10 °R	Average daily minimum ambient temperature, Table 7.1-7		T_{AN}	498.60 °R	Average daily minimum ambient temperature, Table 7.1-7		T_{AN}	489.20 °R
Liquid Bulk Temperature Eq. 1-31:				Liquid Bulk Temperature Eq. 1-31:				Liquid Bulk Temperature Eq. 1-31:			
TB = TAA + 0.003 as I		T_B	515.46	TB = TAA + 0.003 as I		T_B	505.82	TB = TAA + 0.003 as I		T_B	495.88
Average Daily Liquid Surface Temperature Eq. 1-28				Average Daily Liquid Surface Temperature Eq. 1-28				Average Daily Liquid Surface Temperature Eq. 1-28			
TLA = 0.3*TAA + 0.7*TB + 0.004*α ¹		T_{LA}	516.20 °R	TLA = 0.3*TAA + 0.7*TB + 0.004*α ¹		T_{LA}	506.30 °R	TLA = 0.3*TAA + 0.7*TB + 0.004*α ¹		T_{LA}	496.26 °R
True Vapor Pressure Eq. 1-25:				True Vapor Pressure Eq. 1-25:				True Vapor Pressure Eq. 1-25:			
PVA = exp(A-(B/TLA))		P_{VA}	6.790 psia	PVA = exp(A-(B/TLA))		P_{VA}	6.340 psia	PVA = exp(A-(B/TLA))		P_{VA}	5.205 psia
Vapor pressure function Eq. 2-4:				Vapor pressure function Eq. 2-4:				Vapor pressure function Eq. 2-4:			
$P^* = P_{VA}/P_{VA}(1+(1-(P_{VA}/P_{VA}))^{0.5})^2$		P^*	0.154 NA	$P^* = P_{VA}/P_{VA}(1+(1-(P_{VA}/P_{VA}))^{0.5})^2$		P^*	0.140 NA	$P^* = P_{VA}/P_{VA}(1+(1-(P_{VA}/P_{VA}))^{0.5})^2$		P^*	0.109 NA
Rim Seal Losses Eq. 2-3:				Rim Seal Losses Eq. 2-3:				Rim Seal Losses Eq. 2-3:			
$L_R = ((K_{G1} + K_{G2})/V)DP^* M_v K_v/12$ months		L_R	204.59 lb/month	$L_R = ((K_{G1} + K_{G2})/V)DP^* M_v K_v/12$ months		L_R	181.00 lb/month	$L_R = ((K_{G1} + K_{G2})/V)DP^* M_v K_v/12$ months		L_R	140.55 lb/month
Withdrawal losses Eq. 2-19:				Withdrawal losses Eq. 2-19:				Withdrawal losses Eq. 2-19:			
$L_W = (((0.943)QC_s W_v)/D)^{0.75} [1+(N_F/D)]$		L_W	6.19 lb/month	$L_W = (((0.943)QC_s W_v)/D)^{0.75} [1+(N_F/D)]$		L_W	6.19 lb/month	$L_W = (((0.943)QC_s W_v)/D)^{0.75} [1+(N_F/D)]$		L_W	6.19 lb/month
Deck Fitting Losses Eq. 2-13:				Deck Fitting Losses Eq. 2-13:				Deck Fitting Losses Eq. 2-13:			
$L_F = F_F P^* M_v K_v$		L_F	595.66 lb/month	$L_F = F_F P^* M_v K_v$		L_F	526.98 lb/month	$L_F = F_F P^* M_v K_v$		L_F	409.21 lb/month
Deck Seam Losses Eq. 2-18:				Deck Seam Losses Eq. 2-18:				Deck Seam Losses Eq. 2-18:			
$L_D = K_D S_D P^* M_v K_v/12$ months		L_D	304.66 lb/month	$L_D = K_D S_D P^* M_v K_v/12$ months		L_D	269.53 lb/month	$L_D = K_D S_D P^* M_v K_v/12$ months		L_D	209.29 lb/month
HAPS Speciation				HAPS Speciation				HAPS Speciation			
Product - same as January Gasoline				Product - same as January Gasoline				Product - same as January Gasoline			
Total HAP Monthly Emissions				Total HAP Monthly Emissions				Total HAP Monthly Emissions			
			22.203 lb/month				17.125 lb/month				12.235 lb/month
Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{Vi}(L_R + L_F + L_D) + Z_{Li}L_W$				Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{Vi}(L_R + L_F + L_D) + Z_{Li}L_W$				Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{Vi}(L_R + L_F + L_D) + Z_{Li}L_W$			
		L_{Ti}				L_{Ti}				L_{Ti}	
hexane			4.2778 lb/month	hexane			3.3480 lb/month	hexane			2.3991 lb/month
benzene			4.7297 lb/month	benzene			3.6481 lb/month	benzene			2.5795 lb/month
2,2,4 TMP			5.4533 lb/month	2,2,4 TMP			4.1899 lb/month	2,2,4 TMP			2.9662 lb/month
toluene			5.4524 lb/month	toluene			4.1478 lb/month	toluene			2.9333 lb/month
ethylbenzene			0.3970 lb/month	ethylbenzene			0.3074 lb/month	ethylbenzene			0.2289 lb/month
xylenes			1.7835 lb/month	xylenes			1.3909 lb/month	xylenes			1.0488 lb/month
naphthalene			0.0277 lb/month	naphthalene			0.0270 lb/month	naphthalene			0.0264 lb/month
cumene			0.0816 lb/month	cumene			0.0660 lb/month	cumene			0.0529 lb/month
Vapor Weight Concentrations Eq. 40-6 $Z_{Vi} = y_i M_i / M_v$				Vapor Weight Concentrations Eq. 40-6 $Z_{Vi} = y_i M_i / M_v$				Vapor Weight Concentrations Eq. 40-6 $Z_{Vi} = y_i M_i / M_v$			
		M_i	M_v			M_i	M_v			M_i	M_v
hexane		86.18	62	hexane		86.18	60	hexane		86.18	60
benzene		78.11	62	benzene		78.11	60	benzene		78.11	60
2,2,4 TMP		114.23	62	2,2,4 TMP		114.23	60	2,2,4 TMP		114.23	60
toluene		92.14	62	toluene		92.14	60	toluene		92.14	60
ethylbenzene		106.17	62	ethylbenzene		106.17	60	ethylbenzene		106.17	60
xylenes		106.17	62	xylenes		106.17	60	xylenes		106.17	60
naphthalene		128.17	62	naphthalene		128.17	60	naphthalene		128.17	60
cumene		120.19	62	cumene		120.19	60	cumene		120.19	60
Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{VA}$				Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{VA}$				Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{VA}$			
		$P_i = P_{VA}(k_i)$	P_{VA}			$P_i = P_{VA}(k_i)$	P_{VA}			$P_i = P_{VA}(k_i)$	P_{VA}
hexane		0.018638	6.790	hexane		0.014875	6.340	hexane		0.011186	5.205
benzene		0.022527	6.790	benzene		0.017664	6.340	benzene		0.013033	5.205
2,2,4 TMP		0.017363	6.790	2,2,4 TMP		0.013463	6.340	2,2,4 TMP		0.009817	5.205
toluene		0.020754	6.790	toluene		0.015726	6.340	toluene		0.011191	5.205
ethylbenzene		0.001114	6.790	ethylbenzene		0.000811	6.340	ethylbenzene		0.000553	5.205
xylenes		0.004845	6.790	xylenes		0.003518	6.340	xylenes		0.002391	5.205
naphthalene		0.000006	6.790	naphthalene		0.000004	6.340	naphthalene		0.000002	5.205
cumene		0.000161	6.790	cumene		0.000114	6.340	cumene		0.000075	5.205
Liquid Mole Fraction Eq. 40-4 $x_i = (Z_{Li} M_i) / M_l$				Liquid Mole Fraction Eq. 40-4 $x_i = (Z_{Li} M_i) / M_l$				Liquid Mole Fraction Eq. 40-4 $x_i = (Z_{Li} M_i) / M_l$			
		Z_{Li}	M_i			Z_{Li}	M_i			Z_{Li}	M_i
hexane		0.01	92	hexane		0.01	96	hexane		0.01	96
benzene		0.018	92	benzene		0.018	96	benzene		0.018	96
2,2,4 TMP		0.04	92	2,2,4 TMP		0.04	96	2,2,4 TMP		0.04	96
toluene		0.07	92	toluene		0.07	96	toluene		0.07	96
ethylbenzene		0.014	92	ethylbenzene		0.014	96	ethylbenzene		0.014	96
xylenes		0.07	92	xylenes		0.07	96	xylenes		0.07	96
naphthalene		0.00415	92	naphthalene		0.00415	96	naphthalene		0.00415	96
cumene		0.005	92	cumene		0.005	96	cumene		0.005	96
Component Vapor pressure $P_{VA} = (0.019337)10^*(A-(B/(TLA+C)))$				Component Vapor pressure $P_{VA} = (0.019337)10^*(A-(B/(TLA+C)))$				Component Vapor pressure $P_{VA} = (0.019337)10^*(A-(B/(TLA+C)))$			
		A	B			A	B			A	B
hexane		6.878	1171.5	hexane		6.878	1171.5	hexane		6.878	1171.5
benzene		6.906	1211	benzene		6.906	1211	benzene		6.906	1211
2,2,4 TMP		6.812	1257.8	2,2,4 TMP		6.812	1257.8	2,2,4 TMP		6.812	1257.8
toluene		7.017	1377.6	toluene		7.017	1377.6	toluene		7.017	1377.6
ethylbenzene		6.95	1419.3	ethylbenzene		6.95	1419.3	ethylbenzene		6.95	1419.3
xylenes		7.009	1462.3	xylenes		7.009	1462.3	xylenes		7.009	1462.3
naphthalene		7.146	1831.6	naphthalene		7.146	1831.6	naphthalene		7.146	1831.6
cumene		6.929	1455.8	cumene		6.929	1455.8	cumene		6.929	1455.8

MONTHLY IFR TANK VOC AND HAP ESTIMATIONS

INPUT DATA				MONTH January				MONTH February				MONTH March			
Tank No.	Symbol	Units		Symbol	Units	Symbol	Units	Symbol	Units	Symbol	Units	Symbol	Units		
30531															
Nearest US Location		Bridgeport, CT		Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D + L_P$)	LT	141.88	lb/month	Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D + L_P$)	LT	149.37	lb/month	Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D + L_P$)	LT	177.83	lb/month
Absolute Pressure	P_A	14.69	psi	Product Type		Gasoline - RVP 15		Product Type		Gasoline - RVP 15		Product Type		Gasoline - RVP 15	
Product Information				Monthly Throughput (only change if actual is known)	Q_{month}	38,792.74	barrels/month	Monthly Throughput (only change if actual is known)	Q_{month}	38,792.74	barrels/month	Monthly Throughput (only change if actual is known)	Q_{month}	38,792.74	barrels/month
Average organic liquid density	W_L	5.60	lb/gal	Vapor Molecular weight	M_v	60.15		Vapor Molecular weight	M_v	60.15		Vapor Molecular weight	M_v	60.15	
Average Reid Vapor Pressure	RVP	13.00		Vapor Pressure Equation Constant A	A	11.60		Vapor Pressure Equation Constant A	A	11.60		Vapor Pressure Equation Constant A	A	11.60	
Product factor, 0.4 for crude oils or 1 for other organic liquids	K_c	1.00		Vapor Pressure Equation Constant B	B	4937.93	$^{\circ}R$	Vapor Pressure Equation Constant B	B	4937.93	$^{\circ}R$	Vapor Pressure Equation Constant B	B	4937.93	$^{\circ}R$
Tank design data				Daily total solar insolation on a horizontal surface	I	560.0	Btu/ft ² -day	Daily total solar insolation on a horizontal surface	I	847.0	Btu/ft ² -day	Daily total solar insolation on a horizontal surface	I	1156.0	Btu/ft ² -day
Shell height	Hs	48.00	ft	Average Daily Ambient Temperature Eq. 1-30				Average Daily Ambient Temperature Eq. 1-30				Average Daily Ambient Temperature Eq. 1-30			
Diameter	D	70.00	ft	$T_{AA} = ((TAX+TAN)/2)$	T_{AA}	490.50	$^{\circ}R$	$T_{AA} = ((TAX+TAN)/2)$	T_{AA}	492.20	$^{\circ}R$	$T_{AA} = ((TAX+TAN)/2)$	T_{AA}	498.90	$^{\circ}R$
Throughput	Q	1,629,295	gal/month	Average daily maximum ambient temperature, Table 7.1-7	T_{AX}	496.90	$^{\circ}R$	Average daily maximum ambient temperature, Table 7.1-7	T_{AX}	498.80	$^{\circ}R$	Average daily maximum ambient temperature, Table 7.1-7	T_{AX}	506.00	$^{\circ}R$
Maximum Filling Height (use Hs-1 if unknown)	H_{Lx}	47.00	ft	Average daily minimum ambient temperature, Table 7.1-7	T_{AN}	484.10	$^{\circ}R$	Average daily minimum ambient temperature, Table 7.1-7	T_{AN}	485.60	$^{\circ}R$	Average daily minimum ambient temperature, Table 7.1-7	T_{AN}	491.80	$^{\circ}R$
Minimum Filling Height (use 1 if unknown)	H_{Lx}	1.00	ft	Liquid Bulk Temperature Eq. 1-31:				Liquid Bulk Temperature Eq. 1-31:				Liquid Bulk Temperature Eq. 1-31:			
Liquid height (assume 1/2 Hs)	H_L	24.00	ft	$T_B = T_{AA} + 0.003 \text{ as } 1$	T_B	490.92		$T_B = T_{AA} + 0.003 \text{ as } 1$	T_B	492.84		$T_B = T_{AA} + 0.003 \text{ as } 1$	T_B	499.77	
Tank Construction (pick from drop down list)		Welded		Average Daily Liquid Surface Temperature Eq. 2-6				Average Daily Liquid Surface Temperature Eq. 1-28				Average Daily Liquid Surface Temperature Eq. 1-28			
Tank Color (pick from drop down list)		White		$T_{LA} = 0.3T_{AA} + 0.7T_B + 0.004 \alpha^1$	T_{LA}	491.35	$^{\circ}R$	$T_{LA} = 0.3T_{AA} + 0.7T_B + 0.004 \alpha^1$	T_{LA}	493.49	$^{\circ}R$	$T_{LA} = 0.3T_{AA} + 0.7T_B + 0.004 \alpha^1$	T_{LA}	500.66	$^{\circ}R$
Tank Shell Condition (pick from drop down list)		Average		True Vapor Pressure Eq. 1-25:				True Vapor Pressure Eq. 1-25:				True Vapor Pressure Eq. 1-25:			
Tank Interior Condition (pick from drop down list)		Light Rust		$P_{VA} = \exp(A - (B/T_{LA}))$	P_{VA}	4.713	psia	$P_{VA} = \exp(A - (B/T_{LA}))$	P_{VA}	4.922	psia	$P_{VA} = \exp(A - (B/T_{LA}))$	P_{VA}	5.681	psia
Tank paint solar absorptance, dimensionless, Table 7.1-6	α	0.25		Vapor pressure function Eq. 2-4:				Vapor pressure function Eq. 2-4:				Vapor pressure function Eq. 2-4:			
				$P^* = P_{VA}/P_A / (1 + (1 - (P_{VA}/P_A))^{0.5})^2$	P^*	0.096	NA	$P^* = P_{VA}/P_A / (1 + (1 - (P_{VA}/P_A))^{0.5})^2$	P^*	0.102	NA	$P^* = P_{VA}/P_A / (1 + (1 - (P_{VA}/P_A))^{0.5})^2$	P^*	0.122	NA
Internal floating roof design data				Rim Seal Losses Eq. 2-3:				Rim Seal Losses Eq. 2-3:				Rim Seal Losses Eq. 2-3:			
Rim Seal Type:		Mechanical-shoe seal	Shoe-mounted secondary	$L_R = ((K_{S1} + K_{S2}) \sqrt{DP^* M_v K_c}) / 12 \text{ months}$	L_R	54.12	lb/month	$L_R = ((K_{S1} + K_{S2}) \sqrt{DP^* M_v K_c}) / 12 \text{ months}$	L_R	57.08	lb/month	$L_R = ((K_{S1} + K_{S2}) \sqrt{DP^* M_v K_c}) / 12 \text{ months}$	L_R	68.28	lb/month
Rim Seal Fit (Average or Tight fitting)		Average		Withdrawal losses Eq. 2-19:				Withdrawal losses Eq. 2-19:				Withdrawal losses Eq. 2-19:			
Number of fixed roof support columns	Nc	0.00	NA	$L_W = (((0.943)OCsW_v) / D)^2 [1 + (N_F/D)]$	L_W	4.39	lb/month	$L_W = (((0.943)OCsW_v) / D)^2 [1 + (N_F/D)]$	L_W	4.39	lb/month	$L_W = (((0.943)OCsW_v) / D)^2 [1 + (N_F/D)]$	L_W	4.39	lb/month
Effective column diameter (1.1 for 8x7 in. built up columns; 0.7 for 8 in. pipe columns; 1.0 for 8 in. pipe columns)	Fc	1.00	ft	Deck Fitting Losses Eq. 2-13:				Deck Fitting Losses Eq. 2-13:				Deck Fitting Losses Eq. 2-13:			
Deck seam loss per unit seam length factor, 0.0 or 0.14	KD	0.00	lb-mole/ft-yr	$L_F = F_F P^* M_v K_c$	LF	83.36	lb/month	$L_F = F_F P^* M_v K_c$	LF	87.91	lb/month	$L_F = F_F P^* M_v K_c$	LF	105.16	lb/month
Zero wind speed LR factor, see Table 7.1-8	KRa	1.6	lb-mole/ft-yr	Deck Seam Losses Eq. 2-18:				Deck Seam Losses Eq. 2-18:				Deck Seam Losses Eq. 2-18:			
Wind speed dependent LR factor, see Table 7.1-8	KRb	0.3	lb-mole/(mph) ^{1.75} ft ² yr	$L_D = K_D S_D^2 P^* M_v K_c / 12 \text{ months}$	LD	0.00	lb/month	$L_D = K_D S_D^2 P^* M_v K_c / 12 \text{ months}$	LD	0.00	lb/month	$L_D = K_D S_D^2 P^* M_v K_c / 12 \text{ months}$	LD	0.00	lb/month
Average ambient wind speed at tank site, for IFR use Zero	v	0.0	mph	HAPS Speciation				HAPS Speciation				HAPS Speciation			
Seal-related wind speed exponent, see Table 7.1-8	n	1.6	NA	Product - select from list		Gasoline		Product - same as January		Gasoline		Product - same as January		Gasoline	
Shell clingage factor, see Table 7.1-10	Cs	0.0015	bb/1,000 ft ²	Total HAP Monthly Emissions		2.855	lb/month	Total HAP Monthly Emissions		3.008	lb/month	Total HAP Monthly Emissions		3.619	lb/month
Deck Design Data				Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{Li}L_W$				Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{Li}L_W$				Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{Li}L_W$			
Deck Seam (choose Welded or Bolted)		Welded		hexane	0.4485	lb/month		hexane	0.4791	lb/month		hexane	0.5993	lb/month	
Deck construction type not required for welded seams		NA		benzene	0.5022	lb/month		benzene	0.5361	lb/month		benzene	0.6705	lb/month	
If bolted continuous sheet or panel, enter width		0		TMP	0.6389	lb/month		TMP	0.6774	lb/month		TMP	0.8306	lb/month	
If bolted panel, also enter length		0		toluene	0.7281	lb/month		toluene	0.7655	lb/month		toluene	0.9161	lb/month	
Deck seam length factor: Length of Seam / Area of Deck	SD	NA	ft/ft ²	ethylbenzene	0.0849	lb/month		ethylbenzene	0.0872	lb/month		ethylbenzene	0.0968	lb/month	
Deck Fitting Data				xylenes	0.4085	lb/month		xylenes	0.4186	lb/month		xylenes	0.4603	lb/month	
Access Hatch Bolted cover, gasketed	Qty	5	1.6	naphthalene	0.0183	lb/month		naphthalene	0.0183	lb/month		naphthalene	0.0184	lb/month	
Column Well Bolted cover, gasketed sliding cover	0	33.0		cumene	0.0255	lb/month		cumene	0.0259	lb/month		cumene	0.0275	lb/month	
Unslotted Guidepole and Well Gasketed sliding cover w/pole sleeve	0	8.6		Vapor Weight Concentrations Eq. 40-4 $Z_{vi} = y_i M_i / M_v$				Vapor Weight Concentrations Eq. 40-4 $Z_{vi} = y_i M_i / M_v$				Vapor Weight Concentrations Eq. 40-4 $Z_{vi} = y_i M_i / M_v$			
Slotted guidepole/sample well Gasketed sliding cover, with pole sleeve	0	11.0		hexane	86.18	60	0.00294	hexane	86.18	60	0.00300	hexane	86.18	60	0.00320
Gauge-float well (automatic g) Bolted cover, gasketed	0	2.8		benzene	78.11	60	0.00308	benzene	78.11	60	0.00315	benzene	78.11	60	0.00341
Gauge-hatch/sample port Slit fabric seal, 10% open area	2	12.0		2,2,4 TMP	114.23	60	0.00337	2,2,4 TMP	114.23	60	0.00346	2,2,4 TMP	114.23	60	0.00378
Vacuum Breaker Weighted mechanical actuation, gasketed	1	6.2		toluene	92.14	60	0.00306	toluene	92.14	60	0.00316	toluene	92.14	60	0.00351
Deck drain Stub drain (1-inch diameter)	0	1.2		ethylbenzene	106.17	60	0.00017	ethylbenzene	106.17	60	0.00018	ethylbenzene	106.17	60	0.00020
Legs (IFR type) IFR type, Adjustable	17	7.9		xylenes	106.17	60	0.00074	xylenes	106.17	60	0.00077	xylenes	106.17	60	0.00088
Rim Vent Weighted mechanical actuation, gasketed	0	0.7		naphthalene	128.17	60	0.00000	naphthalene	128.17	60	0.00000	naphthalene	128.17	60	0.00000
Ladder Sliding cover, gasketed	0	56.0		cumene	120.19	60	0.00003	cumene	120.19	60	0.00003	cumene	120.19	60	0.00003
Ladder / Guide-Pole Combin' Ladder sleeve, gasketed sliding cover	0	60.0		Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{VA}$				Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{VA}$				Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{VA}$			
Monthly deck fitting loss factor	F_F	14.38	per month	hexane	0.009680	4.713	0.00205	hexane	0.010314	4.922	0.00210	hexane	0.012697	5.681	0.00224
				benzene	0.011169	4.713	0.00237	benzene	0.011951	4.922	0.00243	benzene	0.014919	5.681	0.00263
				2,2,4 TMP	0.008362	4.713	0.00177	2,2,4 TMP	0.008971	4.922	0.00182	2,2,4 TMP	0.011297	5.681	0.00199
				toluene	0.009416	4.713	0.00200	toluene	0.010156	4.922	0.00206	toluene	0.013018	5.681	0.00229
				ethylbenzene	0.000455	4.713	0.00010	ethylbenzene	0.000495	4.922	0.00010	ethylbenzene	0.000655	5.681	0.00012
				xylenes	0.001965	4.713	0.00042	xylenes	0.002141	4.922	0.00044	xylenes	0.002839	5.681	0.00050
				naphthalene	0.000002	4.713	0.00000	naphthalene	0.000002	4.922	0.00000	naphthalene	0.000003	5.681	0.00000
				cumene	0.000061	4.713	0.00001	cumene	0.000067	4.922	0.00001	cumene	0.000090	5.681	0.00002
				Liquid Mole Fraction Eq. 40-4 $X_i = (Z_{Li} M_i) / M_L$				Liquid Mole Fraction Eq. 40-4 $X_i = (Z_{Li} M_i) / M_L$				Liquid Mole Fraction Eq. 40-4 $X_i = (Z_{Li} M_i) / M_L$			
				hexane	0.01	96	0.01114	hexane	0.01	96	0.01114	hexane	0.01	96	0.01114
				benzene	0.018	96	0.02212	benzene	0.018	96	0.02212	benzene	0.018	96	0.02212
				2,2,4 TMP	0.04	96	0.03362	2,2,4 TMP	0.04	96	0.03362	2,2,4 TMP	0.04	96	0.03362
				toluene	0.07	96	0.07293	toluene	0.07	96	0.07293	toluene	0.07	96	0.07293
				ethylbenzene	0.014	96	0.01266	ethylbenzene	0.014	96	0.01266	ethylbenzene	0.014	96	0.01266
				xylenes	0.07	96	0.06329	xylenes	0.07	96	0.06329	xylenes	0.07	96	0.06329
				naphthalene	0.00415	96	0.00311	naphthalene	0.00415	96	0.00311	naphthalene	0.00415	96	0.00311
				cumene	0.005	96	0.00399	cumene	0.005	96	0.00399	cumene	0.005	96	0.00399
				Component Vapor pressure $P_{VA} = (0.019337)10^4(A - (B/(TLA+C)))$				Component Vapor pressure $P_{VA} = (0.019337)10^4(A - (B/(TLA+C)))$				Component Vapor pressure $P_{VA} = (0.019337)10^4(A - (B/(TLA+C)))$			
				hexane	6.878	1171.5	224.37	hexane	6.878	1171.5	224.37	hexane	6.878	1171.5	224.37
				benzene	6.906	1211	220.79	benzene	6.906	1211	220.79	benzene	6.906	1211	220.79
				2,2,4 TMP	6.812	1257.8	220.74	2,2,4 TMP	6.812	1257.8	220.74	2,2,4 TMP	6.812	1257.8	220.74
				toluene	7										

MONTH April				MONTH May				MONTH June			
ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units
Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_F + L_D$)		LT	204.67 lb/month	Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_F + L_D$)		LT	161.83 lb/month	Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_F + L_D$)		LT	205.02 lb/month
			0.10 tons/month				0.08 tons/month				0.10 tons/month
Product Type		Gasoline - RVP 13.5		Product Type		Gasoline - RVP 9		Product Type		Gasoline - RVP 9	
Monthly Throughput (only change if actual is known)		Q_{month}	38,792.74 barrels/month	Monthly Throughput (only change if actual is known)		Q_{month}	38,792.74 barrels/month	Monthly Throughput (only change if actual is known)		Q_{month}	38,792.74 barrels/month
Vapor Molecular weight		M_v	62.00	Vapor Molecular weight		M_v	68.00	Vapor Molecular weight		M_v	68.00
Vapor Pressure Equation Constant A		A	11.63	Vapor Pressure Equation Constant A		A	11.76	Vapor Pressure Equation Constant A		A	11.76
Vapor Pressure Equation Constant B		B	5015.72 °R	Vapor Pressure Equation Constant B		B	5315.06 °R	Vapor Pressure Equation Constant B		B	5315.06 °R
Daily total solar insolation on a horizontal surface		I	1490.0 Btu/ft ² -day	Daily total solar insolation on a horizontal surface		I	1750.0 Btu/ft ² -day	Daily total solar insolation on a horizontal surface		I	1862.0 Btu/ft ² -day
Average Daily Ambient Temperature Eq. 1-30				Average Daily Ambient Temperature Eq. 1-30				Average Daily Ambient Temperature Eq. 1-30			
TAA = ((TAX+TAN)/2)		T_{AA}	509.15 °R	TAA = ((TAX+TAN)/2)		T_{AA}	518.65 °R	TAA = ((TAX+TAN)/2)		T_{AA}	528.60 °R
Average daily maximum ambient temperature, Table 7.1		T_{AX}	516.80 °R	Average daily maximum ambient temperature, Table 7.1-7		T_{AX}	526.50 °R	Average daily maximum ambient temperature, Table 7.1-7		T_{AX}	536.10 °R
Average daily minimum ambient temperature, Table 7.1		T_{AN}	501.50 °R	Average daily minimum ambient temperature, Table 7.1-7		T_{AN}	510.80 °R	Average daily minimum ambient temperature, Table 7.1-7		T_{AN}	521.10 °R
Liquid Bulk Temperature Eq. 1-31:				Liquid Bulk Temperature Eq. 1-31:				Liquid Bulk Temperature Eq. 1-31:			
TB = TAA + 0.003 cs I		T_B	510.27	TB = TAA + 0.003 cs I		T_B	519.96	TB = TAA + 0.003 cs I		T_B	530.00
Average Daily Liquid Surface Temperature Eq. 1-28				Average Daily Liquid Surface Temperature Eq. 1-28				Average Daily Liquid Surface Temperature Eq. 1-28			
TLA = 0.3*TAA + 0.7*TB + 0.004*α ¹		T_{LA}	511.42 °R	TLA = 0.3*TAA + 0.7*TB + 0.004*α ¹		T_{LA}	521.32 °R	TLA = 0.3*TAA + 0.7*TB + 0.004*α ¹		T_{LA}	531.44 °R
True Vapor Pressure Eq. 1-25:				True Vapor Pressure Eq. 1-25:				True Vapor Pressure Eq. 1-25:			
PvA = exp(A-(B/TLA))		P_{vA}	6.201 psia	PvA = exp(A-(B/TLA))		P_{vA}	4.763 psia	PvA = exp(A-(B/TLA))		P_{vA}	5.783 psia
Vapor pressure function Eq. 2-4:				Vapor pressure function Eq. 2-4:				Vapor pressure function Eq. 2-4:			
$P^* = P_{vA}/P_A/(1+(1-(P_{vA}/P_A))^{0.5})^2$		P^*	0.136 NA	$P^* = P_{vA}/P_A/(1+(1-(P_{vA}/P_A))^{0.5})^2$		P^*	0.098 NA	$P^* = P_{vA}/P_A/(1+(1-(P_{vA}/P_A))^{0.5})^2$		P^*	0.124 NA
Rim Seal Losses Eq. 2-3:				Rim Seal Losses Eq. 2-3:				Rim Seal Losses Eq. 2-3:			
$L_R = ((K_{R3} + K_{R5} \sqrt{V})/DP^* M_v K_c)/12$ months		L_R	78.84 lb/month	$L_R = ((K_{R3} + K_{R5} \sqrt{V})/DP^* M_v K_c)/12$ months		L_R	61.98 lb/month	$L_R = ((K_{R3} + K_{R5} \sqrt{V})/DP^* M_v K_c)/12$ months		L_R	78.98 lb/month
Withdrawal losses Eq. 2-19:				Withdrawal losses Eq. 2-19:				Withdrawal losses Eq. 2-19:			
$L_W = (((0.943)QC/W)/D)^{0.5} * (1 + (N_e F_e / D))$		L_W	4.39 lb/month	$L_W = (((0.943)QC/W)/D)^{0.5} * (1 + (N_e F_e / D))$		L_W	4.39 lb/month	$L_W = (((0.943)QC/W)/D)^{0.5} * (1 + (N_e F_e / D))$		L_W	4.39 lb/month
Deck Fitting Losses Eq. 2-13:				Deck Fitting Losses Eq. 2-13:				Deck Fitting Losses Eq. 2-13:			
$L_F = F_r P^* M_v K_c$		LF	121.43 lb/month	$L_F = F_r P^* M_v K_c$		LF	95.46 lb/month	$L_F = F_r P^* M_v K_c$		LF	121.64 lb/month
Deck Seam Losses Eq. 2-18:				Deck Seam Losses Eq. 2-18:				Deck Seam Losses Eq. 2-18:			
$L_D = K_D S_D P^* M_v K_c / 12$ months		LD	0.00 lb/month	$L_D = K_D S_D P^* M_v K_c / 12$ months		LD	0.00 lb/month	$L_D = K_D S_D P^* M_v K_c / 12$ months		LD	0.00 lb/month
HAPS Speciation				HAPS Speciation				HAPS Speciation			
Product - same as January		Gasoline		Product - same as January		Gasoline		Product - same as January		Gasoline	
Total HAP Monthly Emissions			4.589 lb/month	Total HAP Monthly Emissions			5.483 lb/month	Total HAP Monthly Emissions			7.256 lb/month
Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{Li}L_W$				Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{Li}L_W$				Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{Li}L_W$			
hexane		L_{Ti}	0.7803 lb/month	hexane		L_{Ti}	0.9367 lb/month	hexane		L_{Ti}	1.2535 lb/month
benzene			0.8790 lb/month	benzene			1.0656 lb/month	benzene			1.4380 lb/month
2,2,4 TMP			1.0725 lb/month	2,2,4 TMP			1.2939 lb/month	2,2,4 TMP			1.7325 lb/month
toluene			1.1626 lb/month	toluene			1.3980 lb/month	toluene			1.8597 lb/month
ethylbenzene			0.1134 lb/month	ethylbenzene			0.1302 lb/month	ethylbenzene			0.1630 lb/month
xylenes			0.5327 lb/month	xylenes			0.6069 lb/month	xylenes			0.7511 lb/month
naphthalene			0.0185 lb/month	naphthalene			0.0187 lb/month	naphthalene			0.0190 lb/month
cumene			0.0303 lb/month	cumene			0.0333 lb/month	cumene			0.0392 lb/month
Vapor Weight Concentrations Eq. 40-4 $Z_{vi} = y_i M_i / M_v$				Vapor Weight Concentrations Eq. 40-4 $Z_{vi} = y_i M_i / M_v$				Vapor Weight Concentrations Eq. 40-4 $Z_{vi} = y_i M_i / M_v$			
hexane		M_i	86.18	hexane		M_i	86.18	hexane		M_i	86.18
benzene		M_v	62	benzene		M_v	68	benzene		M_v	68
2,2,4 TMP		Z_{vi}	0.00368	2,2,4 TMP		Z_{vi}	0.00567	2,2,4 TMP		Z_{vi}	0.00603
toluene			0.00399	toluene			0.00627	toluene			0.00677
ethylbenzene			0.00448	ethylbenzene			0.00710	ethylbenzene			0.00776
xylenes			0.00427	xylenes			0.00693	xylenes			0.00774
naphthalene			0.00026	naphthalene			0.00044	naphthalene			0.00051
cumene			0.00113	cumene			0.00190	cumene			0.00221
			0.00000				0.00000				0.00000
			0.00004				0.00007				0.00009
Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{vA}$				Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{vA}$				Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{vA}$			
hexane		$P_i = P_{vA}(x_i)$	6.201	hexane		$P_i = P_{vA}(x_i)$	4.763	hexane		$P_i = P_{vA}(x_i)$	5.783
benzene		P_{vA}	0.00265	benzene		P_{vA}	0.00447	benzene		P_{vA}	0.00476
2,2,4 TMP		y_i	0.00317	2,2,4 TMP		y_i	0.00546	2,2,4 TMP		y_i	0.00590
toluene			0.00243	toluene			0.00423	toluene			0.00462
ethylbenzene			0.00287	ethylbenzene			0.00511	ethylbenzene			0.00571
xylenes			0.00015	xylenes			0.00028	xylenes			0.00032
naphthalene			0.00066	naphthalene			0.00122	naphthalene			0.00142
cumene			0.00000	cumene			0.00000	cumene			0.00000
			0.00002				0.00004				0.00005
Liquid Mole Fraction Eq. 40-4 $x_i = (Z_{Li} M_i) / M_i$				Liquid Mole Fraction Eq. 40-4 $x_i = (Z_{Li} M_i) / M_i$				Liquid Mole Fraction Eq. 40-4 $x_i = (Z_{Li} M_i) / M_i$			
hexane		Z_{Li}	0.01	hexane		Z_{Li}	0.01	hexane		Z_{Li}	0.01
benzene		M_i	86.18	benzene		M_i	86.18	benzene		M_i	86.18
2,2,4 TMP		M_v	62	2,2,4 TMP		M_v	68	2,2,4 TMP		M_v	68
toluene		X_i	0.01068	toluene		X_i	0.01068	toluene		X_i	0.01068
ethylbenzene			0.02120	ethylbenzene			0.02120	ethylbenzene			0.02120
xylenes			0.03222	xylenes			0.03222	xylenes			0.03222
naphthalene			0.06989	naphthalene			0.06989	naphthalene			0.06989
cumene			0.01213	cumene			0.01213	cumene			0.01213
			0.06066				0.06066				0.06066
			0.00298				0.00298				0.00298
			0.00000				0.00000				0.00000
			0.00005				0.00005				0.00005
			0.00383				0.00383				0.00383
Component Vapor pressure $P_{vA} = (0.019337)10^4(A-(B/(TLA+C)))$				Component Vapor pressure $P_{vA} = (0.019337)10^4(A-(B/(TLA+C)))$				Component Vapor pressure $P_{vA} = (0.019337)10^4(A-(B/(TLA+C)))$			
hexane		A	6.878	hexane		A	6.878	hexane		A	6.878
benzene		B	1171.5	benzene		B	1171.5	benzene		B	1171.5
2,2,4 TMP		C	224.37	2,2,4 TMP		C	224.37	2,2,4 TMP		C	224.37
toluene		P_{vA}	1.5366	toluene		P_{vA}	1.9962	toluene		P_{vA}	2.5773
ethylbenzene			0.9273	ethylbenzene			1.2255	ethylbenzene			1.6087
xylenes			0.4679	xylenes			0.6251	xylenes			0.8293
naphthalene			0.2550	naphthalene			0.3484	naphthalene			0.4725
cumene			0.0773	cumene			0.1098	cumene			0.1546
			0.0672				0.0957				0.1351
			0.0016				0.0026				0.0040
			0.0349				0.0509				0.0735

MONTH July				MONTH August				MONTH eptember						
ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units			
Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_F + L_D$)		LT	233.00	lb/month	Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_F + L_D$)		LT	227.28	lb/month	Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_F + L_D$)		LT	314.98	lb/month
			0.12	tons/month				0.11	tons/month				0.16	tons/month
Product Type			Gasoline - RVP 9		Product Type			Gasoline - RVP 9		Product Type			Gasoline - RVP 13.5	
Monthly Throughput (only change if actual is known)		Q_{month}	38,792.74	barrels/month	Monthly Throughput (only change if actual is known)		Q_{month}	38,792.74	barrels/month	Monthly Throughput (only change if actual is known)		Q_{month}	38,792.74	barrels/month
Vapor Molecular weight		M_v	68.00		Vapor Molecular weight		M_v	68.00		Vapor Molecular weight		M_v	62.00	
Vapor Pressure Equation Constant A		A	11.76		Vapor Pressure Equation Constant A		A	11.76		Vapor Pressure Equation Constant A		A	11.63	
Vapor Pressure Equation Constant B		B	5315.06	$^{\circ}R$	Vapor Pressure Equation Constant B		B	5315.06	$^{\circ}R$	Vapor Pressure Equation Constant B		B	5015.72	$^{\circ}R$
Daily total solar insolation on a horizontal surface		I	1904.0	Btu/ft ² -day	Daily total solar insolation on a horizontal surface		I	1685.0	Btu/ft ² -day	Daily total solar insolation on a horizontal surface		I	1320.0	Btu/ft ² -day
Average Daily Ambient Temperature Eq. 1-30					Average Daily Ambient Temperature Eq. 1-30					Average Daily Ambient Temperature Eq. 1-30				
TAA = ((TAX+TAN)/2)		T_{AA}	533.90	$^{\circ}R$	TAA = ((TAX+TAN)/2)		T_{AA}	533.20	$^{\circ}R$	TAA = ((TAX+TAN)/2)		T_{AA}	526.15	$^{\circ}R$
Average daily maximum ambient temperature, Table 7.1-7		T_{AX}	541.10	$^{\circ}R$	Average daily maximum ambient temperature, Table 7.1-7		T_{AX}	540.10	$^{\circ}R$	Average daily maximum ambient temperature, Table 7.1-7		T_{AX}	533.40	$^{\circ}R$
Average daily minimum ambient temperature, Table 7.1-7		T_{AN}	526.70	$^{\circ}R$	Average daily minimum ambient temperature, Table 7.1-7		T_{AN}	526.30	$^{\circ}R$	Average daily minimum ambient temperature, Table 7.1-7		T_{AN}	518.90	$^{\circ}R$
Liquid Bulk Temperature Eq 1-31:					Liquid Bulk Temperature Eq 1-31:					Liquid Bulk Temperature Eq 1-31:				
TB = TAA + 0.003 cs I		T_B	535.33		TB = TAA + 0.003 cs I		T_B	534.46		TB = TAA + 0.003 cs I		T_B	527.14	
Average Daily Liquid Surface Temperature Eq. 1-28					Average Daily Liquid Surface Temperature Eq. 1-28					Average Daily Liquid Surface Temperature Eq. 1-28				
TLA = 0.3*TAA + 0.7*TB + 0.004*α ¹		T_{LA}	536.80	$^{\circ}R$	TLA = 0.3*TAA + 0.7*TB + 0.004*α ¹		T_{LA}	535.77	$^{\circ}R$	TLA = 0.3*TAA + 0.7*TB + 0.004*α ¹		T_{LA}	528.16	$^{\circ}R$
True Vapor Pressure Eq. 1-25:					True Vapor Pressure Eq. 1-25:					True Vapor Pressure Eq. 1-25:				
PVA = exp(A-(B/TLA))		P_{VA}	6.391	psia	PVA = exp(A-(B/TLA))		P_{VA}	6.270	psia	PVA = exp(A-(B/TLA))		P_{VA}	8.462	psia
Vapor pressure function Eq. 2-4:					Vapor pressure function Eq. 2-4:					Vapor pressure function Eq. 2-4:				
$P^* = P_{VA}/P_{VA}(1+(1-(P_{VA}/P_A))^{0.5})^2$		P^*	0.142	NA	$P^* = P_{VA}/P_{VA}(1+(1-(P_{VA}/P_A))^{0.5})^2$		P^*	0.138	NA	$P^* = P_{VA}/P_{VA}(1+(1-(P_{VA}/P_A))^{0.5})^2$		P^*	0.211	NA
Rim Seal Losses Eq. 2-3:					Rim Seal Losses Eq. 2-3:					Rim Seal Losses Eq. 2-3:				
$L_R = ((K_{R1} + K_{R2} \sqrt{DP})^2 M_v K_c) / 12 \text{ months}$		L_R	90.00	lb/month	$L_R = ((K_{R1} + K_{R2} \sqrt{DP})^2 M_v K_c) / 12 \text{ months}$		L_R	87.75	lb/month	$L_R = ((K_{R1} + K_{R2} \sqrt{DP})^2 M_v K_c) / 12 \text{ months}$		L_R	122.27	lb/month
Withdrawal losses Eq. 2-19:					Withdrawal losses Eq. 2-19:					Withdrawal losses Eq. 2-19:				
$L_W = ((0.943)QC_s W_v) / D [1 + (N_e F_e / D)]$		L_W	4.39	lb/month	$L_W = ((0.943)QC_s W_v) / D [1 + (N_e F_e / D)]$		L_W	4.39	lb/month	$L_W = ((0.943)QC_s W_v) / D [1 + (N_e F_e / D)]$		L_W	4.39	lb/month
Deck Fitting Losses Eq.2-13:					Deck Fitting Losses Eq.2-13:					Deck Fitting Losses Eq.2-13:				
$L_F = F_f P^* M_v K_c$		LF	138.61	lb/month	$L_F = F_f P^* M_v K_c$		LF	135.15	lb/month	$L_F = F_f P^* M_v K_c$		LF	188.32	lb/month
Deck Seam Losses Eq. 2-18:					Deck Seam Losses Eq. 2-18:					Deck Seam Losses Eq. 2-18:				
$L_D = K_D S_D^2 P^* M_v K_c / 12 \text{ months}$		LD	0.00	lb/month	$L_D = K_D S_D^2 P^* M_v K_c / 12 \text{ months}$		LD	0.00	lb/month	$L_D = K_D S_D^2 P^* M_v K_c / 12 \text{ months}$		LD	0.00	lb/month
HAPS Speciation					HAPS Speciation					HAPS Speciation				
Product - same as January			Gasoline		Product - same as January			Gasoline		Product - same as January			Gasoline	
Total HAP Monthly Emissions			8.466	lb/month	Total HAP Monthly Emissions			8.215	lb/month	Total HAP Monthly Emissions			7.626	lb/month
Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{vi}L_W$					Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{vi}L_W$					Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{vi}L_W$				
L_{Ti}					L_{Ti}					L_{Ti}				
hexane			1.4654	lb/month	hexane			1.4217	lb/month	hexane			1.3378	lb/month
benzene			1.6895	lb/month	benzene			1.6376	lb/month	benzene			1.5251	lb/month
2,2,4 TMP			2.0307	lb/month	2,2,4 TMP			1.9690	lb/month	2,2,4 TMP			1.8267	lb/month
toluene			2.1781	lb/month	toluene			2.1120	lb/month	toluene			1.9420	lb/month
ethylbenzene			0.1862	lb/month	ethylbenzene			0.1813	lb/month	ethylbenzene			0.1672	lb/month
xylenes			0.8531	lb/month	xylenes			0.8318	lb/month	xylenes			0.7688	lb/month
naphthalene			0.0192	lb/month	naphthalene			0.0192	lb/month	naphthalene			0.0190	lb/month
cumene			0.0434	lb/month	cumene			0.0425	lb/month	cumene			0.0398	lb/month
Vapor Weight Concentrations Eq. 40-6 $Z_{vi} = y_i M_i / M_v$					Vapor Weight Concentrations Eq. 40-6 $Z_{vi} = y_i M_i / M_v$					Vapor Weight Concentrations Eq. 40-6 $Z_{vi} = y_i M_i / M_v$				
M_i		M_v	Z_{vi}		M_i		M_v	Z_{vi}		M_i		M_v	Z_{vi}	
hexane		68	0.00622		hexane		68	0.00618		hexane		62	0.00417	
benzene		68	0.00704		benzene		68	0.00699		benzene		62	0.00466	
2,2,4 TMP		68	0.00811		2,2,4 TMP		68	0.00805		2,2,4 TMP		62	0.00532	
toluene		68	0.00818		toluene		68	0.00810		toluene		62	0.00526	
ethylbenzene		68	0.00055		ethylbenzene		68	0.00054		ethylbenzene		62	0.00034	
xylenes		68	0.00239		xylenes		68	0.00235		xylenes		62	0.00149	
naphthalene		68	0.00000		naphthalene		68	0.00000		naphthalene		62	0.00000	
cumene		68	0.00009		cumene		68	0.00009		cumene		62	0.00006	
Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{VA}$					Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{VA}$					Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{VA}$				
$P_i = P_{VA}(x_i)$		P_{VA}	y_i		$P_i = P_{VA}(x_i)$		P_{VA}	y_i		$P_i = P_{VA}(x_i)$		P_{VA}	y_i	
hexane		6.391	0.00491		hexane		6.270	0.00488		hexane		8.462	0.00300	
benzene		6.391	0.00613		benzene		6.270	0.00609		benzene		8.462	0.00370	
2,2,4 TMP		6.391	0.00483		2,2,4 TMP		6.270	0.00479		2,2,4 TMP		8.462	0.00289	
toluene		6.391	0.00604		toluene		6.270	0.00598		toluene		8.462	0.00354	
ethylbenzene		6.391	0.00035		ethylbenzene		6.270	0.00034		ethylbenzene		8.462	0.00020	
xylenes		6.391	0.00153		xylenes		6.270	0.00151		xylenes		8.462	0.00087	
naphthalene		6.391	0.00000		naphthalene		6.270	0.00000		naphthalene		8.462	0.00000	
cumene		6.391	0.00005		cumene		6.270	0.00005		cumene		8.462	0.00003	
Liquid Mole Fraction Eq. 40-4 $x_i = (Z_{vi} M_i) / M_i$					Liquid Mole Fraction Eq. 40-4 $x_i = (Z_{vi} M_i) / M_i$					Liquid Mole Fraction Eq. 40-4 $x_i = (Z_{vi} M_i) / M_i$				
Z_{vi}		M_i	M_i	x_i	Z_{vi}		M_i	M_i	x_i	Z_{vi}		M_i	M_i	x_i
hexane		92	86.18	0.01068	hexane		92	86.18	0.01068	hexane		92	86.18	0.01068
benzene		92	78.11	0.02120	benzene		92	78.11	0.02120	benzene		92	78.11	0.02120
2,2,4 TMP		92	114.23	0.03222	2,2,4 TMP		92	114.23	0.03222	2,2,4 TMP		92	114.23	0.03222
toluene		92	92.14	0.06989	toluene		92	92.14	0.06989	toluene		92	92.14	0.06989
ethylbenzene		92	106.17	0.01213	ethylbenzene		92	106.17	0.01213	ethylbenzene		92	106.17	0.01213
xylenes		92	106.17	0.06066	xylenes		92	106.17	0.06066	xylenes		92	106.17	0.06066
naphthalene		92	128.17	0.00298	naphthalene		92	128.17	0.00298	naphthalene		92	128.17	0.00298
cumene		92	120.19	0.00383	cumene		92	120.19	0.00383	cumene		92	120.19	0.00383
Component Vapor pressure $P_{VA} = (0.019337)10^4 (A - (B/(TLA+C)))$					Component Vapor pressure $P_{VA} = (0.019337)10^4 (A - (B/(TLA+C)))$					Component Vapor pressure $P_{VA} = (0.019337)10^4 (A - (B/(TLA+C)))$				
A		B	C	P_{VA}	A		B	C	P_{VA}	A		B	C	P_{VA}
hexane		1171.5	224.37	2.9373	hexane		1171.5	224.37	2.8649	hexane		1171.5	224.37	2.3757
benzene		1211	220.79	1.8489	benzene		1211	220.79	1.8004	benzene		1211	220.79	1.4751
2,2,4 TMP		1257.8	220.74	0.9583	2,2,4 TMP		1257.8	220.74	0.9322	2,2,4 TMP		1257.8	220.74	0.7579
toluene		1377.6	222.64	0.5523	toluene		1377.6	222.64	0.5361	toluene		1377.6	222.64	0.4288
ethylbenzene		1419.3	212.61	0.1841	ethylbenzene		1419.3	212.61	0.1781	ethylbenzene		1419.3	212.61	0.1387
xylenes		1462.3	215.11	0.1611	xylenes		1462.3	215.11	0.1558	xylenes		1462.3	215.11	0.1211
naphthalene		1831.6	211.82	0.0050	naphthalene		1831.6	211.82	0.0048	naphthalene		1831.6	211.82	0.0035
cumene		1455.8	207.2	0.0887	cumene		1455.8	207.2	0.0856	cumene		1455.8	207.2	0.0654

MONTH October				MONTH November				MONTH December										
ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units							
Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D + L_{LD}$)		LT	230.52	lb/month	Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D + L_{LD}$)		LT	204.45	lb/month	Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D + L_{LD}$)		LT	159.74	lb/month				
			0.12	tons/month				0.10	tons/month				0.08	tons/month				
Product Type			Gasoline - RVP 13.5		Product Type			Gasoline - RVP 15		Product Type			Gasoline - RVP 15					
Monthly Throughput (only change if actual is known)		Q_{month}	38,792.74	barrels/month	Monthly Throughput (only change if actual is known)		Q_{month}	38,792.74	barrels/month	Monthly Throughput (only change if actual is known)		Q_{month}	38,792.74	barrels/month				
Vapor Molecular weight		M_v	62.00		Vapor Molecular weight		M_v	60.15		Vapor Molecular weight		M_v	60.15					
Vapor Pressure Equation Constant A		A	11.63		Vapor Pressure Equation Constant A		A	11.60		Vapor Pressure Equation Constant A		A	11.60					
Vapor Pressure Equation Constant B		B	5015.72	$^{\circ}R$	Vapor Pressure Equation Constant B		B	4937.93	$^{\circ}R$	Vapor Pressure Equation Constant B		B	4937.93	$^{\circ}R$				
Daily total solar insolation on a horizontal surface		I	948.0	Btu/ft ² -day	Daily total solar insolation on a horizontal surface		I	621.0	Btu/ft ² -day	Daily total solar insolation on a horizontal surface		I	501.0	Btu/ft ² -day				
Average Daily Ambient Temperature Eq. 1-30					Average Daily Ambient Temperature Eq. 1-30					Average Daily Ambient Temperature Eq. 1-30								
TAA = ((TAX+TAN)/2)		T_{AA}	514.75	$^{\circ}R$	TAA = ((TAX+TAN)/2)		T_{AA}	505.35	$^{\circ}R$	TAA = ((TAX+TAN)/2)		T_{AA}	495.50	$^{\circ}R$				
Average daily maximum ambient temperature, Table 7.1-7		T_{AX}	522.40	$^{\circ}R$	Average daily maximum ambient temperature, Table 7.1-7		T_{AX}	512.10	$^{\circ}R$	Average daily maximum ambient temperature, Table 7.1-7		T_{AX}	501.80	$^{\circ}R$				
Average daily minimum ambient temperature, Table 7.1-7		T_{AN}	507.10	$^{\circ}R$	Average daily minimum ambient temperature, Table 7.1-7		T_{AN}	498.60	$^{\circ}R$	Average daily minimum ambient temperature, Table 7.1-7		T_{AN}	489.20	$^{\circ}R$				
Liquid Bulk Temperature Eq 1-31:					Liquid Bulk Temperature Eq 1-31:					Liquid Bulk Temperature Eq 1-31:								
TB = TAA + 0.003 as I		T_B	515.46		TB = TAA + 0.003 as I		T_B	505.82		TB = TAA + 0.003 as I		T_B	495.88					
Average Daily Liquid Surface Temperature Eq. 1-28					Average Daily Liquid Surface Temperature Eq. 1-28					Average Daily Liquid Surface Temperature Eq. 1-28								
TLA = 0.3*TAA + 0.7*TB + 0.004* α 1		T_{LA}	516.20	$^{\circ}R$	TLA = 0.3*TAA + 0.7*TB + 0.004* α 1		T_{LA}	506.30	$^{\circ}R$	TLA = 0.3*TAA + 0.7*TB + 0.004* α 1		T_{LA}	496.26	$^{\circ}R$				
True Vapor Pressure Eq. 1-25:					True Vapor Pressure Eq. 1-25:					True Vapor Pressure Eq. 1-25:								
PVA = exp(A-(B/TLA))		P_{VA}	6.790	psia	PVA = exp(A-(B/TLA))		P_{VA}	6.340	psia	PVA = exp(A-(B/TLA))		P_{VA}	5.205	psia				
Vapor pressure function Eq. 2-4:					Vapor pressure function Eq. 2-4:					Vapor pressure function Eq. 2-4:								
$P^* = P_{VA}/P_A/(1+(1-(P_{VA}/P_A))^{0.5})^2$		P^*	0.154	NA	$P^* = P_{VA}/P_A/(1+(1-(P_{VA}/P_A))^{0.5})^2$		P^*	0.140	NA	$P^* = P_{VA}/P_A/(1+(1-(P_{VA}/P_A))^{0.5})^2$		P^*	0.109	NA				
Rim Seal Losses Eq. 2-3:					Rim Seal Losses Eq. 2-3:					Rim Seal Losses Eq. 2-3:								
$L_R = ((K_{GA} + K_{GB}) \sqrt{DP^* M_v K_c}) / 12$ months		L_R	89.02	lb/month	$L_R = ((K_{GA} + K_{GB}) \sqrt{DP^* M_v K_c}) / 12$ months		L_R	78.76	lb/month	$L_R = ((K_{GA} + K_{GB}) \sqrt{DP^* M_v K_c}) / 12$ months		L_R	61.16	lb/month				
Withdrawal losses Eq. 2-19:					Withdrawal losses Eq. 2-19:					Withdrawal losses Eq. 2-19:								
$L_W = ((0.943)OCsW_j/D)^{1.1} (N_c F_j/D)$		L_W	4.39	lb/month	$L_W = ((0.943)OCsW_j/D)^{1.1} (N_c F_j/D)$		L_W	4.39	lb/month	$L_W = ((0.943)OCsW_j/D)^{1.1} (N_c F_j/D)$		L_W	4.39	lb/month				
Deck Fitting Losses Eq.2-13:					Deck Fitting Losses Eq.2-13:					Deck Fitting Losses Eq.2-13:								
$L_F = F_r P^* M_v K_c$		LF	137.11	lb/month	$L_F = F_r P^* M_v K_c$		LF	121.30	lb/month	$L_F = F_r P^* M_v K_c$		LF	94.19	lb/month				
Deck Seam Losses Eq. 2-18:					Deck Seam Losses Eq. 2-18:					Deck Seam Losses Eq. 2-18:								
$L_D = K_D S_D P^* M_v K_c / 12$ months		LD	0.00	lb/month	$L_D = K_D S_D P^* M_v K_c / 12$ months		LD	0.00	lb/month	$L_D = K_D S_D P^* M_v K_c / 12$ months		LD	0.00	lb/month				
HAPS Speciation				HAPS Speciation				HAPS Speciation										
Product - same as January			Gasoline	Product - same as January			Gasoline	Product - same as January			Gasoline	Product - same as January			Gasoline			
Total HAP Monthly Emissions			5.266	lb/month	Total HAP Monthly Emissions			4.227	lb/month	Total HAP Monthly Emissions			3.226	lb/month				
Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{vi}L_W$					Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{vi}L_W$					Individual HAP Monthly Em Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{vi}L_W$								
	hexane	L_{Ti}	0.9067	lb/month		hexane	0.7164	lb/month		hexane	0.5222	lb/month						
	benzene	L_{Ti}	1.0242	lb/month		benzene	0.8028	lb/month		benzene	0.5841	lb/month						
	2,2,4 TMP	L_{Ti}	1.2410	lb/month		2,2,4 TMP	0.9824	lb/month		2,2,4 TMP	0.7320	lb/month						
	toluene	L_{Ti}	1.3345	lb/month		toluene	1.0675	lb/month		toluene	0.8189	lb/month						
	ethylbenzene	L_{Ti}	0.1250	lb/month		ethylbenzene	0.1066	lb/month		ethylbenzene	0.0906	lb/month						
	xylenes	L_{Ti}	0.5836	lb/month		xylenes	0.5032	lb/month		xylenes	0.4332	lb/month						
	naphthalene	L_{Ti}	0.0186	lb/month		naphthalene	0.0185	lb/month		naphthalene	0.0184	lb/month						
	cumene	L_{Ti}	0.0323	lb/month		cumene	0.0291	lb/month		cumene	0.0264	lb/month						
Vapor Weight Concentrations Eq. 40-6 $Z_{vi} = y_i M_i / M_v$					Vapor Weight Concentrations Eq. 40-6 $Z_{vi} = y_i M_i / M_v$					Vapor Weight Concentration $Z_{vi} = y_i M_i / M_v$								
	hexane	M_i	86.18			hexane	86.18			hexane	86.18							
	benzene	M_i	78.11			benzene	78.11			benzene	78.11							
	2,2,4 TMP	M_i	114.23			2,2,4 TMP	114.23			2,2,4 TMP	114.23							
	toluene	M_i	92.14			toluene	92.14			toluene	92.14							
	ethylbenzene	M_i	106.17			ethylbenzene	106.17			ethylbenzene	106.17							
	xylenes	M_i	106.17			xylenes	106.17			xylenes	106.17							
	naphthalene	M_i	128.17			naphthalene	128.17			naphthalene	128.17							
	cumene	M_i	120.19			cumene	120.19			cumene	120.19							
Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{VA}$					Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{VA}$					Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{VA}$								
	hexane	$P_i = P_{VA}(x_i)$	0.018638	6.790	0.00275		hexane	0.014875	6.340	0.00235		hexane	0.011186	5.205	0.00215			
	benzene	$P_i = P_{VA}(x_i)$	0.022527	6.790	0.00332		benzene	0.017664	6.340	0.00279		benzene	0.013033	5.205	0.00250			
	2,2,4 TMP	$P_i = P_{VA}(x_i)$	0.017363	6.790	0.00256		2,2,4 TMP	0.013463	6.340	0.00212		2,2,4 TMP	0.009817	5.205	0.00189			
	toluene	$P_i = P_{VA}(x_i)$	0.020754	6.790	0.00306		toluene	0.015726	6.340	0.00248		toluene	0.011191	5.205	0.00215			
	ethylbenzene	$P_i = P_{VA}(x_i)$	0.001114	6.790	0.00016		ethylbenzene	0.000811	6.340	0.00013		ethylbenzene	0.000553	5.205	0.00011			
	xylenes	$P_i = P_{VA}(x_i)$	0.004845	6.790	0.00071		xylenes	0.003518	6.340	0.00055		xylenes	0.002391	5.205	0.00046			
	naphthalene	$P_i = P_{VA}(x_i)$	0.000006	6.790	0.00000		naphthalene	0.000004	6.340	0.00000		naphthalene	0.000002	5.205	0.00000			
	cumene	$P_i = P_{VA}(x_i)$	0.000161	6.790	0.00002		cumene	0.000114	6.340	0.00002		cumene	0.000075	5.205	0.00001			
Liquid Mole Fraction Eq. 40-4 $x_i = (Z_{vi} M_i) / M_i$					Liquid Mole Fraction Eq. 40-4 $x_i = (Z_{vi} M_i) / M_i$					Liquid Mole Fraction Eq. 40-4 $x_i = (Z_{vi} M_i) / M_i$								
	hexane	Z_{vi}	0.01	92	0.01068		hexane	0.01	96	0.01114		hexane	0.01	96	0.01114			
	benzene	Z_{vi}	0.018	92	0.02120		benzene	0.018	96	0.02212		benzene	0.018	96	0.02212			
	2,2,4 TMP	Z_{vi}	0.04	92	0.03222		2,2,4 TMP	0.04	96	0.03362		2,2,4 TMP	0.04	96	0.03362			
	toluene	Z_{vi}	0.07	92	0.06989		toluene	0.07	96	0.07293		toluene	0.07	96	0.07293			
	ethylbenzene	Z_{vi}	0.014	92	0.01213		ethylbenzene	0.014	96	0.01266		ethylbenzene	0.014	96	0.01266			
	xylenes	Z_{vi}	0.07	92	0.06066		xylenes	0.07	96	0.06329		xylenes	0.07	96	0.06329			
	naphthalene	Z_{vi}	0.00415	92	0.00298		naphthalene	0.00415	96	0.00311		naphthalene	0.00415	96	0.00311			
	cumene	Z_{vi}	0.005	92	0.00383		cumene	0.005	96	0.00399		cumene	0.005	96	0.00399			
Component Vapor pressure $P_{VA} = (0.019337)10^4(A-(B/(TLA+C)))$					Component Vapor pressure $P_{VA} = (0.019337)10^4(A-(B/(TLA+C)))$					Component Vapor pressure $P_{VA} = (0.019337)10^4(A-(B/(TLA+C)))$								
	hexane	A	6.878	1171.5	224.37	1.7459		hexane	6.878	1171.5	224.37	1.3354		hexane	6.878	1171.5	224.37	1.0042
	benzene	A	6.906	1211	220.79	1.0625		benzene	6.906	1211	220.79	0.7984		benzene	6.906	1211	220.79	0.5891
	2,2,4 TMP	A	6.812	1257.8	220.74	0.5390		2,2,4 TMP	6.812	1257.8	220.74	0.4005		2,2,4 TMP	6.812	1257.8	220.74	0.2920
	toluene	A	7.017	1377.6	222.64	0.2969		toluene	7.017	1377.6	222.64	0.2156		toluene	7.017	1377.6	222.64	0.1534
	ethylbenzene	A	6.95	1419.3	212.61	0.0918		ethylbenzene	6.95	1419.3	212.61	0.0641		ethylbenzene	6.95	1419.3	212.61	0.0436
	xylenes	A	7.009	1462.3	215.11	0.0799		xylenes	7.009	1462.3	215.11	0.0556		xylenes	7.009	1462.3	215.11	0.0378
	naphthalene	A	7.146	1831.6	211.82	0.0020		naphthalene	7.146	1831.6	211.82	0.0013		naphthalene	7.146	1831.6	211.82	0.0008
	cumene	A	6.929	1455.8	207.2	0.0420		cumene	6.929	1455.8	207.2	0.0285		cumene	6.929	1455.8	207.2	0.0188

MONTHLY IFR TANK VOC AND HAP ESTIMATIONS

INPUT DATA				MONTH January				MONTH February				MONTH March			
Tank No.	Symbol	Units		Symbol	Units	Symbol	Units	Symbol	Units	Symbol	Units	Symbol	Units		
30532															
Nearest US Location		Bridgeport, CT		Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D + L_{L_1}$)	LT	166.96	lb/month	Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D + L_{L_1}$)	LT	175.73	lb/month	Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D + L_{L_1}$)	LT	208.99	lb/month
Absolute Pressure	P_A	14.69	psi	Product Type		Gasoline - RVP 15		Product Type		Gasoline - RVP 15		Product Type		Gasoline - RVP 15	
Product Information				Monthly Throughput (only change if actual is known)	Q_{month}	79,287.24	barrels/month	Monthly Throughput (only change if actual is known)	Q_{month}	79,287.24	barrels/month	Monthly Throughput (only change if actual is known)	Q_{month}	79,287.24	barrels/month
Average organic liquid density	W_L	5.60	lb/gal	Vapor Molecular weight	M_v	60.15		Vapor Molecular weight	M_v	60.15		Vapor Molecular weight	M_v	60.15	
Average Reid Vapor Pressure	RVP	13.00		Vapor Pressure Equation Constant A	A	11.60		Vapor Pressure Equation Constant A	A	11.60		Vapor Pressure Equation Constant A	A	11.60	
Product factor, 0.4 for crude oils or 1 for other organic liquids	K_c	1.00		Vapor Pressure Equation Constant B	B	4937.93	$^{\circ}R$	Vapor Pressure Equation Constant B	B	4937.93	$^{\circ}R$	Vapor Pressure Equation Constant B	B	4937.93	$^{\circ}R$
Tank design data				Daily total solar insolation on a horizontal surface	I	560.0	Btu/ft ² -day	Daily total solar insolation on a horizontal surface	I	847.0	Btu/ft ² -day	Daily total solar insolation on a horizontal surface	I	1156.0	Btu/ft ² -day
Shell height	Hs	48.00	ft	Average Daily Ambient Temperature Eq. 1-30				Average Daily Ambient Temperature Eq. 1-30				Average Daily Ambient Temperature Eq. 1-30			
Diameter	D	100.00	ft	$T_{AA} = ((TAX+TAN)/2)$	T_{AA}	490.50	$^{\circ}R$	$T_{AA} = ((TAX+TAN)/2)$	T_{AA}	492.20	$^{\circ}R$	$T_{AA} = ((TAX+TAN)/2)$	T_{AA}	498.90	$^{\circ}R$
Throughput	Q	3,330,064	gal/month	Average daily maximum ambient temperature, Table 7.1-7	T_{AX}	496.90	$^{\circ}R$	Average daily maximum ambient temperature, Table 7.1-7	T_{AX}	498.80	$^{\circ}R$	Average daily maximum ambient temperature, Table 7.1-7	T_{AX}	506.00	$^{\circ}R$
Maximum Filling Height (use Hs-1 if unknown)	H_{LX}	47.00	ft	Average daily minimum ambient temperature, Table 7.1-7	T_{AN}	484.10	$^{\circ}R$	Average daily minimum ambient temperature, Table 7.1-7	T_{AN}	485.60	$^{\circ}R$	Average daily minimum ambient temperature, Table 7.1-7	T_{AN}	491.80	$^{\circ}R$
Minimum Filling Height (use Hs-1 if unknown)	H_{LX}	1.00	ft	Liquid Bulk Temperature Eq. 1-31:				Liquid Bulk Temperature Eq. 1-31:				Liquid Bulk Temperature Eq. 1-31:			
Liquid height (assume 1/2 Hs)	H_L	24.00	ft	$T_B = T_{AA} + 0.003 \text{ as } I$	T_B	490.92		$T_B = T_{AA} + 0.003 \text{ as } I$	T_B	492.84		$T_B = T_{AA} + 0.003 \text{ as } I$	T_B	499.77	
Tank Construction (pick from drop down list)		Welded		Average Daily Liquid Surface Temperature Eq. 2-6				Average Daily Liquid Surface Temperature Eq. 1-28				Average Daily Liquid Surface Temperature Eq. 1-28			
Tank Color (pick from drop down list)		White		$T_{LA} = 0.3T_{AA} + 0.7T_B + 0.004 \alpha I$	T_{LA}	491.35	$^{\circ}R$	$T_{LA} = 0.3T_{AA} + 0.7T_B + 0.004 \alpha I$	T_{LA}	493.49	$^{\circ}R$	$T_{LA} = 0.3T_{AA} + 0.7T_B + 0.004 \alpha I$	T_{LA}	500.66	$^{\circ}R$
Tank Shell Condition (pick from drop down list)		Average		True Vapor Pressure Eq. 1-25:				True Vapor Pressure Eq. 1-25:				True Vapor Pressure Eq. 1-25:			
Tank Interior Condition (pick from drop down list)		Light Rust		$P_{VA} = \exp(A - (B/T_{LA}))$	P_{VA}	4.713	psia	$P_{VA} = \exp(A - (B/T_{LA}))$	P_{VA}	4.922	psia	$P_{VA} = \exp(A - (B/T_{LA}))$	P_{VA}	5.681	psia
Tank paint solar absorptance, dimensionless, Table 7.1-6	α	0.25		Vapor pressure function Eq. 2-4:				Vapor pressure function Eq. 2-4:				Vapor pressure function Eq. 2-4:			
				$P^* = P_{VA}/P_A / (1 + (1 - (P_{VA}/P_A))^{0.5})^2$	P^*	0.096	NA	$P^* = P_{VA}/P_A / (1 + (1 - (P_{VA}/P_A))^{0.5})^2$	P^*	0.102	NA	$P^* = P_{VA}/P_A / (1 + (1 - (P_{VA}/P_A))^{0.5})^2$	P^*	0.122	NA
Internal floating roof design data				Rim Seal Losses Eq. 2-3:				Rim Seal Losses Eq. 2-3:				Rim Seal Losses Eq. 2-3:			
Rim Seal Type:		Mechanical-shoe seal		$L_R = ((K_{S1} + K_{S2}) \sqrt{DP}^* M_v K_c) / 12 \text{ months}$	L_R	77.32	lb/month	$L_R = ((K_{S1} + K_{S2}) \sqrt{DP}^* M_v K_c) / 12 \text{ months}$	L_R	81.54	lb/month	$L_R = ((K_{S1} + K_{S2}) \sqrt{DP}^* M_v K_c) / 12 \text{ months}$	L_R	97.54	lb/month
Rim Seal Fit (Average or Tight fitting)		Average		Withdrawal losses Eq. 2-19:				Withdrawal losses Eq. 2-19:				Withdrawal losses Eq. 2-19:			
Number of fixed roof support columns	Nc	0.00	NA	$L_W = (((0.943)OCsW_v) / D) [1 + (N_F/D)]$	L_W	6.28	lb/month	$L_W = (((0.943)OCsW_v) / D) [1 + (N_F/D)]$	L_W	6.28	lb/month	$L_W = (((0.943)OCsW_v) / D) [1 + (N_F/D)]$	L_W	6.28	lb/month
Effective column diameter (1.1 for 8x7 in. built up columns; 0.7 for 8 in. pipe columns; 1.0 for 8 in. pipe columns)	Fc	1.00	ft	Deck Fitting Losses Eq. 2-13:				Deck Fitting Losses Eq. 2-13:				Deck Fitting Losses Eq. 2-13:			
Deck seam loss per unit seam length factor, 0.0 or 0.14	KD	0.00	lb-mole/ft-yr	$L_F = F_F P^* M_v K_c$	LF	83.36	lb/month	$L_F = F_F P^* M_v K_c$	LF	87.91	lb/month	$L_F = F_F P^* M_v K_c$	LF	105.16	lb/month
Zero wind speed LR factor, see Table 7.1-8	KRa	1.6	lb-mole/ft-yr	Deck Seam Losses Eq. 2-18:				Deck Seam Losses Eq. 2-18:				Deck Seam Losses Eq. 2-18:			
Wind speed dependent LR factor, see Table 7.1-8	KRb	0.3	lb-mole/(mph) ^{1.75} ft-yr	$L_{L_1} = K_{S1} D^2 P^* M_v K_c / 12 \text{ months}$	LD	0.00	lb/month	$L_{L_1} = K_{S1} D^2 P^* M_v K_c / 12 \text{ months}$	LD	0.00	lb/month	$L_{L_1} = K_{S1} D^2 P^* M_v K_c / 12 \text{ months}$	LD	0.00	lb/month
Average ambient wind speed at tank site, for IFR use Zero	v	0.0	mph	HAPS Speciation				HAPS Speciation				HAPS Speciation			
Seal-related wind speed exponent, see Table 7.1-8	n	1.6	NA	Product - select from list		Gasoline		Product - same as January		Gasoline		Product - same as January		Gasoline	
Shell clingage factor, see Table 7.1-10	Cs	0.0015	bb/1,000 ft ²	Total HAP Monthly Emissions		3.602	lb/month	Total HAP Monthly Emissions		3.782	lb/month	Total HAP Monthly Emissions		4.496	lb/month
Deck Design Data				Individual HAP Monthly Emissions Eq. 40-2 $L_{T1} = Z_{L1}(L_R + L_F + L_D) + Z_{L1}L_W$				Individual HAP Monthly Emissions Eq. 40-2 $L_{T1} = Z_{L1}(L_R + L_F + L_D) + Z_{L1}L_W$				Individual HAP Monthly Emissions Eq. 40-2 $L_{T1} = Z_{L1}(L_R + L_F + L_D) + Z_{L1}L_W$			
Deck Seam (choose Welded or Bolted)		Welded		hexane	0.5357	lb/month		hexane	0.5715	lb/month		hexane	0.7119	lb/month	
Deck construction type not required for welded seams		NA		benzene	0.6076	lb/month		benzene	0.6473	lb/month		benzene	0.8044	lb/month	
If bolted continuous sheet or panel, enter width		0		TMP	0.7927	lb/month		TMP	0.8377	lb/month		2,2,4 TMP	1.0167	lb/month	
If bolted panel, also enter length		0		toluene	0.9314	lb/month		toluene	0.9752	lb/month		toluene	1.1512	lb/month	
Deck seam length factor: Length of Seam / Area of Deck	SD	NA	ft/ft ²	ethylbenzene	0.1153	lb/month		ethylbenzene	0.1180	lb/month		ethylbenzene	0.1292	lb/month	
Deck Fitting Data				xylenes	0.5579	lb/month		xylenes	0.5697	lb/month		xylenes	0.6184	lb/month	
Access Hatch Bolted cover, gasketed	Qty	5	1.6	naphthalene	0.0262	lb/month		naphthalene	0.0262	lb/month		naphthalene	0.0263	lb/month	
Column Well Bolted cover, gasketed sliding cover	0	33.0		cumene	0.0356	lb/month		cumene	0.0360	lb/month		cumene	0.0378	lb/month	
Unslotted Guidepole and Well Gasketed sliding cover w/pole sleeve	0	8.6		Vapor Weight Concentrations Eq. 40-4 $Z_{vi} = y_i M_i / M_v$				Vapor Weight Concentrations Eq. 40-4 $Z_{vi} = y_i M_i / M_v$				Vapor Weight Concentrations Eq. 40-4 $Z_{vi} = y_i M_i / M_v$			
Slotted guidepole/sample well Gasketed sliding cover, with pole sleeve	0	11.0		hexane	86.18	60	0.00294	hexane	86.18	60	0.00300	hexane	86.18	60	0.00320
Gauge-float well (automatic g) Bolted cover, gasketed	0	2.8		benzene	78.11	60	0.00308	benzene	78.11	60	0.00315	benzene	78.11	60	0.00341
Gauge-hatch/sample port Slit fabric seal, 10% open area	2	12.0		2,2,4 TMP	114.23	60	0.00337	2,2,4 TMP	114.23	60	0.00346	2,2,4 TMP	114.23	60	0.00378
Vacuum Breaker Weighted mechanical actuation, gasketed	1	6.2		toluene	92.14	60	0.00306	toluene	92.14	60	0.00316	toluene	92.14	60	0.00351
Deck drain Stub drain (1-inch diameter)	0	1.2		ethylbenzene	106.17	60	0.00017	ethylbenzene	106.17	60	0.00018	ethylbenzene	106.17	60	0.00020
Legs (IFR type) IFR type, Adjustable	17	7.9		xylenes	106.17	60	0.00074	xylenes	106.17	60	0.00077	xylenes	106.17	60	0.00088
Rim Vent Weighted mechanical actuation, gasketed	0	0.7		naphthalene	128.17	60	0.00000	naphthalene	128.17	60	0.00000	naphthalene	128.17	60	0.00000
Ladder Sliding cover, gasketed	0	56.0		cumene	120.19	60	0.00003	cumene	120.19	60	0.00003	cumene	120.19	60	0.00003
Ladder / Guide-Pole Combin' Ladder sleeve, gasketed sliding cover	0	60.0		Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{VA}$				Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{VA}$				Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{VA}$			
Monthly deck fitting loss factor F_F		14.38	per month	hexane	0.009680	4.713	0.00205	hexane	0.010314	4.922	0.00210	hexane	0.012697	5.681	0.00224
				benzene	0.011169	4.713	0.00237	benzene	0.011919	4.922	0.00243	benzene	0.014919	5.681	0.00263
				2,2,4 TMP	0.008362	4.713	0.00177	2,2,4 TMP	0.008971	4.922	0.00182	2,2,4 TMP	0.011297	5.681	0.00199
				toluene	0.009416	4.713	0.00200	toluene	0.010156	4.922	0.00206	toluene	0.013018	5.681	0.00229
				ethylbenzene	0.000455	4.713	0.00010	ethylbenzene	0.000495	4.922	0.00010	ethylbenzene	0.000655	5.681	0.00012
				xylenes	0.001965	4.713	0.00042	xylenes	0.002141	4.922	0.00044	xylenes	0.002839	5.681	0.00050
				naphthalene	0.000002	4.713	0.00000	naphthalene	0.000002	4.922	0.00000	naphthalene	0.000003	5.681	0.00000
				cumene	0.000061	4.713	0.00001	cumene	0.000067	4.922	0.00001	cumene	0.000090	5.681	0.00002
				Liquid Mole Fraction Eq. 40-4 $X_i = (Z_{Li} M_i) / M_L$				Liquid Mole Fraction Eq. 40-4 $X_i = (Z_{Li} M_i) / M_L$				Liquid Mole Fraction Eq. 40-4 $X_i = (Z_{Li} M_i) / M_L$			
				hexane	0.01	96	0.01114	hexane	0.01	96	0.01114	hexane	0.01	96	0.01114
				benzene	0.018	96	0.02212	benzene	0.018	96	0.02212	benzene	0.018	96	0.02212
				2,2,4 TMP	0.04	96	0.03362	2,2,4 TMP	0.04	96	0.03362	2,2,4 TMP	0.04	96	0.03362
				toluene	0.07	96	0.07293	toluene	0.07	96	0.07293	toluene	0.07	96	0.07293
				ethylbenzene	0.014	96	0.01266	ethylbenzene	0.014	96	0.01266	ethylbenzene	0.014	96	0.01266
				xylenes	0.07	96	0.06329	xylenes	0.07	96	0.06329	xylenes	0.07	96	0.06329
				naphthalene	0.00415	96	0.00311	naphthalene	0.00415	96	0.00311	naphthalene	0.00415	96	0.00311
				cumene	0.005	96	0.00399	cumene	0.005	96	0.00399	cumene	0.005	96	0.00399
				Component Vapor pressure $P_{VA} = (0.019337) 10^4 (A - (B/(TLA+C)))$				Component Vapor pressure $P_{VA} = (0.019337) 10^4 (A - (B/(TLA+C)))$				Component Vapor pressure $P_{VA} = (0.019337) 10^4 (A - (B/(TLA+C)))$			
				hexane	6.878	1171.5	224.37	hexane	6.878	1171.5	224.37	hexane	6.878	1171.5	224.37
				benzene	6.906	1211	220.79	benzene	6.906	1211	220.79	benzene	6.906	1211	220.79
				2,2,4 TMP	6.812	1257.8	220.74	2,2,4 TMP	6.812	1257.8	220.74	2,2,4 TMP	6.812	1257.8	220.74

MONTH April				MONTH May				MONTH June			
ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units
Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_F + L_D$)		LT	240.35 lb/month	Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_F + L_D$)		LT	190.29 lb/month	Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_F + L_D$)		LT	240.76 lb/month
			0.12 tons/month				0.10 tons/month				0.12 tons/month
Product Type		Gasoline - RVP 13.5		Product Type		Gasoline - RVP 9		Product Type		Gasoline - RVP 9	
Monthly Throughput (only change if actual is known)		Q_{month}	79,287.24 barrels/month	Monthly Throughput (only change if actual is known)		Q_{month}	79,287.24 barrels/month	Monthly Throughput (only change if actual is known)		Q_{month}	79,287.24 barrels/month
Vapor Molecular weight		M_v	62.00	Vapor Molecular weight		M_v	68.00	Vapor Molecular weight		M_v	68.00
Vapor Pressure Equation Constant A		A	11.63	Vapor Pressure Equation Constant A		A	11.76	Vapor Pressure Equation Constant A		A	11.76
Vapor Pressure Equation Constant B		B	5015.72 °R	Vapor Pressure Equation Constant B		B	5315.06 °R	Vapor Pressure Equation Constant B		B	5315.06 °R
Daily total solar insolation on a horizontal surface		I	1490.0 Btu/ft ² -day	Daily total solar insolation on a horizontal surface		I	1750.0 Btu/ft ² -day	Daily total solar insolation on a horizontal surface		I	1862.0 Btu/ft ² -day
Average Daily Ambient Temperature Eq. 1-30				Average Daily Ambient Temperature Eq. 1-30				Average Daily Ambient Temperature Eq. 1-30			
TAA = ((TAX+TAN)/2)		T_{AA}	509.15 °R	TAA = ((TAX+TAN)/2)		T_{AA}	518.65 °R	TAA = ((TAX+TAN)/2)		T_{AA}	528.60 °R
Average daily maximum ambient temperature, Table 7.1		T_{AX}	516.80 °R	Average daily maximum ambient temperature, Table 7.1-7		T_{AX}	526.50 °R	Average daily maximum ambient temperature, Table 7.1-7		T_{AX}	536.10 °R
Average daily minimum ambient temperature, Table 7.1		T_{AN}	501.50 °R	Average daily minimum ambient temperature, Table 7.1-7		T_{AN}	510.80 °R	Average daily minimum ambient temperature, Table 7.1-7		T_{AN}	521.10 °R
Liquid Bulk Temperature Eq. 1-31:				Liquid Bulk Temperature Eq. 1-31:				Liquid Bulk Temperature Eq. 1-31:			
TB = TAA + 0.003 cs I		T_B	510.27	TB = TAA + 0.003 cs I		T_B	519.96	TB = TAA + 0.003 cs I		T_B	530.00
Average Daily Liquid Surface Temperature Eq. 1-28				Average Daily Liquid Surface Temperature Eq. 1-28				Average Daily Liquid Surface Temperature Eq. 1-28			
TLA = 0.3*TAA + 0.7*TB + 0.004*α ¹		T_{LA}	511.42 °R	TLA = 0.3*TAA + 0.7*TB + 0.004*α ¹		T_{LA}	521.32 °R	TLA = 0.3*TAA + 0.7*TB + 0.004*α ¹		T_{LA}	531.44 °R
True Vapor Pressure Eq. 1-25:				True Vapor Pressure Eq. 1-25:				True Vapor Pressure Eq. 1-25:			
PvA = exp(A-(B/TLA))		P_{vA}	6.201 psia	PvA = exp(A-(B/TLA))		P_{vA}	4.763 psia	PvA = exp(A-(B/TLA))		P_{vA}	5.783 psia
Vapor pressure function Eq. 2-4:				Vapor pressure function Eq. 2-4:				Vapor pressure function Eq. 2-4:			
$P^* = P_{vA}/P_A/(1+(1-(P_{vA}/P_A))^{0.5})^2$		P^*	0.136 NA	$P^* = P_{vA}/P_A/(1+(1-(P_{vA}/P_A))^{0.5})^2$		P^*	0.098 NA	$P^* = P_{vA}/P_A/(1+(1-(P_{vA}/P_A))^{0.5})^2$		P^*	0.124 NA
Rim Seal Losses Eq. 2-3:				Rim Seal Losses Eq. 2-3:				Rim Seal Losses Eq. 2-3:			
$L_R = ((K_{R3} + K_{R5} \sqrt{V})/DP^* M_v K_c)/12$ months		L_R	112.64 lb/month	$L_R = ((K_{R3} + K_{R5} \sqrt{V})/DP^* M_v K_c)/12$ months		L_R	88.54 lb/month	$L_R = ((K_{R3} + K_{R5} \sqrt{V})/DP^* M_v K_c)/12$ months		L_R	112.83 lb/month
Withdrawal losses Eq. 2-19:				Withdrawal losses Eq. 2-19:				Withdrawal losses Eq. 2-19:			
$L_W = (((0.943)QC(W)/D)^2(1+(N_c F_w/D)))$		L_W	6.28 lb/month	$L_W = (((0.943)QC(W)/D)^2(1+(N_c F_w/D)))$		L_W	6.28 lb/month	$L_W = (((0.943)QC(W)/D)^2(1+(N_c F_w/D)))$		L_W	6.28 lb/month
Deck Fitting Losses Eq. 2-13:				Deck Fitting Losses Eq. 2-13:				Deck Fitting Losses Eq. 2-13:			
$L_F = F_r P^* M_v K_c$		LF	121.43 lb/month	$L_F = F_r P^* M_v K_c$		LF	95.46 lb/month	$L_F = F_r P^* M_v K_c$		LF	121.64 lb/month
Deck Seam Losses Eq. 2-18:				Deck Seam Losses Eq. 2-18:				Deck Seam Losses Eq. 2-18:			
$L_D = K_D S_D P^* M_v K_c/12$ months		LD	0.00 lb/month	$L_D = K_D S_D P^* M_v K_c/12$ months		LD	0.00 lb/month	$L_D = K_D S_D P^* M_v K_c/12$ months		LD	0.00 lb/month
HAPS Speciation				HAPS Speciation				HAPS Speciation			
Product - same as January			Gasoline	Product - same as January			Gasoline	Product - same as January			Gasoline
Total HAP Monthly Emissions			5.629 lb/month	Total HAP Monthly Emissions			6.674 lb/month	Total HAP Monthly Emissions			8.746 lb/month
Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{Li}L_W$				Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{Li}L_W$				Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{Li}L_W$			
hexane		L_{Ti}	0.9234 lb/month	hexane		L_{Ti}	1.1062 lb/month	hexane		L_{Ti}	1.4765 lb/month
benzene			1.0480 lb/month	benzene			1.2661 lb/month	benzene			1.7014 lb/month
2,2,4 TMP			1.2995 lb/month	2,2,4 TMP			1.5682 lb/month	2,2,4 TMP			2.0708 lb/month
toluene			1.4392 lb/month	toluene			1.7143 lb/month	toluene			2.2540 lb/month
ethylbenzene			0.1486 lb/month	ethylbenzene			0.1683 lb/month	ethylbenzene			0.2066 lb/month
xylenes			0.7031 lb/month	xylenes			0.7898 lb/month	xylenes			0.9584 lb/month
naphthalene			0.0264 lb/month	naphthalene			0.0266 lb/month	naphthalene			0.0270 lb/month
cumene			0.0412 lb/month	cumene			0.0447 lb/month	cumene			0.0516 lb/month
Vapor Weight Concentrations Eq. 40-4 $Z_{vi} = y_i M_i / M_v$				Vapor Weight Concentrations Eq. 40-4 $Z_{vi} = y_i M_i / M_v$				Vapor Weight Concentrations Eq. 40-4 $Z_{vi} = y_i M_i / M_v$			
hexane		M_i	86.18	hexane		M_i	86.18	hexane		M_i	86.18
benzene		M_v	62	benzene		M_v	68	benzene		M_v	68
2,2,4 TMP		Z_{vi}	0.00368	2,2,4 TMP		Z_{vi}	0.00567	2,2,4 TMP		Z_{vi}	0.00603
toluene			0.00399	toluene			0.00627	toluene			0.00677
ethylbenzene			0.00448	ethylbenzene			0.00710	ethylbenzene			0.00776
xylenes			0.00427	xylenes			0.00693	xylenes			0.00774
naphthalene			0.00026	naphthalene			0.00044	naphthalene			0.00051
cumene			0.00113	cumene			0.00190	cumene			0.00221
			0.00000				0.00000				0.00000
			0.00004				0.00007				0.00009
Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{vA}$				Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{vA}$				Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{vA}$			
hexane		$P_i = P_{vA}(x_i)$	6.201	hexane		$P_i = P_{vA}(x_i)$	4.763	hexane		$P_i = P_{vA}(x_i)$	5.783
benzene		P_{vA}	0.00265	benzene		P_{vA}	0.00447	benzene		P_{vA}	0.00476
2,2,4 TMP			0.00317	2,2,4 TMP			0.00546	2,2,4 TMP			0.00590
toluene			0.00243	toluene			0.00423	toluene			0.00462
ethylbenzene			0.00287	ethylbenzene			0.00511	ethylbenzene			0.00571
xylenes			0.00015	xylenes			0.00028	xylenes			0.00032
naphthalene			0.00066	naphthalene			0.00122	naphthalene			0.00142
cumene			0.00000	cumene			0.00000	cumene			0.00000
			0.00002				0.00004				0.00005
Liquid Mole Fraction Eq. 40-4 $x_i = (Z_{Li} M_i) / M_i$				Liquid Mole Fraction Eq. 40-4 $x_i = (Z_{Li} M_i) / M_i$				Liquid Mole Fraction Eq. 40-4 $x_i = (Z_{Li} M_i) / M_i$			
hexane		Z_{Li}	0.01	hexane		Z_{Li}	0.01	hexane		Z_{Li}	0.01
benzene		M_i	86.18	benzene		M_i	86.18	benzene		M_i	86.18
2,2,4 TMP		M_v	62	2,2,4 TMP		M_v	68	2,2,4 TMP		M_v	68
toluene		X_i	0.01068	toluene		X_i	0.01068	toluene		X_i	0.01068
ethylbenzene			0.02120	ethylbenzene			0.02120	ethylbenzene			0.02120
xylenes			0.03222	xylenes			0.03222	xylenes			0.03222
naphthalene			0.06989	naphthalene			0.06989	naphthalene			0.06989
cumene			0.01213	cumene			0.01213	cumene			0.01213
			0.06066				0.06066				0.06066
			0.00298				0.00298				0.00298
			0.00383				0.00383				0.00383
Component Vapor pressure $P_{vA} = (0.019337)10^4(A-(B/(TLA+C)))$				Component Vapor pressure $P_{vA} = (0.019337)10^4(A-(B/(TLA+C)))$				Component Vapor pressure $P_{vA} = (0.019337)10^4(A-(B/(TLA+C)))$			
hexane		A	6.878	hexane		A	6.878	hexane		A	6.878
benzene		B	1171.5	benzene		B	1171.5	benzene		B	1171.5
2,2,4 TMP		C	224.37	2,2,4 TMP		C	224.37	2,2,4 TMP		C	224.37
toluene		P_{vA}	1.5366	toluene		P_{vA}	1.9962	toluene		P_{vA}	2.5773
ethylbenzene			0.9273	ethylbenzene			1.2255	ethylbenzene			1.6087
xylenes			0.4679	xylenes			0.6251	xylenes			0.8293
naphthalene			0.2550	naphthalene			0.3484	naphthalene			0.4725
cumene			0.0773	cumene			0.1098	cumene			0.1546
			0.0672				0.0957				0.1351
			0.0016				0.0026				0.0040
			0.0349				0.0509				0.0735

MONTH July				MONTH August				MONTH September			
ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units
Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D + L_S$)		LT	273.46 lb/month	Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D + L_S$)		LT	266.78 lb/month	Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D + L_S$)		LT	369.28 lb/month
			0.14 tons/month				0.13 tons/month				0.18 tons/month
Product Type			Gasoline - RVP 9	Product Type			Gasoline - RVP 9	Product Type			Gasoline - RVP 13.5
Monthly Throughput (only change if actual is known)		Q_{month}	79,287.24 barrels/month	Monthly Throughput (only change if actual is known)		Q_{month}	79,287.24 barrels/month	Monthly Throughput (only change if actual is known)		Q_{month}	79,287.24 barrels/month
Vapor Molecular weight		M_v	68.00	Vapor Molecular weight		M_v	68.00	Vapor Molecular weight		M_v	62.00
Vapor Pressure Equation Constant A		A	11.76	Vapor Pressure Equation Constant A		A	11.76	Vapor Pressure Equation Constant A		A	11.63
Vapor Pressure Equation Constant B		B	5315.06	Vapor Pressure Equation Constant B		B	5315.06	Vapor Pressure Equation Constant B		B	5015.72
Daily total solar insolation on a horizontal surface		I	1904.0 Btu/ft ² -day	Daily total solar insolation on a horizontal surface		I	1685.0 Btu/ft ² -day	Daily total solar insolation on a horizontal surface		I	1320.0 Btu/ft ² -day
Average Daily Ambient Temperature Eq. 1-30				Average Daily Ambient Temperature Eq. 1-30				Average Daily Ambient Temperature Eq. 1-30			
TAA = ((TAX+TAN)/2)		T_{AA}	533.90 °R	TAA = ((TAX+TAN)/2)		T_{AA}	533.20 °R	TAA = ((TAX+TAN)/2)		T_{AA}	526.15 °R
Average daily maximum ambient temperature, Table 7.1-7		T_{AX}	541.10 °R	Average daily maximum ambient temperature, Table 7.1-7		T_{AX}	540.10 °R	Average daily maximum ambient temperature, Table 7.1-7		T_{AX}	533.40 °R
Average daily minimum ambient temperature, Table 7.1-7		T_{AN}	526.70 °R	Average daily minimum ambient temperature, Table 7.1-7		T_{AN}	526.30 °R	Average daily minimum ambient temperature, Table 7.1-7		T_{AN}	518.90 °R
Liquid Bulk Temperature Eq. 1-31:				Liquid Bulk Temperature Eq. 1-31:				Liquid Bulk Temperature Eq. 1-31:			
TB = TAA + 0.003 as I		T_B	535.33	TB = TAA + 0.003 as I		T_B	534.46	TB = TAA + 0.003 as I		T_B	527.14
Average Daily Liquid Surface Temperature Eq. 1-28				Average Daily Liquid Surface Temperature Eq. 1-28				Average Daily Liquid Surface Temperature Eq. 1-28			
TLA = 0.3TAA + 0.7TB + 0.004αI		T_{LA}	536.80 °R	TLA = 0.3TAA + 0.7TB + 0.004αI		T_{LA}	535.77 °R	TLA = 0.3TAA + 0.7TB + 0.004αI		T_{LA}	528.16 °R
True Vapor Pressure Eq. 1-25:				True Vapor Pressure Eq. 1-25:				True Vapor Pressure Eq. 1-25:			
PvA = exp(A-(B/TLA))		P_{vA}	6.391 psia	PvA = exp(A-(B/TLA))		P_{vA}	6.270 psia	PvA = exp(A-(B/TLA))		P_{vA}	8.462 psia
Vapor pressure function Eq. 2-4:				Vapor pressure function Eq. 2-4:				Vapor pressure function Eq. 2-4:			
$P^* = P_{vA}/P_A(1+(1-(P_{vA}/P_A))^{0.5})^2$		P^*	0.142 NA	$P^* = P_{vA}/P_A(1+(1-(P_{vA}/P_A))^{0.5})^2$		P^*	0.138 NA	$P^* = P_{vA}/P_A(1+(1-(P_{vA}/P_A))^{0.5})^2$		P^*	0.211 NA
Rim Seal Losses Eq. 2-3:				Rim Seal Losses Eq. 2-3:				Rim Seal Losses Eq. 2-3:			
$L_R = ((K_{S1} + K_{S2} \sqrt{V})/DP^* M_v K_c)/12$ months		L_R	128.57 lb/month	$L_R = ((K_{S1} + K_{S2} \sqrt{V})/DP^* M_v K_c)/12$ months		L_R	125.35 lb/month	$L_R = ((K_{S1} + K_{S2} \sqrt{V})/DP^* M_v K_c)/12$ months		L_R	174.68 lb/month
Withdrawal losses Eq. 2-19:				Withdrawal losses Eq. 2-19:				Withdrawal losses Eq. 2-19:			
$L_W = ((0.943/QCsw)/D)^{0.75} [1+(N_e F_w/D)]$		L_W	6.28 lb/month	$L_W = ((0.943/QCsw)/D)^{0.75} [1+(N_e F_w/D)]$		L_W	6.28 lb/month	$L_W = ((0.943/QCsw)/D)^{0.75} [1+(N_e F_w/D)]$		L_W	6.28 lb/month
Deck Fitting Losses Eq.2-13:				Deck Fitting Losses Eq.2-13:				Deck Fitting Losses Eq.2-13:			
$L_F = F_f P^* M_v K_c$		LF	138.61 lb/month	$L_F = F_f P^* M_v K_c$		LF	135.15 lb/month	$L_F = F_f P^* M_v K_c$		LF	188.32 lb/month
Deck Seam Losses Eq. 2-18:				Deck Seam Losses Eq. 2-18:				Deck Seam Losses Eq. 2-18:			
$L_D = K_D S_D P^* M_v K_c/12$ months		LD	0.00 lb/month	$L_D = K_D S_D P^* M_v K_c/12$ months		LD	0.00 lb/month	$L_D = K_D S_D P^* M_v K_c/12$ months		LD	0.00 lb/month
HAPS Speciation				HAPS Speciation				HAPS Speciation			
Product - same as January			Gasoline	Product - same as January			Gasoline	Product - same as January			Gasoline
Total HAP Monthly Emissions			10.160 lb/month	Total HAP Monthly Emissions			9.867 lb/month	Total HAP Monthly Emissions			9.179 lb/month
Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{vi}L_W$				Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{vi}L_W$				Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{vi}L_W$			
hexane		L_{Ti}	1.7241 lb/month	hexane		L_{Ti}	1.6731 lb/month	hexane		L_{Ti}	1.5750 lb/month
benzene			1.9953 lb/month	benzene			1.9346 lb/month	benzene			1.8032 lb/month
2,2,4 TMP			2.4193 lb/month	2,2,4 TMP			2.3472 lb/month	2,2,4 TMP			2.1809 lb/month
toluene			2.6261 lb/month	toluene			2.5488 lb/month	toluene			2.3502 lb/month
ethylbenzene			0.2337 lb/month	ethylbenzene			0.2280 lb/month	ethylbenzene			0.2115 lb/month
xylenes			1.0775 lb/month	xylenes			1.0526 lb/month	xylenes			0.9790 lb/month
naphthalene			0.0272 lb/month	naphthalene			0.0272 lb/month	naphthalene			0.0270 lb/month
cumene			0.0565 lb/month	cumene			0.0554 lb/month	cumene			0.0522 lb/month
Vapor Weight Concentrations Eq. 40-5 $Z_{vi} = y_i M_i / M_v$				Vapor Weight Concentrations Eq. 40-5 $Z_{vi} = y_i M_i / M_v$				Vapor Weight Concentrations Eq. 40-5 $Z_{vi} = y_i M_i / M_v$			
hexane		Z_{vi}	0.00622	hexane		Z_{vi}	0.00618	hexane		Z_{vi}	0.00417
benzene			0.00704	benzene			0.00699	benzene			0.00466
2,2,4 TMP			0.00811	2,2,4 TMP			0.00805	2,2,4 TMP			0.00532
toluene			0.00818	toluene			0.00810	toluene			0.00526
ethylbenzene			0.00055	ethylbenzene			0.00054	ethylbenzene			0.00034
xylenes			0.00239	xylenes			0.00235	xylenes			0.00149
naphthalene			0.00000	naphthalene			0.00000	naphthalene			0.00000
cumene			0.00009	cumene			0.00009	cumene			0.00006
Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{vA}$				Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{vA}$				Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{vA}$			
hexane		y_i	0.00491	hexane		y_i	0.00488	hexane		y_i	0.00300
benzene			0.00613	benzene			0.00609	benzene			0.00370
2,2,4 TMP			0.00483	2,2,4 TMP			0.00479	2,2,4 TMP			0.00289
toluene			0.00604	toluene			0.00598	toluene			0.00354
ethylbenzene			0.00035	ethylbenzene			0.00034	ethylbenzene			0.00020
xylenes			0.00153	xylenes			0.00151	xylenes			0.00087
naphthalene			0.00000	naphthalene			0.00000	naphthalene			0.00000
cumene			0.00005	cumene			0.00005	cumene			0.00003
Liquid Mole Fraction Eq. 40-4 $x_i = (Z_{vi} M_i) / M_i$				Liquid Mole Fraction Eq. 40-4 $x_i = (Z_{vi} M_i) / M_i$				Liquid Mole Fraction Eq. 40-4 $x_i = (Z_{vi} M_i) / M_i$			
hexane		x_i	0.01068	hexane		x_i	0.01068	hexane		x_i	0.01068
benzene			0.02120	benzene			0.02120	benzene			0.02120
2,2,4 TMP			0.03222	2,2,4 TMP			0.03222	2,2,4 TMP			0.03222
toluene			0.06989	toluene			0.06989	toluene			0.06989
ethylbenzene			0.01213	ethylbenzene			0.01213	ethylbenzene			0.01213
xylenes			0.06066	xylenes			0.06066	xylenes			0.06066
naphthalene			0.00298	naphthalene			0.00298	naphthalene			0.00298
cumene			0.00383	cumene			0.00383	cumene			0.00383
Component Vapor pressure $P_{vAi} = (0.019337)10^4 (A - (B/(TLA+C)))$				Component Vapor pressure $P_{vAi} = (0.019337)10^4 (A - (B/(TLA+C)))$				Component Vapor pressure $P_{vAi} = (0.019337)10^4 (A - (B/(TLA+C)))$			
hexane		A	6.878	hexane		A	6.878	hexane		A	6.878
benzene		B	1171.5	benzene		B	1171.5	benzene		B	1171.5
2,2,4 TMP		C	224.37	2,2,4 TMP		C	224.37	2,2,4 TMP		C	224.37
toluene		P_{vAi}	2.9373	toluene		P_{vAi}	2.8649	toluene		P_{vAi}	2.3757
ethylbenzene			6.906	ethylbenzene			6.906	ethylbenzene			6.906
xylenes			1211	xylenes			1211	xylenes			1211
naphthalene			220.79	naphthalene			220.79	naphthalene			220.79
cumene			0.9583	cumene			0.9322	cumene			0.7579
hexane			7.017	hexane			7.017	hexane			7.017
ethylbenzene			1377.6	ethylbenzene			1377.6	ethylbenzene			1377.6
xylenes			222.64	xylenes			222.64	xylenes			222.64
naphthalene			0.5361	naphthalene			0.5361	naphthalene			0.5361
cumene			0.1781	cumene			0.1781	cumene			0.1781
hexane			6.95	hexane			6.95	hexane			6.95
ethylbenzene			1419.3	ethylbenzene			1419.3	ethylbenzene			1419.3
xylenes			212.61	xylenes			212.61	xylenes			212.61
naphthalene			0.1611	naphthalene			0.1611	naphthalene			0.1611
cumene			0.0050	cumene			0.0050	cumene			0.0050
hexane			7.146	hexane			7.146	hexane			7.146
ethylbenzene			1831.6	ethylbenzene			1831.6	ethylbenzene			1831.6
xylenes			211.82	xylenes			211.82	xylenes			211.82
naphthalene			0.0048	naphthalene			0.0048	naphthalene			0.0048
cumene			0.0856	cumene			0.0856	cumene			0.0856

MONTH October				MONTH November				MONTH December									
ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units						
Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D + L_{LD}$)		LT	270.57	lb/month	Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D + L_{LD}$)		LT	240.09	lb/month	Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D + L_{LD}$)		LT	187.84	lb/month			
			0.14	tons/month				0.12	tons/month				0.09	tons/month			
Product Type			Gasoline - RVP 13.5		Product Type			Gasoline - RVP 15		Product Type			Gasoline - RVP 15				
Monthly Throughput (only change if actual is known)		Q_{month}	79,287.24	barrels/month	Monthly Throughput (only change if actual is known)		Q_{month}	79,287.24	barrels/month	Monthly Throughput (only change if actual is known)		Q_{month}	79,287.24	barrels/month			
Vapor Molecular weight		M_v	62.00		Vapor Molecular weight		M_v	60.15		Vapor Molecular weight		M_v	60.15				
Vapor Pressure Equation Constant A		A	11.63		Vapor Pressure Equation Constant A		A	11.60		Vapor Pressure Equation Constant A		A	11.60				
Vapor Pressure Equation Constant B		B	5015.72	$^{\circ}R$	Vapor Pressure Equation Constant B		B	4937.93	$^{\circ}R$	Vapor Pressure Equation Constant B		B	4937.93	$^{\circ}R$			
Daily total solar insolation on a horizontal surface		I	948.0	Btu/ft ² -day	Daily total solar insolation on a horizontal surface		I	621.0	Btu/ft ² -day	Daily total solar insolation on a horizontal surface		I	501.0	Btu/ft ² -day			
Average Daily Ambient Temperature Eq. 1-30					Average Daily Ambient Temperature Eq. 1-30					Average Daily Ambient Temperature Eq. 1-30							
TAA = ((TAX+TAN)/2)		T_{AA}	514.75	$^{\circ}R$	TAA = ((TAX+TAN)/2)		T_{AA}	505.35	$^{\circ}R$	TAA = ((TAX+TAN)/2)		T_{AA}	495.50	$^{\circ}R$			
Average daily maximum ambient temperature, Table 7.1-7		T_{AX}	522.40	$^{\circ}R$	Average daily maximum ambient temperature, Table 7.1-7		T_{AX}	512.10	$^{\circ}R$	Average daily maximum ambient temperature, Table 7.1-7		T_{AX}	501.80	$^{\circ}R$			
Average daily minimum ambient temperature, Table 7.1-7		T_{AN}	507.10	$^{\circ}R$	Average daily minimum ambient temperature, Table 7.1-7		T_{AN}	498.60	$^{\circ}R$	Average daily minimum ambient temperature, Table 7.1-7		T_{AN}	489.20	$^{\circ}R$			
Liquid Bulk Temperature Eq 1-31:					Liquid Bulk Temperature Eq 1-31:					Liquid Bulk Temperature Eq 1-31:							
TB = TAA + 0.003 as I		T_B	515.46		TB = TAA + 0.003 as I		T_B	505.82		TB = TAA + 0.003 as I		T_B	495.88				
Average Daily Liquid Surface Temperature Eq. 1-28					Average Daily Liquid Surface Temperature Eq. 1-28					Average Daily Liquid Surface Temperature Eq. 1-28							
TLA = 0.3*TAA + 0.7*TB + 0.004* α 1		T_{LA}	516.20	$^{\circ}R$	TLA = 0.3*TAA + 0.7*TB + 0.004* α 1		T_{LA}	506.30	$^{\circ}R$	TLA = 0.3*TAA + 0.7*TB + 0.004* α 1		T_{LA}	496.26	$^{\circ}R$			
True Vapor Pressure Eq. 1-25:					True Vapor Pressure Eq. 1-25:					True Vapor Pressure Eq. 1-25:							
PVA = exp(A-(B/TLA))		P_{VA}	6.790	psia	PVA = exp(A-(B/TLA))		P_{VA}	6.340	psia	PVA = exp(A-(B/TLA))		P_{VA}	5.205	psia			
Vapor pressure function Eq. 2-4:					Vapor pressure function Eq. 2-4:					Vapor pressure function Eq. 2-4:							
$P^* = P_{VA}/P_A/(1+(1-(P_{VA}/P_A))^{0.5})^2$		P^*	0.154	NA	$P^* = P_{VA}/P_A/(1+(1-(P_{VA}/P_A))^{0.5})^2$		P^*	0.140	NA	$P^* = P_{VA}/P_A/(1+(1-(P_{VA}/P_A))^{0.5})^2$		P^*	0.109	NA			
Rim Seal Losses Eq. 2-3:					Rim Seal Losses Eq. 2-3:					Rim Seal Losses Eq. 2-3:							
$L_R = ((K_{GA} + K_{GB}) \sqrt{DP^* M_v K_c}) / 12 \text{ months}$		L_R	127.18	lb/month	$L_R = ((K_{GA} + K_{GB}) \sqrt{DP^* M_v K_c}) / 12 \text{ months}$		L_R	112.51	lb/month	$L_R = ((K_{GA} + K_{GB}) \sqrt{DP^* M_v K_c}) / 12 \text{ months}$		L_R	87.37	lb/month			
Withdrawal losses Eq. 2-19:					Withdrawal losses Eq. 2-19:					Withdrawal losses Eq. 2-19:							
$L_W = ((0.943)OCsW_j/D_j)^{1.1} (N_j F_j/D_j)$		L_W	6.28	lb/month	$L_W = ((0.943)OCsW_j/D_j)^{1.1} (N_j F_j/D_j)$		L_W	6.28	lb/month	$L_W = ((0.943)OCsW_j/D_j)^{1.1} (N_j F_j/D_j)$		L_W	6.28	lb/month			
Deck Fitting Losses Eq.2-13:					Deck Fitting Losses Eq.2-13:					Deck Fitting Losses Eq.2-13:							
$L_F = F_f P^* M_v K_c$		LF	137.11	lb/month	$L_F = F_f P^* M_v K_c$		LF	121.30	lb/month	$L_F = F_f P^* M_v K_c$		LF	94.19	lb/month			
Deck Seam Losses Eq. 2-18:					Deck Seam Losses Eq. 2-18:					Deck Seam Losses Eq. 2-18:							
$L_D = K_D S_D^{0.7} P^* M_v K_c / 12 \text{ months}$		LD	0.00	lb/month	$L_D = K_D S_D^{0.7} P^* M_v K_c / 12 \text{ months}$		LD	0.00	lb/month	$L_D = K_D S_D^{0.7} P^* M_v K_c / 12 \text{ months}$		LD	0.00	lb/month			
HAPS Speciation				HAPS Speciation				HAPS Speciation									
Product - same as January				Product - same as January				Product - same as January				Product - same as January					
Gasoline			6.420	lb/month	Gasoline			5.206	lb/month	Gasoline			4.036	lb/month			
Total HAP Monthly Emissions			6.420	lb/month	Total HAP Monthly Emissions			5.206	lb/month	Total HAP Monthly Emissions			4.036	lb/month			
Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{vi}L_W$					Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{vi}L_W$					Individual HAP Monthly Em Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{vi}L_W$							
		L_{Ti}					L_{Ti}					L_{Ti}					
hexane			1.0712	lb/month	hexane			0.8488	lb/month	hexane			0.6218	lb/month			
benzene			1.2177	lb/month	benzene			0.9590	lb/month	benzene			0.7034	lb/month			
2,2,4 TMP			1.4964	lb/month	2,2,4 TMP			1.1942	lb/month	2,2,4 TMP			0.9015	lb/month			
toluene			1.6401	lb/month	toluene			1.3281	lb/month	toluene			1.0376	lb/month			
ethylbenzene			0.1622	lb/month	ethylbenzene			0.1407	lb/month	ethylbenzene			0.1219	lb/month			
xylenes			0.7626	lb/month	xylenes			0.6686	lb/month	xylenes			0.5868	lb/month			
naphthalene			0.0266	lb/month	naphthalene			0.0264	lb/month	naphthalene			0.0262	lb/month			
cumene			0.0435	lb/month	cumene			0.0398	lb/month	cumene			0.0366	lb/month			
Vapor Weight Concentrations Eq. 40-6 $Z_{vi} = y_i M_i / M_v$					Vapor Weight Concentrations Eq. 40-6 $Z_{vi} = y_i M_i / M_v$					Vapor Weight Concentration $Z_{vi} = y_i M_i / M_v$							
		M_i	M_v	Z_{vi}			M_i	M_v	Z_{vi}			M_i	M_v	Z_{vi}			
hexane		86.18	62	0.00382	hexane		86.18	60	0.00336	hexane		86.18	60	0.00308			
benzene		78.11	62	0.00418	benzene		78.11	60	0.00362	benzene		78.11	60	0.00325			
2,2,4 TMP		114.23	62	0.00471	2,2,4 TMP		114.23	60	0.00403	2,2,4 TMP		114.23	60	0.00358			
toluene		92.14	62	0.00454	toluene		92.14	60	0.00380	toluene		92.14	60	0.00329			
ethylbenzene		106.17	62	0.00028	ethylbenzene		106.17	60	0.00023	ethylbenzene		106.17	60	0.00019			
xylenes		106.17	62	0.00122	xylenes		106.17	60	0.00098	xylenes		106.17	60	0.00081			
naphthalene		128.17	62	0.00000	naphthalene		128.17	60	0.00000	naphthalene		128.17	60	0.00000			
cumene		120.19	62	0.00005	cumene		120.19	60	0.00004	cumene		120.19	60	0.00003			
Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{VA}$					Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{VA}$					Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{VA}$							
		$P_i = P_{VA}(x_i)$	P_{VA}	y_i			$P_i = P_{VA}(x_i)$	P_{VA}	y_i			$P_i = P_{VA}(x_i)$	P_{VA}	y_i			
hexane		0.018638	6.790	0.00275	hexane		0.014875	6.340	0.00235	hexane		0.011186	5.205	0.00215			
benzene		0.022527	6.790	0.00332	benzene		0.017664	6.340	0.00279	benzene		0.013033	5.205	0.00250			
2,2,4 TMP		0.017363	6.790	0.00256	2,2,4 TMP		0.013463	6.340	0.00212	2,2,4 TMP		0.009817	5.205	0.00189			
toluene		0.020754	6.790	0.00306	toluene		0.015726	6.340	0.00248	toluene		0.011191	5.205	0.00215			
ethylbenzene		0.001114	6.790	0.00016	ethylbenzene		0.000811	6.340	0.00013	ethylbenzene		0.000553	5.205	0.00011			
xylenes		0.004845	6.790	0.00071	xylenes		0.003518	6.340	0.00055	xylenes		0.002391	5.205	0.00046			
naphthalene		0.000006	6.790	0.00000	naphthalene		0.000004	6.340	0.00000	naphthalene		0.000002	5.205	0.00000			
cumene		0.000161	6.790	0.00002	cumene		0.000114	6.340	0.00002	cumene		0.000075	5.205	0.00001			
Liquid Mole Fraction Eq. 40-4 $x_i = (Z_{vi} M_i) / M_i$					Liquid Mole Fraction Eq. 40-4 $x_i = (Z_{vi} M_i) / M_i$					Liquid Mole Fraction Eq. 40-4 $x_i = (Z_{vi} M_i) / M_i$							
		Z_{vi}	M_i	M_v	x_i			Z_{vi}	M_i	M_v	x_i			Z_{vi}	M_i	M_v	x_i
hexane		0.01	92	86.18	0.01068	hexane		0.01	96	86.18	0.01114	hexane		0.01	96	86.18	0.01114
benzene		0.018	92	78.11	0.02120	benzene		0.018	96	78.11	0.02212	benzene		0.018	96	78.11	0.02212
2,2,4 TMP		0.04	92	114.23	0.03222	2,2,4 TMP		0.04	96	114.23	0.03362	2,2,4 TMP		0.04	96	114.23	0.03362
toluene		0.07	92	92.14	0.06989	toluene		0.07	96	92.14	0.07293	toluene		0.07	96	92.14	0.07293
ethylbenzene		0.014	92	106.17	0.01213	ethylbenzene		0.014	96	106.17	0.01266	ethylbenzene		0.014	96	106.17	0.01266
xylenes		0.07	92	106.17	0.06066	xylenes		0.07	96	106.17	0.06329	xylenes		0.07	96	106.17	0.06329
naphthalene		0.00415	92	128.17	0.00298	naphthalene		0.00415	96	128.17	0.00311	naphthalene		0.00415	96	128.17	0.00311
cumene		0.005	92	120.19	0.00383	cumene		0.005	96	120.19	0.00399	cumene		0.005	96	120.19	0.00399
Component Vapor pressure $P_{VA} = (0.019337)10^4(A-(B/(TLA+C)))$					Component Vapor pressure $P_{VA} = (0.019337)10^4(A-(B/(TLA+C)))$					Component Vapor pressure $P_{VA} = (0.019337)10^4(A-(B/(TLA+C)))$							
		A	B	C	P_{VA}			A	B	C	P_{VA}			A	B	C	P_{VA}
hexane		6.878	1171.5	224.37	1.7459	hexane		6.878	1171.5	224.37	1.3354	hexane		6.878	1171.5	224.37	1.0042
benzene		6.906	1211	220.79	1.0625	benzene		6.906	1211	220.79	0.7984	benzene		6.906	1211	220.79	0.5891
2,2,4 TMP		6.812	1257.8	220.74	0.5390	2,2,4 TMP		6.812	1257.8	220.74	0.4005	2,2,4 TMP		6.812	1257.8	220.74	0.2920
toluene		7.017	1377.6	222.64	0.2969	toluene		7.017	1377.6	222.64	0.2156	toluene		7.017	1377.6	222.64	0.1534
ethylbenzene		6.95	1419.3	212.61	0.0918	ethylbenzene		6.95	1419.3	212.61	0.0641	ethylbenzene		6.95	1419.3	212.61	0.0436
xylenes		7.009	1462.3	215.11	0.0799	xylenes		7.009	1462.3	215.11	0.0556	xylenes		7.009	1462.3	215.11	0.0378
naphthalene		7.146	1831.6	211.82	0.0020	naphthalene		7.146	1831.6	211.82	0.0013	naphthalene		7.14			

MONTHLY IFR TANK VOC AND HAP ESTIMATIONS

INPUT DATA				MONTH January				MONTH February				MONTH March			
Tank No.	Symbol	Units		Symbol	Units	Symbol	Units	Symbol	Units	Symbol	Units	Symbol	Units		
30534															
Nearest US Location		Bridgeport, CT		Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D + L_P$)	LT	711.22	lb/month	Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D + L_P$)	LT	749.47	lb/month	Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D + L_P$)	LT	894.65	lb/month
						0.36	tons/month			0.37	tons/month			0.45	tons/month
Absolute Pressure	P_A	14.69	psi	Product Type		Gasoline - RVP 15		Product Type		Gasoline - RVP 15		Product Type		Gasoline - RVP 15	
Product Information				Monthly Throughput (only change if actual is known)	Q_{month}	148,578.18	barrels/month	Monthly Throughput (only change if actual is known)	Q_{month}	148,578.18	barrels/month	Monthly Throughput (only change if actual is known)	Q_{month}	148,578.18	barrels/month
Average organic liquid density	W_L	5.60	lb/gal	Vapor Molecular weight	M_v	60.15		Vapor Molecular weight	M_v	60.15		Vapor Molecular weight	M_v	60.15	
Average Reid Vapor Pressure	RVP	13.00		Vapor Pressure Equation Constant A	A	11.60		Vapor Pressure Equation Constant A	A	11.60		Vapor Pressure Equation Constant A	A	11.60	
Product factor; 0.4 for crude oils or 1 for other organic liquids	K_c	1.00		Vapor Pressure Equation Constant B	B	4937.93	$^{\circ}R$	Vapor Pressure Equation Constant B	B	4937.93	$^{\circ}R$	Vapor Pressure Equation Constant B	B	4937.93	$^{\circ}R$
Tank design data				Daily total solar insolation on a horizontal surface	I	560.0	Btu/ft ² -day	Daily total solar insolation on a horizontal surface	I	847.0	Btu/ft ² -day	Daily total solar insolation on a horizontal surface	I	1156.0	Btu/ft ² -day
Shell height	Hs	48.00	ft	Average Daily Ambient Temperature Eq. 1-30				Average Daily Ambient Temperature Eq. 1-30				Average Daily Ambient Temperature Eq. 1-30			
Diameter	D	134.00	ft	$T_{AA} = ((TAX+TAN)/2)$	T_{AA}	490.50	$^{\circ}R$	$T_{AA} = ((TAX+TAN)/2)$	T_{AA}	492.20	$^{\circ}R$	$T_{AA} = ((TAX+TAN)/2)$	T_{AA}	498.90	$^{\circ}R$
Throughput	Q	6,240,284	gal/month	Average daily maximum ambient temperature, Table 7.1-7	T_{AX}	496.90	$^{\circ}R$	Average daily maximum ambient temperature, Table 7.1-7	T_{AX}	498.80	$^{\circ}R$	Average daily maximum ambient temperature, Table 7.1-7	T_{AX}	506.00	$^{\circ}R$
Maximum Filling Height (use Hs-1 if unknown)	H_{Lx}	47.00	ft	Average daily minimum ambient temperature, Table 7.1-7	T_{AN}	484.10	$^{\circ}R$	Average daily minimum ambient temperature, Table 7.1-7	T_{AN}	485.60	$^{\circ}R$	Average daily minimum ambient temperature, Table 7.1-7	T_{AN}	491.80	$^{\circ}R$
Minimum Filling Height (use Hs-1 if unknown)	H_{Lx}	1.00	ft	Liquid Bulk Temperature Eq. 1-31:				Liquid Bulk Temperature Eq. 1-31:				Liquid Bulk Temperature Eq. 1-31:			
Liquid height (assume 1/2 Hs)	H_L	24.00	ft	$T_B = T_{AA} + 0.003 \text{ as } l$	T_B	490.92		$T_B = T_{AA} + 0.003 \text{ as } l$	T_B	492.84		$T_B = T_{AA} + 0.003 \text{ as } l$	T_B	499.77	
Tank Construction (pick from drop down list)		Welded		Average Daily Liquid Surface Temperature Eq. 2-6				Average Daily Liquid Surface Temperature Eq. 1-28				Average Daily Liquid Surface Temperature Eq. 1-28			
Tank Color (pick from drop down list)		White		$T_{LA} = 0.3T_{AA} + 0.7T_B + 0.004 \alpha^2$	T_{LA}	491.35	$^{\circ}R$	$T_{LA} = 0.3T_{AA} + 0.7T_B + 0.004 \alpha^2$	T_{LA}	493.49	$^{\circ}R$	$T_{LA} = 0.3T_{AA} + 0.7T_B + 0.004 \alpha^2$	T_{LA}	500.66	$^{\circ}R$
Tank Shell Condition (pick from drop down list)		Average		True Vapor Pressure Eq. 1-25:				True Vapor Pressure Eq. 1-25:				True Vapor Pressure Eq. 1-25:			
Tank Interior Condition (pick from drop down list)		Light Rust		$P_{VA} = \exp(A - (B/T_{LA}))$	P_{VA}	4.713	psia	$P_{VA} = \exp(A - (B/T_{LA}))$	P_{VA}	4.922	psia	$P_{VA} = \exp(A - (B/T_{LA}))$	P_{VA}	5.681	psia
Tank paint solar absorptance, dimensionless, Table 7.1-6	α	0.25		Vapor pressure function Eq. 2-4:				Vapor pressure function Eq. 2-4:				Vapor pressure function Eq. 2-4:			
				$P^* = P_{VA}/P_A / (1 + (1 - (P_{VA}/P_A))^{0.5})^2$	P^*	0.096	NA	$P^* = P_{VA}/P_A / (1 + (1 - (P_{VA}/P_A))^{0.5})^2$	P^*	0.102	NA	$P^* = P_{VA}/P_A / (1 + (1 - (P_{VA}/P_A))^{0.5})^2$	P^*	0.122	NA
Internal floating roof design data				Rim Seal Losses Eq. 2-3:				Rim Seal Losses Eq. 2-3:				Rim Seal Losses Eq. 2-3:			
Rim Seal Type:		Mechanical-shoe seal	Shoe-mounted secondary	$L_R = ((K_{S1} + K_{S2}) \sqrt{DP^* M_v K_c}) / 12 \text{ months}$	L_R	103.61	lb/month	$L_R = ((K_{S1} + K_{S2}) \sqrt{DP^* M_v K_c}) / 12 \text{ months}$	L_R	109.26	lb/month	$L_R = ((K_{S1} + K_{S2}) \sqrt{DP^* M_v K_c}) / 12 \text{ months}$	L_R	130.71	lb/month
Rim Seal Fit (Average or Tight fitting)		Average		Withdrawal losses Eq. 2-19:				Withdrawal losses Eq. 2-19:				Withdrawal losses Eq. 2-19:			
Number of fixed roof support columns	Nc	16.00	NA	$L_W = (((0.943)OCsW_v) / D)^2 [1 + (N_F/D)]$	L_W	9.83	lb/month	$L_W = (((0.943)OCsW_v) / D)^2 [1 + (N_F/D)]$	L_W	9.83	lb/month	$L_W = (((0.943)OCsW_v) / D)^2 [1 + (N_F/D)]$	L_W	9.83	lb/month
Effective column diameter (1.1 for 8x7 in. built up columns; 0.7 for 8 in. pipe columns; 1.0 for 8 in. pipe columns)	Fc	1.00	ft	Deck Fitting Losses Eq. 2-13:				Deck Fitting Losses Eq. 2-13:				Deck Fitting Losses Eq. 2-13:			
Deck seam loss per unit seam length factor; 0.0 or 0.14	KD	0.14	lb-mole/ft-yr	$L_F = F_F P^* M_v K_c$	LF	354.81	lb/month	$L_F = F_F P^* M_v K_c$	LF	374.16	lb/month	$L_F = F_F P^* M_v K_c$	LF	447.60	lb/month
Zero wind speed LR factor; see Table 7.1-8	KRa	1.6	lb-mole/ft-yr	Deck Seam Losses Eq. 2-18:				Deck Seam Losses Eq. 2-18:				Deck Seam Losses Eq. 2-18:			
Wind speed dependent LR factor; see Table 7.1-8	KRb	0.3	lb-mole/(mph) ^{1.75} yr	$L_D = K_D S_D^2 P^* M_v K_c / 12 \text{ months}$	LD	242.97	lb/month	$L_D = K_D S_D^2 P^* M_v K_c / 12 \text{ months}$	LD	256.22	lb/month	$L_D = K_D S_D^2 P^* M_v K_c / 12 \text{ months}$	LD	306.51	lb/month
Average ambient wind speed at tank site; for IFR use Zero	v	0.0	mph	HAPS Speciation				HAPS Speciation				HAPS Speciation			
Seal-related wind speed exponent; see Table 7.1-8	n	1.6	NA	Product - select from list		Gasoline		Product - same as January		Gasoline		Product - same as January		Gasoline	
Shell clingage factor; see Table 7.1-10	Cs	0.0015	bb/1,000 ft ²	Total HAP Monthly Emissions		11.660	lb/month	Total HAP Monthly Emissions		12.443	lb/month	Total HAP Monthly Emissions		15.561	lb/month
Deck Design Data				Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{Li}(L_R + L_F + L_D) + Z_{Li}L_W$				Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{Li}(L_R + L_F + L_D) + Z_{Li}L_W$				Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{Li}(L_R + L_F + L_D) + Z_{Li}L_W$			
Deck Seam (choose Welded or Bolted)		Bolted		hexane	2.1625	lb/month		hexane	2.3187	lb/month		hexane	2.9318	lb/month	
Select Deck Construction Type		Continuous sheet		benzene	2.3356	lb/month		benzene	2.5090	lb/month		benzene	3.1945	lb/month	
If bolted continuous sheet or panel, enter width		5	ft	TMP	2.7567	lb/month		TMP	2.9532	lb/month		TMP	3.7347	lb/month	
If bolted panel, also enter length		0	ft	toluene	2.8349	lb/month		toluene	3.0260	lb/month		toluene	3.7942	lb/month	
Deck seam length factor; Length of Seam / Area of Deck	SD	0.20	ft/ft ²	ethylbenzene	0.2571	lb/month		ethylbenzene	0.2690	lb/month		ethylbenzene	0.3178	lb/month	
Deck Fitting Data				xylenes	1.2043	lb/month		xylenes	1.2561	lb/month		xylenes	1.4687	lb/month	
Access Hatch Bolted cover, gasketed	Qty	2	1.6	naphthalene	0.0414	lb/month		naphthalene	0.0415	lb/month		naphthalene	0.0418	lb/month	
Column Well Bolted cover, gasketed sliding cover	16	33.0		cumene	0.0673	lb/month		cumene	0.0692	lb/month		cumene	0.0773	lb/month	
Unslotted Guidepole and Well Gasketed sliding cover w/pole sleeve	0	8.6		Vapor Weight Concentrations Eq. 40-4 $Z_{vi} = y_i M_i / M_v$				Vapor Weight Concentrations Eq. 40-4 $Z_{vi} = y_i M_i / M_v$				Vapor Weight Concentrations Eq. 40-4 $Z_{vi} = y_i M_i / M_v$			
Slotted guidepole/sample well Gasketed sliding cover, with pole wiper	0	41.0		hexane	86.18	60	0.00294	hexane	86.18	60	0.00300	hexane	86.18	60	0.00320
Gauge-float well (automatic g) Unbolted cover, ungasketed	0	14.0		benzene	78.11	60	0.00308	benzene	78.11	60	0.00315	benzene	78.11	60	0.00341
Gauge-hatch/sample port Slit fabric seal, 10% open area	2	12.0		2,2,4 TMP	114.23	60	0.00337	2,2,4 TMP	114.23	60	0.00346	2,2,4 TMP	114.23	60	0.00378
Vacuum Breaker Weighted mechanical actuation, gasketed	1	6.2		toluene	92.14	60	0.00306	toluene	92.14	60	0.00316	toluene	92.14	60	0.00351
Deck drain Stub drain (1-inch diameter)	144	1.2		ethylbenzene	106.17	60	0.00017	ethylbenzene	106.17	60	0.00018	ethylbenzene	106.17	60	0.00020
Legs (IFR type) IFR type, Adjustable	0	7.9		xylenes	106.17	60	0.00074	xylenes	106.17	60	0.00077	xylenes	106.17	60	0.00088
Rim Vent Weighted mechanical actuation, gasketed	0	0.7		naphthalene	128.17	60	0.00000	naphthalene	128.17	60	0.00000	naphthalene	128.17	60	0.00000
Ladder Sliding cover, ungasketed	0	98.0		cumene	120.19	60	0.00003	cumene	120.19	60	0.00003	cumene	120.19	60	0.00003
Ladder / Guide-Pole Combin'l Ladder sleeve, gasketed sliding cover	0	60.0		Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{VA}$				Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{VA}$				Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{VA}$			
Monthly deck fitting loss factor	F_F	61.18	per month	hexane	0.009680	4.713	0.00205	hexane	0.010314	4.922	0.00210	hexane	0.012697	5.681	0.00224
				benzene	0.011169	4.713	0.00237	benzene	0.011951	4.922	0.00243	benzene	0.014919	5.681	0.00263
				2,2,4 TMP	0.008362	4.713	0.00177	2,2,4 TMP	0.008971	4.922	0.00182	2,2,4 TMP	0.011297	5.681	0.00199
				toluene	0.009416	4.713	0.00200	toluene	0.010156	4.922	0.00206	toluene	0.013018	5.681	0.00229
				ethylbenzene	0.000455	4.713	0.00010	ethylbenzene	0.000495	4.922	0.00010	ethylbenzene	0.000655	5.681	0.00012
				xylenes	0.001965	4.713	0.00042	xylenes	0.002141	4.922	0.00044	xylenes	0.002839	5.681	0.00050
				naphthalene	0.000002	4.713	0.00000	naphthalene	0.000002	4.922	0.00000	naphthalene	0.000003	5.681	0.00000
				cumene	0.000061	4.713	0.00001	cumene	0.000067	4.922	0.00001	cumene	0.000090	5.681	0.00002
				Liquid Mole Fraction Eq. 40-4 $X_i = (Z_{Li} M_i) / M_L$				Liquid Mole Fraction Eq. 40-4 $X_i = (Z_{Li} M_i) / M_L$				Liquid Mole Fraction Eq. 40-4 $X_i = (Z_{Li} M_i) / M_L$			
				hexane	0.01	96	0.01114	hexane	0.01	96	0.01114	hexane	0.01	96	0.01114
				benzene	0.018	96	0.02212	benzene	0.018	96	0.02212	benzene	0.018	96	0.02212
				2,2,4 TMP	0.04	96	0.03362	2,2,4 TMP	0.04	96	0.03362	2,2,4 TMP	0.04	96	0.03362
				toluene	0.07	96	0.07293	toluene	0.07	96	0.07293	toluene	0.07	96	0.07293
				ethylbenzene	0.014	96	0.01266	ethylbenzene	0.014	96	0.01266	ethylbenzene	0.014	96	0.01266
				xylenes	0.07	96	0.06329	xylenes	0.07	96	0.06329	xylenes	0.07	96	0.06329
				naphthalene	0.00415	96	0.00311	naphthalene	0.00415	96	0.00311	naphthalene	0.00415	96	0.00311
				cumene	0.005	96	0.00399	cumene	0.005	96	0.00399	cumene	0.005	96	0.00399
				Component Vapor pressure $P_{VA} = (0.019337)10^4(A - (B/(TLA+C)))$				Component Vapor pressure $P_{VA} = (0.019337)10^4(A - (B/(TLA+C)))$				Component Vapor pressure $P_{VA} = (0.019337)10^4(A - (B/(TLA+C)))$			
				hexane	6.878	1171.5	224.37	hexane	6.878	1171.5	224.37	hexane	6.878	1171.5	224.37
				benzene	6.906	1211	220.79	benzene	6.906	1211	220.79	benzene	6.906	1211	220.79
				2,2,4 TMP	6.812	1257.8	220.74	2,2							

MONTH April				MONTH May				MONTH June			
ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units
Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_F + L_D$)		LT	1,031.55 lb/month	Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_F + L_D$)		LT	813.02 lb/month	Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_F + L_D$)		LT	1,033.32 lb/month
			0.52 tons/month				0.41 tons/month				0.52 tons/month
Product Type		Gasoline - RVP 13.5		Product Type		Gasoline - RVP 9		Product Type		Gasoline - RVP 9	
Monthly Throughput (only change if actual is known)		Q_{month}	148,578.18 barrels/month	Monthly Throughput (only change if actual is known)		Q_{month}	148,578.18 barrels/month	Monthly Throughput (only change if actual is known)		Q_{month}	148,578.18 barrels/month
Vapor Molecular weight		M_v	62.00	Vapor Molecular weight		M_v	68.00	Vapor Molecular weight		M_v	68.00
Vapor Pressure Equation Constant A		A	11.63	Vapor Pressure Equation Constant A		A	11.76	Vapor Pressure Equation Constant A		A	11.76
Vapor Pressure Equation Constant B		B	5015.72 °R	Vapor Pressure Equation Constant B		B	5315.06 °R	Vapor Pressure Equation Constant B		B	5315.06 °R
Daily total solar insolation on a horizontal surface		I	1490.0 Btu/ft ² -day	Daily total solar insolation on a horizontal surface		I	1750.0 Btu/ft ² -day	Daily total solar insolation on a horizontal surface		I	1862.0 Btu/ft ² -day
Average Daily Ambient Temperature Eq. 1-30				Average Daily Ambient Temperature Eq. 1-30				Average Daily Ambient Temperature Eq. 1-30			
TAA = ((TAX+TAN)/2)		T_{AA}	509.15 °R	TAA = ((TAX+TAN)/2)		T_{AA}	518.65 °R	TAA = ((TAX+TAN)/2)		T_{AA}	528.60 °R
Average daily maximum ambient temperature, Table 7.1		T_{AX}	516.80 °R	Average daily maximum ambient temperature, Table 7.1-7		T_{AX}	526.50 °R	Average daily maximum ambient temperature, Table 7.1-7		T_{AX}	536.10 °R
Average daily minimum ambient temperature, Table 7.1		T_{AN}	501.50 °R	Average daily minimum ambient temperature, Table 7.1-7		T_{AN}	510.80 °R	Average daily minimum ambient temperature, Table 7.1-7		T_{AN}	521.10 °R
Liquid Bulk Temperature Eq. 1-31:				Liquid Bulk Temperature Eq. 1-31:				Liquid Bulk Temperature Eq. 1-31:			
TB = TAA + 0.003 cs I		T_B	510.27	TB = TAA + 0.003 cs I		T_B	519.96	TB = TAA + 0.003 cs I		T_B	530.00
Average Daily Liquid Surface Temperature Eq. 1-28				Average Daily Liquid Surface Temperature Eq. 1-28				Average Daily Liquid Surface Temperature Eq. 1-28			
TLA = 0.3*TAA + 0.7*TB + 0.004*αI		T_{LA}	511.42 °R	TLA = 0.3*TAA + 0.7*TB + 0.004*αI		T_{LA}	521.32 °R	TLA = 0.3*TAA + 0.7*TB + 0.004*αI		T_{LA}	531.44 °R
True Vapor Pressure Eq. 1-25:				True Vapor Pressure Eq. 1-25:				True Vapor Pressure Eq. 1-25:			
PvA = exp(A-(B/TLA))		P_{vA}	6.201 psia	PvA = exp(A-(B/TLA))		P_{vA}	4.763 psia	PvA = exp(A-(B/TLA))		P_{vA}	5.783 psia
Vapor pressure function Eq. 2-4:				Vapor pressure function Eq. 2-4:				Vapor pressure function Eq. 2-4:			
$P^* = P_{vA}/P_A/(1+(1-(P_{vA}/P_A))^{5.5})^2$		P^*	0.136 NA	$P^* = P_{vA}/P_A/(1+(1-(P_{vA}/P_A))^{5.5})^2$		P^*	0.098 NA	$P^* = P_{vA}/P_A/(1+(1-(P_{vA}/P_A))^{5.5})^2$		P^*	0.124 NA
Rim Seal Losses Eq. 2-3:				Rim Seal Losses Eq. 2-3:				Rim Seal Losses Eq. 2-3:			
$L_R = ((K_{R1} + K_{R2} \sqrt{V})/DP^* M_v K_c)/12$ months		L_R	150.93 lb/month	$L_R = ((K_{R1} + K_{R2} \sqrt{V})/DP^* M_v K_c)/12$ months		L_R	118.65 lb/month	$L_R = ((K_{R1} + K_{R2} \sqrt{V})/DP^* M_v K_c)/12$ months		L_R	151.19 lb/month
Withdrawal losses Eq. 2-19:				Withdrawal losses Eq. 2-19:				Withdrawal losses Eq. 2-19:			
$L_W = ((0.943)QC(W)/D)^{0.75} * (1 + (N_c F_w/D))$		L_W	9.83 lb/month	$L_W = ((0.943)QC(W)/D)^{0.75} * (1 + (N_c F_w/D))$		L_W	9.83 lb/month	$L_W = ((0.943)QC(W)/D)^{0.75} * (1 + (N_c F_w/D))$		L_W	9.83 lb/month
Deck Fitting Losses Eq. 2-13:				Deck Fitting Losses Eq. 2-13:				Deck Fitting Losses Eq. 2-13:			
$L_F = F_f P^* M_v K_c$		LF	516.85 lb/month	$L_F = F_f P^* M_v K_c$		LF	406.31 lb/month	$L_F = F_f P^* M_v K_c$		LF	517.75 lb/month
Deck Seam Losses Eq. 2-18:				Deck Seam Losses Eq. 2-18:				Deck Seam Losses Eq. 2-18:			
$L_D = K_D S_D P^* M_v K_c/12$ months		LD	353.93 lb/month	$L_D = K_D S_D P^* M_v K_c/12$ months		LD	278.23 lb/month	$L_D = K_D S_D P^* M_v K_c/12$ months		LD	354.55 lb/month
HAPS Speciation				HAPS Speciation				HAPS Speciation			
Product - same as January		Gasoline		Product - same as January		Gasoline		Product - same as January		Gasoline	
Total HAP Monthly Emissions			20.508 lb/month	Total HAP Monthly Emissions			25.069 lb/month	Total HAP Monthly Emissions			34.113 lb/month
Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{Li}L_W$				Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{Li}L_W$				Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{Li}L_W$			
hexane		L_{Ti}	3.8550 lb/month	hexane		L_{Ti}	4.6527 lb/month	hexane		L_{Ti}	6.2691 lb/month
benzene			4.2579 lb/month	benzene			5.2100 lb/month	benzene			7.1100 lb/month
2,2,4 TMP			4.9688 lb/month	2,2,4 TMP			6.0981 lb/month	2,2,4 TMP			8.3358 lb/month
toluene			5.0516 lb/month	toluene			6.2523 lb/month	toluene			8.6078 lb/month
ethylbenzene			0.4024 lb/month	ethylbenzene			0.4885 lb/month	ethylbenzene			0.6559 lb/month
xylenes			1.8384 lb/month	xylenes			2.2169 lb/month	xylenes			2.9525 lb/month
naphthalene			0.0425 lb/month	naphthalene			0.0432 lb/month	naphthalene			0.0448 lb/month
cumene			0.0918 lb/month	cumene			0.1072 lb/month	cumene			0.1372 lb/month
Vapor Weight Concentrations Eq. 40-4 $Z_{vi} = y_i M_i / M_v$				Vapor Weight Concentrations Eq. 40-4 $Z_{vi} = y_i M_i / M_v$				Vapor Weight Concentrations Eq. 40-4 $Z_{vi} = y_i M_i / M_v$			
hexane		M_i	86.18	hexane		M_i	86.18	hexane		M_i	86.18
benzene		M_v	62	benzene		M_v	68	benzene		M_v	68
2,2,4 TMP		Z_{vi}	0.00368	2,2,4 TMP		Z_{vi}	0.00567	2,2,4 TMP		Z_{vi}	0.00603
toluene			0.00399	toluene			0.00627	toluene			0.00677
ethylbenzene			0.00448	ethylbenzene			0.00710	ethylbenzene			0.00776
xylenes			0.00427	xylenes			0.00693	xylenes			0.00774
naphthalene			0.00026	naphthalene			0.00044	naphthalene			0.00051
cumene			0.00113	cumene			0.00190	cumene			0.00221
			0.00000				0.00000				0.00000
			0.00004				0.00007				0.00009
Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{vA}$				Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{vA}$				Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{vA}$			
hexane		$P_i = P_{vA}(x_i)$	6.201	hexane		$P_i = P_{vA}(x_i)$	4.763	hexane		$P_i = P_{vA}(x_i)$	5.783
benzene		P_{vA}	0.00265	benzene		P_{vA}	0.00447	benzene		P_{vA}	0.00476
2,2,4 TMP		y_i	0.00317	2,2,4 TMP		y_i	0.00546	2,2,4 TMP		y_i	0.00590
toluene			0.00243	toluene			0.00423	toluene			0.00462
ethylbenzene			0.00287	ethylbenzene			0.00511	ethylbenzene			0.00571
xylenes			0.00015	xylenes			0.00028	xylenes			0.00032
naphthalene			0.00066	naphthalene			0.00122	naphthalene			0.00142
cumene			0.00000	cumene			0.00000	cumene			0.00000
			0.00002				0.00004				0.00005
Liquid Mole Fraction Eq. 40-4 $x_i = (Z_{Li} M_i) / M_i$				Liquid Mole Fraction Eq. 40-4 $x_i = (Z_{Li} M_i) / M_i$				Liquid Mole Fraction Eq. 40-4 $x_i = (Z_{Li} M_i) / M_i$			
hexane		Z_{Li}	0.01	hexane		Z_{Li}	0.01	hexane		Z_{Li}	0.01
benzene		M_i	92	benzene		M_i	92	benzene		M_i	92
2,2,4 TMP		M_i	86.18	2,2,4 TMP		M_i	86.18	2,2,4 TMP		M_i	86.18
toluene		X_i	0.01068	toluene		X_i	0.01068	toluene		X_i	0.01068
ethylbenzene			0.02120	ethylbenzene			0.02120	ethylbenzene			0.02120
xylenes			0.03222	xylenes			0.03222	xylenes			0.03222
naphthalene			0.06989	naphthalene			0.06989	naphthalene			0.06989
cumene			0.01213	cumene			0.01213	cumene			0.01213
			0.06066				0.06066				0.06066
			0.00298				0.00298				0.00298
			0.00383				0.00383				0.00383
Component Vapor pressure $P_{vA} = (0.019337)10^4(A-(B/(TLA+C)))$				Component Vapor pressure $P_{vA} = (0.019337)10^4(A-(B/(TLA+C)))$				Component Vapor pressure $P_{vA} = (0.019337)10^4(A-(B/(TLA+C)))$			
hexane		A	6.878	hexane		A	6.878	hexane		A	6.878
benzene		B	1171.5	benzene		B	1171.5	benzene		B	1171.5
2,2,4 TMP		C	224.37	2,2,4 TMP		C	224.37	2,2,4 TMP		C	224.37
toluene		P_{vA}	1.5366	toluene		P_{vA}	1.9962	toluene		P_{vA}	2.5773
ethylbenzene			0.9273	ethylbenzene			1.2255	ethylbenzene			1.6087
xylenes			0.4679	xylenes			0.6251	xylenes			0.8293
naphthalene			0.2550	naphthalene			0.3484	naphthalene			0.4725
cumene			0.0773	cumene			0.1098	cumene			0.1546
			0.0672				0.0957				0.1351
			0.0016				0.0026				0.0040
			0.0349				0.0509				0.0735

MONTH July				MONTH August				MONTH eptember			
ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units
Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D + L_G$)		LT	1,176.08 lb/month	Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D + L_G$)		LT	1,146.91 lb/month	Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D + L_G$)		LT	1,594.32 lb/month
			0.59 tons/month				0.57 tons/month				0.80 tons/month
Product Type			Gasoline - RVP 9	Product Type			Gasoline - RVP 9	Product Type			Gasoline - RVP 13.5
Monthly Throughput (only change if actual is known)		Q_{month}	148,578.18 barrels/month	Monthly Throughput (only change if actual is known)		Q_{month}	148,578.18 barrels/month	Monthly Throughput (only change if actual is known)		Q_{month}	148,578.18 barrels/month
Vapor Molecular weight		M_v	68.00	Vapor Molecular weight		M_v	68.00	Vapor Molecular weight		M_v	62.00
Vapor Pressure Equation Constant A		A	11.76	Vapor Pressure Equation Constant A		A	11.76	Vapor Pressure Equation Constant A		A	11.63
Vapor Pressure Equation Constant B		B	5315.06	Vapor Pressure Equation Constant B		B	5315.06	Vapor Pressure Equation Constant B		B	5015.72
Daily total solar insolation on a horizontal surface		I	1904.0 Btu/ft ² -day	Daily total solar insolation on a horizontal surface		I	1685.0 Btu/ft ² -day	Daily total solar insolation on a horizontal surface		I	1320.0 Btu/ft ² -day
Average Daily Ambient Temperature Eq. 1-30				Average Daily Ambient Temperature Eq. 1-30				Average Daily Ambient Temperature Eq. 1-30			
TAA = ((TAX+TAN)/2)		T_{AA}	533.90 °R	TAA = ((TAX+TAN)/2)		T_{AA}	533.20 °R	TAA = ((TAX+TAN)/2)		T_{AA}	526.15 °R
Average daily maximum ambient temperature, T		T_{AX}	541.10 °R	Average daily maximum ambient temperature, T		T_{AX}	540.10 °R	Average daily maximum ambient temperature, Table 7.1-7		T_{AX}	533.40 °R
Average daily minimum ambient temperature, T		T_{AN}	526.70 °R	Average daily minimum ambient temperature, T		T_{AN}	526.30 °R	Average daily minimum ambient temperature, Table 7.1-7		T_{AN}	518.90 °R
Liquid Bulk Temperature Eq 1-31:				Liquid Bulk Temperature Eq 1-31:				Liquid Bulk Temperature Eq 1-31:			
TB = TAA + 0.003 cs I		T_B	535.33	TB = TAA + 0.003 cs I		T_B	534.46	TB = TAA + 0.003 cs I		T_B	527.14
Average Daily Liquid Surface Temperature Eq. 1-28				Average Daily Liquid Surface Temperature Eq. 1-28				Average Daily Liquid Surface Temperature Eq. 1-28			
TLA = 0.3TAA + 0.7TB + 0.004αI		T_{LA}	536.80 °R	TLA = 0.3TAA + 0.7TB + 0.004αI		T_{LA}	535.77 °R	TLA = 0.3TAA + 0.7TB + 0.004αI		T_{LA}	528.16 °R
True Vapor Pressure Eq. 1-25:				True Vapor Pressure Eq. 1-25:				True Vapor Pressure Eq. 1-25:			
PvA = exp(A-(B/TLA))		P_{vA}	6.391 psia	PvA = exp(A-(B/TLA))		P_{vA}	6.270 psia	PvA = exp(A-(B/TLA))		P_{vA}	8.462 psia
Vapor pressure function Eq. 2-4:				Vapor pressure function Eq. 2-4:				Vapor pressure function Eq. 2-4:			
$P^* = P_{vA}/P_A(1+(1-(P_{vA}/P_A))^{0.5})^2$		P^*	0.142 NA	$P^* = P_{vA}/P_A(1+(1-(P_{vA}/P_A))^{0.5})^2$		P^*	0.138 NA	$P^* = P_{vA}/P_A(1+(1-(P_{vA}/P_A))^{0.5})^2$		P^*	0.211 NA
Rim Seal Losses Eq. 2-3:				Rim Seal Losses Eq. 2-3:				Rim Seal Losses Eq. 2-3:			
$L_R = ((K_{eq} + K_{eq} \sqrt{DP})^2 M_v K_c) / 12 \text{ months}$		L_R	172.28 lb/month	$L_R = ((K_{eq} + K_{eq} \sqrt{DP})^2 M_v K_c) / 12 \text{ months}$		L_R	167.97 lb/month	$L_R = ((K_{eq} + K_{eq} \sqrt{DP})^2 M_v K_c) / 12 \text{ months}$		L_R	234.06 lb/month
Withdrawal losses Eq. 2-19:				Withdrawal losses Eq. 2-19:				Withdrawal losses Eq. 2-19:			
$L_W = ((0.943/QC_s W_c) / D) [1 + (N_c F_c / D)]$		L_W	9.83 lb/month	$L_W = ((0.943/QC_s W_c) / D) [1 + (N_c F_c / D)]$		L_W	9.83 lb/month	$L_W = ((0.943/QC_s W_c) / D) [1 + (N_c F_c / D)]$		L_W	9.83 lb/month
Deck Fitting Losses Eq.2-13:				Deck Fitting Losses Eq.2-13:				Deck Fitting Losses Eq.2-13:			
$L_F = F_f P^* M_v K_c$		LF	589.97 lb/month	$L_F = F_f P^* M_v K_c$		LF	575.21 lb/month	$L_F = F_f P^* M_v K_c$		LF	801.54 lb/month
Deck Seam Losses Eq. 2-18:				Deck Seam Losses Eq. 2-18:				Deck Seam Losses Eq. 2-18:			
$L_D = K_D S_D^2 P^* M_v K_c / 12 \text{ months}$		LD	404.00 lb/month	$L_D = K_D S_D^2 P^* M_v K_c / 12 \text{ months}$		LD	393.89 lb/month	$L_D = K_D S_D^2 P^* M_v K_c / 12 \text{ months}$		LD	548.88 lb/month
HAPS Speciation				HAPS Speciation				HAPS Speciation			
Product - same as January			Gasoline	Product - same as January			Gasoline	Product - same as January			Gasoline
Total HAP Monthly Emissions			40.283 lb/month	Total HAP Monthly Emissions			39.005 lb/month	Total HAP Monthly Emissions			36.002 lb/month
Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{Li}L_W$				Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{Li}L_W$				Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{Li}L_W$			
L_{Ti}				L_{Ti}				L_{Ti}			
hexane			7.3499 lb/month	hexane			7.1273 lb/month	hexane			6.6992 lb/month
benzene			8.3930 lb/month	benzene			8.1281 lb/month	benzene			7.5544 lb/month
2,2,4 TMP			9.8570 lb/month	2,2,4 TMP			9.5423 lb/month	2,2,4 TMP			8.8163 lb/month
toluene			10.2321 lb/month	toluene			9.8948 lb/month	toluene			9.0279 lb/month
ethylbenzene			0.7739 lb/month	ethylbenzene			0.7492 lb/month	ethylbenzene			0.6770 lb/month
xylenes			3.4726 lb/month	xylenes			3.3639 lb/month	xylenes			3.0427 lb/month
naphthalene			0.0459 lb/month	naphthalene			0.0457 lb/month	naphthalene			0.0448 lb/month
cumene			0.1586 lb/month	cumene			0.1541 lb/month	cumene			0.1400 lb/month
Vapor Weight Concentrations Eq. 40-6 $Z_{vi} = y_i M_i / M_v$				Vapor Weight Concentrations Eq. 40-6 $Z_{vi} = y_i M_i / M_v$				Vapor Weight Concentrations Eq. 40-6 $Z_{vi} = y_i M_i / M_v$			
Z_{vi}				Z_{vi}				Z_{vi}			
hexane			0.00622	hexane			0.00618	hexane			0.00417
benzene			0.00704	benzene			0.00699	benzene			0.00466
2,2,4 TMP			0.00811	2,2,4 TMP			0.00805	2,2,4 TMP			0.00532
toluene			0.00818	toluene			0.00810	toluene			0.00526
ethylbenzene			0.00055	ethylbenzene			0.00054	ethylbenzene			0.00034
xylenes			0.00239	xylenes			0.00235	xylenes			0.00149
naphthalene			0.00000	naphthalene			0.00000	naphthalene			0.00000
cumene			0.00009	cumene			0.00009	cumene			0.00006
Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{vA}$				Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{vA}$				Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{vA}$			
y_i				y_i				y_i			
hexane			0.00491	hexane			0.00488	hexane			0.00300
benzene			0.00613	benzene			0.00609	benzene			0.00370
2,2,4 TMP			0.00483	2,2,4 TMP			0.00479	2,2,4 TMP			0.00289
toluene			0.00604	toluene			0.00598	toluene			0.00354
ethylbenzene			0.00035	ethylbenzene			0.00034	ethylbenzene			0.00020
xylenes			0.00153	xylenes			0.00151	xylenes			0.00087
naphthalene			0.00000	naphthalene			0.00000	naphthalene			0.00000
cumene			0.00005	cumene			0.00005	cumene			0.00003
Liquid Mole Fraction Eq. 40-4 $X_i = (Z_{Li} M_i) / M_L$				Liquid Mole Fraction Eq. 40-4 $X_i = (Z_{Li} M_i) / M_L$				Liquid Mole Fraction Eq. 40-4 $X_i = (Z_{Li} M_i) / M_L$			
X_i				X_i				X_i			
hexane			0.01068	hexane			0.01068	hexane			0.01068
benzene			0.02120	benzene			0.02120	benzene			0.02120
2,2,4 TMP			0.03222	2,2,4 TMP			0.03222	2,2,4 TMP			0.03222
toluene			0.06989	toluene			0.06989	toluene			0.06989
ethylbenzene			0.01213	ethylbenzene			0.01213	ethylbenzene			0.01213
xylenes			0.06066	xylenes			0.06066	xylenes			0.06066
naphthalene			0.00298	naphthalene			0.00298	naphthalene			0.00298
cumene			0.00383	cumene			0.00383	cumene			0.00383
Component Vapor pressure $P_{vAi} = (0.019337)10^A (A - (B/(TLA+C)))$				Component Vapor pressure $P_{vAi} = (0.019337)10^A (A - (B/(TLA+C)))$				Component Vapor pressure $P_{vAi} = (0.019337)10^A (A - (B/(TLA+C)))$			
P_{vAi}				P_{vAi}				P_{vAi}			
hexane			2.9373	hexane			2.8649	hexane			2.3757
benzene			1.8489	benzene			1.8004	benzene			1.4751
2,2,4 TMP			0.9583	2,2,4 TMP			0.9322	2,2,4 TMP			0.7579
toluene			0.5523	toluene			0.5361	toluene			0.4288
ethylbenzene			0.1841	ethylbenzene			0.1781	ethylbenzene			0.1387
xylenes			0.1611	xylenes			0.1558	xylenes			0.1211
naphthalene			0.0050	naphthalene			0.0048	naphthalene			0.0035
cumene			0.0887	cumene			0.0856	cumene			0.0654

MONTH October				MONTH November				MONTH December			
ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units
Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D + L_{LD}$)		LT	1,163.45 lb/month	Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D + L_{LD}$)		LT	1,030.43 lb/month	Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D + L_{LD}$)		LT	802.34 lb/month
			0.58 tons/month				0.52 tons/month				0.40 tons/month
Product Type			Gasoline - RVP 13.5	Product Type			Gasoline - RVP 15	Product Type			Gasoline - RVP 15
Monthly Throughput (only change if actual is known)		Q_{month}	148,578.18 barrels/month	Monthly Throughput (only change if actual is known)		Q_{month}	148,578.18 barrels/month	Monthly Throughput (only change if actual is known)		Q_{month}	148,578.18 barrels/month
Vapor Molecular weight		M_v	62.00	Vapor Molecular weight		M_v	60.15	Vapor Molecular weight		M_v	60.15
Vapor Pressure Equation Constant A		A	11.63	Vapor Pressure Equation Constant A		A	11.60	Vapor Pressure Equation Constant A		A	11.60
Vapor Pressure Equation Constant B		B	5015.72 °R	Vapor Pressure Equation Constant B		B	4937.93 °R	Vapor Pressure Equation Constant B		B	4937.93 °R
Daily total solar insolation on a horizontal surface		I	948.0 Btu/ft ² -day	Daily total solar insolation on a horizontal surface		I	621.0 Btu/ft ² -day	Daily total solar insolation on a horizontal surface		I	501.0 Btu/ft ² -day
Average Daily Ambient Temperature Eq. 1-30				Average Daily Ambient Temperature Eq. 1-30				Average Daily Ambient Temperature Eq. 1-30			
TAA = ((TAX+TAN)/2)		T_{AA}	514.75 °R	TAA = ((TAX+TAN)/2)		T_{AA}	505.35 °R	TAA = ((TAX+TAN)/2)		T_{AA}	495.50 °R
Average daily maximum ambient temperature, Table 7.1-7		T_{AX}	522.40 °R	Average daily maximum ambient temperature, Table 7.1-7		T_{AX}	512.10 °R	Average daily maximum ambient temperature, Table 7.1-7		T_{AX}	501.80 °R
Average daily minimum ambient temperature, Table 7.1-7		T_{AN}	507.10 °R	Average daily minimum ambient temperature, Table 7.1-7		T_{AN}	498.60 °R	Average daily minimum ambient temperature, Table 7.1-7		T_{AN}	489.20 °R
Liquid Bulk Temperature Eq 1-31:				Liquid Bulk Temperature Eq 1-31:				Liquid Bulk Temperature Eq 1-31:			
TB = TAA + 0.003 as I		T_B	515.46	TB = TAA + 0.003 as I		T_B	505.82	TB = TAA + 0.003 as I		T_B	495.88
Average Daily Liquid Surface Temperature Eq. 1-28				Average Daily Liquid Surface Temperature Eq. 1-28				Average Daily Liquid Surface Temperature Eq. 1-28			
TLA = 0.3*TAA + 0.7*TB + 0.004*α ¹		T_{LA}	516.20 °R	TLA = 0.3*TAA + 0.7*TB + 0.004*α ¹		T_{LA}	506.30 °R	TLA = 0.3*TAA + 0.7*TB + 0.004*α ¹		T_{LA}	496.26 °R
True Vapor Pressure Eq. 1-25:				True Vapor Pressure Eq. 1-25:				True Vapor Pressure Eq. 1-25:			
PVA = exp(A-(B/TLA))		P_{VA}	6.790 psia	PVA = exp(A-(B/TLA))		P_{VA}	6.340 psia	PVA = exp(A-(B/TLA))		P_{VA}	5.205 psia
Vapor pressure function Eq. 2-4:				Vapor pressure function Eq. 2-4:				Vapor pressure function Eq. 2-4:			
$P^* = P_{VA}/P_A/(1+(1-(P_{VA}/P_A))^{0.5})^2$		P^*	0.154 NA	$P^* = P_{VA}/P_A/(1+(1-(P_{VA}/P_A))^{0.5})^2$		P^*	0.140 NA	$P^* = P_{VA}/P_A/(1+(1-(P_{VA}/P_A))^{0.5})^2$		P^*	0.109 NA
Rim Seal Losses Eq. 2-3:				Rim Seal Losses Eq. 2-3:				Rim Seal Losses Eq. 2-3:			
$L_R = ((K_{GA} + K_{GB})/DP^* M_v K_c)/12$ months		L_R	170.42 lb/month	$L_R = ((K_{GA} + K_{GB})/DP^* M_v K_c)/12$ months		L_R	150.77 lb/month	$L_R = ((K_{GA} + K_{GB})/DP^* M_v K_c)/12$ months		L_R	117.07 lb/month
Withdrawal losses Eq. 2-19:				Withdrawal losses Eq. 2-19:				Withdrawal losses Eq. 2-19:			
$L_W = ((0.943)OCsW_j/D)^{1/3} [1+(N_e F_e/D)]$		L_W	9.83 lb/month	$L_W = ((0.943)OCsW_j/D)^{1/3} [1+(N_e F_e/D)]$		L_W	9.83 lb/month	$L_W = ((0.943)OCsW_j/D)^{1/3} [1+(N_e F_e/D)]$		L_W	9.83 lb/month
Deck Fitting Losses Eq.2-13:				Deck Fitting Losses Eq.2-13:				Deck Fitting Losses Eq.2-13:			
$L_F = F_r P^* M_v K_c$		LF	583.58 lb/month	$L_F = F_r P^* M_v K_c$		LF	516.29 lb/month	$L_F = F_r P^* M_v K_c$		LF	400.91 lb/month
Deck Seam Losses Eq. 2-18:				Deck Seam Losses Eq. 2-18:				Deck Seam Losses Eq. 2-18:			
$L_D = K_D S_D P^* M_v K_c/12$ months		LD	399.62 lb/month	$L_D = K_D S_D P^* M_v K_c/12$ months		LD	353.55 lb/month	$L_D = K_D S_D P^* M_v K_c/12$ months		LD	274.53 lb/month
HAPS Speciation				HAPS Speciation				HAPS Speciation			
Product - same as January			Gasoline	Product - same as January			Gasoline	Product - same as January			Gasoline
Total HAP Monthly Emissions			23.960 lb/month	Total HAP Monthly Emissions			18.658 lb/month	Total HAP Monthly Emissions			13.553 lb/month
Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{vi}L_W$				Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{vi}L_W$				Individual HAP Monthly Em Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{vi}L_W$			
		L_{Ti}				L_{Ti}				L_{Ti}	
hexane			4.5000 lb/month	hexane			3.5292 lb/month	hexane			2.5385 lb/month
benzene			4.9988 lb/month	benzene			3.8696 lb/month	benzene			2.7538 lb/month
2,2,4 TMP			5.8284 lb/month	2,2,4 TMP			4.5093 lb/month	2,2,4 TMP			3.2317 lb/month
toluene			5.9284 lb/month	toluene			4.5663 lb/month	toluene			3.2983 lb/month
ethylbenzene			0.4617 lb/month	ethylbenzene			0.3680 lb/month	ethylbenzene			0.2861 lb/month
xylenes			2.0978 lb/month	xylenes			1.6878 lb/month	xylenes			1.3307 lb/month
naphthalene			0.0429 lb/month	naphthalene			0.0422 lb/month	naphthalene			0.0416 lb/month
cumene			0.1021 lb/month	cumene			0.0857 lb/month	cumene			0.0720 lb/month
Vapor Weight Concentrations Eq. 40-6 $Z_{vi} = y_i M_i / M_v$				Vapor Weight Concentrations Eq. 40-6 $Z_{vi} = y_i M_i / M_v$				Vapor Weight Concentration $Z_{vi} = y_i M_i / M_v$			
		M_i	M_v			M_i	M_v			M_i	M_v
hexane		86.18	62	hexane		86.18	60	hexane		86.18	60
benzene		78.11	62	benzene		78.11	60	benzene		78.11	60
2,2,4 TMP		114.23	62	2,2,4 TMP		114.23	60	2,2,4 TMP		114.23	60
toluene		92.14	62	toluene		92.14	60	toluene		92.14	60
ethylbenzene		106.17	62	ethylbenzene		106.17	60	ethylbenzene		106.17	60
xylenes		106.17	62	xylenes		106.17	60	xylenes		106.17	60
naphthalene		128.17	62	naphthalene		128.17	60	naphthalene		128.17	60
cumene		120.19	62	cumene		120.19	60	cumene		120.19	60
Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{VA}$				Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{VA}$				Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{VA}$			
		$P_i = P_{VA}(x_i)$	P_{VA}			$P_i = P_{VA}(x_i)$	P_{VA}			$P_i = P_{VA}(x_i)$	P_{VA}
hexane		0.018638	6.790	hexane		0.014875	6.340	hexane		0.011186	5.205
benzene		0.022527	6.790	benzene		0.017664	6.340	benzene		0.013033	5.205
2,2,4 TMP		0.017363	6.790	2,2,4 TMP		0.013463	6.340	2,2,4 TMP		0.009817	5.205
toluene		0.020754	6.790	toluene		0.015726	6.340	toluene		0.011191	5.205
ethylbenzene		0.001114	6.790	ethylbenzene		0.000811	6.340	ethylbenzene		0.000553	5.205
xylenes		0.004845	6.790	xylenes		0.003518	6.340	xylenes		0.002391	5.205
naphthalene		0.000006	6.790	naphthalene		0.000004	6.340	naphthalene		0.000002	5.205
cumene		0.000161	6.790	cumene		0.000114	6.340	cumene		0.000075	5.205
Liquid Mole Fraction Eq. 40-4 $x_i = (Z_{vi} M_i) / M_i$				Liquid Mole Fraction Eq. 40-4 $x_i = (Z_{vi} M_i) / M_i$				Liquid Mole Fraction Eq. 40-4 $x_i = (Z_{vi} M_i) / M_i$			
		Z_{vi}	M_i			Z_{vi}	M_i			Z_{vi}	M_i
hexane		0.01	92	hexane		0.01	96	hexane		0.01	96
benzene		0.018	92	benzene		0.018	96	benzene		0.018	96
2,2,4 TMP		0.04	92	2,2,4 TMP		0.04	96	2,2,4 TMP		0.04	96
toluene		0.07	92	toluene		0.07	96	toluene		0.07	96
ethylbenzene		0.014	92	ethylbenzene		0.014	96	ethylbenzene		0.014	96
xylenes		0.07	92	xylenes		0.07	96	xylenes		0.07	96
naphthalene		0.00415	92	naphthalene		0.00415	96	naphthalene		0.00415	96
cumene		0.005	92	cumene		0.005	96	cumene		0.005	96
Component Vapor pressure $P_{VA} = (0.019337)10^4(A-(B/(TLA+C)))$				Component Vapor pressure $P_{VA} = (0.019337)10^4(A-(B/(TLA+C)))$				Component Vapor pressure $P_{VA} = (0.019337)10^4(A-(B/(TLA+C)))$			
		A	B			A	B			A	B
hexane		6.878	1171.5	hexane		6.878	1171.5	hexane		6.878	1171.5
benzene		6.906	1211	benzene		6.906	1211	benzene		6.906	1211
2,2,4 TMP		6.812	1257.8	2,2,4 TMP		6.812	1257.8	2,2,4 TMP		6.812	1257.8
toluene		7.017	1377.6	toluene		7.017	1377.6	toluene		7.017	1377.6
ethylbenzene		6.95	1419.3	ethylbenzene		6.95	1419.3	ethylbenzene		6.95	1419.3
xylenes		7.009	1462.3	xylenes		7.009	1462.3	xylenes		7.009	1462.3
naphthalene		7.146	1831.6	naphthalene		7.146	1831.6	naphthalene		7.146	1831.6
cumene		6.929	1455.8	cumene		6.929	1455.8	cumene		6.929	1455.8

MONTHLY IFR TANK VOC AND HAP ESTIMATIONS

INPUT DATA				MONTH January				MONTH February				MONTH March			
Tank No.	Symbol	Units		Symbol	Units	Symbol	Units	Symbol	Units	Symbol	Units	Symbol	Units		
30533															
Nearest US Location		Bridgeport, CT		Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D + L_{L_1}$)	LT	146.14	lb/month	Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D + L_{L_1}$)	LT	153.92	lb/month	Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D + L_{L_1}$)	LT	183.47	lb/month
Absolute Pressure	P_A	14.69	psi	Product Type		Gasoline - RVP 15		Product Type		Gasoline - RVP 15		Product Type		Gasoline - RVP 15	
Product Information				Monthly Throughput (only change if actual is known)	Q_{month}	20,923.85	barrels/month	Monthly Throughput (only change if actual is known)	Q_{month}	20,923.85	barrels/month	Monthly Throughput (only change if actual is known)	Q_{month}	20,923.85	barrels/month
Average organic liquid density	W_L	5.60	lb/gal	Vapor Molecular weight	M_v	60.15		Vapor Molecular weight	M_v	60.15		Vapor Molecular weight	M_v	60.15	
Average Reid Vapor Pressure	RVP	13.00		Vapor Pressure Equation Constant A	A	11.60		Vapor Pressure Equation Constant A	A	11.60		Vapor Pressure Equation Constant A	A	11.60	
Product factor, 0.4 for crude oils or 1 for other organic liquids	K_c	1.00		Vapor Pressure Equation Constant B	B	4937.93	$^{\circ}R$	Vapor Pressure Equation Constant B	B	4937.93	$^{\circ}R$	Vapor Pressure Equation Constant B	B	4937.93	$^{\circ}R$
Tank design data				Daily total solar insolation on a horizontal surface	I	560.0	Btu/ft ² -day	Daily total solar insolation on a horizontal surface	I	847.0	Btu/ft ² -day	Daily total solar insolation on a horizontal surface	I	1156.0	Btu/ft ² -day
Shell height	Hs	48.00	ft	Average Daily Ambient Temperature Eq. 1-30				Average Daily Ambient Temperature Eq. 1-30				Average Daily Ambient Temperature Eq. 1-30			
Diameter	D	50.00	ft	$T_{AA} = ((TAX+TAN)/2)$	T_{AA}	490.50	$^{\circ}R$	$T_{AA} = ((TAX+TAN)/2)$	T_{AA}	492.20	$^{\circ}R$	$T_{AA} = ((TAX+TAN)/2)$	T_{AA}	498.90	$^{\circ}R$
Throughput	Q	878,802	gal/month	Average daily maximum ambient temperature, Table 7.1-7	T_{AX}	496.90	$^{\circ}R$	Average daily maximum ambient temperature, Table 7.1-7	T_{AX}	498.80	$^{\circ}R$	Average daily maximum ambient temperature, Table 7.1-7	T_{AX}	506.00	$^{\circ}R$
Maximum Filling Height (use Hs-1 if unknown)	H_{LX}	47.00	ft	Average daily minimum ambient temperature, Table 7.1-7	T_{AN}	484.10	$^{\circ}R$	Average daily minimum ambient temperature, Table 7.1-7	T_{AN}	485.60	$^{\circ}R$	Average daily minimum ambient temperature, Table 7.1-7	T_{AN}	491.80	$^{\circ}R$
Minimum Filling Height (use Hs-1 if unknown)	H_{LX}	1.00	ft	Liquid Bulk Temperature Eq. 1-31:				Liquid Bulk Temperature Eq. 1-31:				Liquid Bulk Temperature Eq. 1-31:			
Liquid height (assume 1/2 Hs)	H_L	24.00	ft	$T_B = T_{AA} + 0.003 \text{ as } 1$	T_B	490.92		$T_B = T_{AA} + 0.003 \text{ as } 1$	T_B	492.84		$T_B = T_{AA} + 0.003 \text{ as } 1$	T_B	499.77	
Tank Construction (pick from drop down list)	Welded			Average Daily Liquid Surface Temperature Eq. 2-6				Average Daily Liquid Surface Temperature Eq. 1-28				Average Daily Liquid Surface Temperature Eq. 1-28			
Tank Color (pick from drop down list)	White			$T_{LA} = 0.3T_{AA} + 0.7T_B + 0.004 \alpha^1$	T_{LA}	491.35	$^{\circ}R$	$T_{LA} = 0.3T_{AA} + 0.7T_B + 0.004 \alpha^1$	T_{LA}	493.49	$^{\circ}R$	$T_{LA} = 0.3T_{AA} + 0.7T_B + 0.004 \alpha^1$	T_{LA}	500.66	$^{\circ}R$
Tank Shell Condition (pick from drop down list)	Average			True Vapor Pressure Eq. 1-25:				True Vapor Pressure Eq. 1-25:				True Vapor Pressure Eq. 1-25:			
Tank Interior Condition (pick from drop down list)	Light Rust			$P_{VA} = \exp(A - (B/T_{LA}))$	P_{VA}	4.713	psia	$P_{VA} = \exp(A - (B/T_{LA}))$	P_{VA}	4.922	psia	$P_{VA} = \exp(A - (B/T_{LA}))$	P_{VA}	5.681	psia
Tank paint solar absorptance, dimensionless, Table 7.1-6	α	0.25		Vapor pressure function Eq. 2-4:				Vapor pressure function Eq. 2-4:				Vapor pressure function Eq. 2-4:			
				$P^* = P_{VA}/P_A / (1 + (1 - (P_{VA}/P_A))^{0.5})^2$	P^*	0.096	NA	$P^* = P_{VA}/P_A / (1 + (1 - (P_{VA}/P_A))^{0.5})^2$	P^*	0.102	NA	$P^* = P_{VA}/P_A / (1 + (1 - (P_{VA}/P_A))^{0.5})^2$	P^*	0.122	NA
Internal floating roof design data				Rim Seal Losses Eq. 2-3:				Rim Seal Losses Eq. 2-3:				Rim Seal Losses Eq. 2-3:			
Rim Seal Type:	Mechanical-shoe seal	Shoe-mounted secondary		$L_R = ((K_{S1} + K_{S2}) \sqrt{DP^*} M_v K_c) / 12 \text{ months}$	L_R	38.66	lb/month	$L_R = ((K_{S1} + K_{S2}) \sqrt{DP^*} M_v K_c) / 12 \text{ months}$	L_R	40.77	lb/month	$L_R = ((K_{S1} + K_{S2}) \sqrt{DP^*} M_v K_c) / 12 \text{ months}$	L_R	48.77	lb/month
Rim Seal Fit (Average or Tight fitting)		Average		Withdrawal losses Eq. 2-19:				Withdrawal losses Eq. 2-19:				Withdrawal losses Eq. 2-19:			
Number of fixed roof support columns	Nc	1.00	NA	$L_W = (((0.943)OCsW_v) / D)^2 [1 + (N_F/D)]$	L_W	3.38	lb/month	$L_W = (((0.943)OCsW_v) / D)^2 [1 + (N_F/D)]$	L_W	3.38	lb/month	$L_W = (((0.943)OCsW_v) / D)^2 [1 + (N_F/D)]$	L_W	3.38	lb/month
Effective column diameter (1.1 for 8x7 in. built up columns; 0.7 for 8 in. pipe columns; 1.0 for 8 in. pipe columns)	Fc	1.00	ft	Deck Fitting Losses Eq. 2-13:				Deck Fitting Losses Eq. 2-13:				Deck Fitting Losses Eq. 2-13:			
Deck seam loss per unit seam length factor, 0.0 or 0.14	KD	0.14	lb-mole/ft-yr	$L_F = F_F P^* M_v K_c$	LF	70.27	lb/month	$L_F = F_F P^* M_v K_c$	LF	74.10	lb/month	$L_F = F_F P^* M_v K_c$	LF	88.64	lb/month
Zero wind speed LR factor, see Table 7.1-8	KRa	1.6	lb-mole/ft-yr	Deck Seam Losses Eq. 2-18:				Deck Seam Losses Eq. 2-18:				Deck Seam Losses Eq. 2-18:			
Wind speed dependent LR factor, see Table 7.1-8	KRb	0.3	lb-mole/(mph) ^{1.75} ft ² yr	$L_D = K_D S_D^2 P^* M_v K_c / 12 \text{ months}$	LD	33.83	lb/month	$L_D = K_D S_D^2 P^* M_v K_c / 12 \text{ months}$	LD	35.67	lb/month	$L_D = K_D S_D^2 P^* M_v K_c / 12 \text{ months}$	LD	42.68	lb/month
Average ambient wind speed at tank site, for IFR use Zero	v	0.0	mph	HAPS Speciation				HAPS Speciation				HAPS Speciation			
Seal-related wind speed exponent, see Table 7.1-8	n	1.6	NA	Product - select from list		Gasoline		Product - same as January		Gasoline		Product - same as January		Gasoline	
Shell clingage factor, see Table 7.1-10	Cs	0.0015	bb/1,000 ft ²	Total HAP Monthly Emissions		2.692	lb/month	Total HAP Monthly Emissions		2.852	lb/month	Total HAP Monthly Emissions		3.486	lb/month
Deck Design Data				Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{Li}L_W$				Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{Li}L_W$				Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{Li}L_W$			
Deck Seam (choose Welded or Bolted)		Bolted		hexane	0.4539	lb/month		hexane	0.4857	lb/month		hexane	0.6105	lb/month	
Select Deck Construction Type		Continuous sheet		benzene	0.5002	lb/month		benzene	0.5355	lb/month		benzene	0.6750	lb/month	
If bolted continuous sheet or panel, enter width		5	ft	TMP	0.6163	lb/month		TMP	0.6563	lb/month		TMP	0.8153	lb/month	
If bolted panel, also enter length		0	ft	toluene	0.6736	lb/month		toluene	0.7125	lb/month		toluene	0.8689	lb/month	
Deck seam length factor: Length of Seam / Area of Deck	SD	0.20	ft/ft ²	ethylbenzene	0.0716	lb/month		ethylbenzene	0.0741	lb/month		ethylbenzene	0.0840	lb/month	
Deck Fitting Data				xylenes	0.3417	lb/month		xylenes	0.3523	lb/month		xylenes	0.3955	lb/month	
Access Hatch Bolted cover, gasketed	Qty	2	1.6	naphthalene	0.0142	lb/month		naphthalene	0.0142	lb/month		naphthalene	0.0142	lb/month	
Column Well Bolted cover, gasketed sliding cover	1	33.0		cumene	0.0206	lb/month		cumene	0.0210	lb/month		cumene	0.0226	lb/month	
Unslotted Guidepole and Well Gasketed sliding cover w/pole sleeve	0	8.6		Vapor Weight Concentrations Eq. 40-4 $Z_{vi} = y_i M_i / M_v$				Vapor Weight Concentrations Eq. 40-4 $Z_{vi} = y_i M_i / M_v$				Vapor Weight Concentrations Eq. 40-4 $Z_{vi} = y_i M_i / M_v$			
Slotted guidepole/sample well Gasketed sliding cover, with pole sleeve	1	11.0		hexane	86.18	60	0.00294	hexane	86.18	60	0.00300	hexane	86.18	60	0.00320
Gauge-float well (automatic g) Unbolted cover, ungasketed	0	14.0		benzene	78.11	60	0.00308	benzene	78.11	60	0.00315	benzene	78.11	60	0.00341
Gauge-hatch/sample port Slit fabric seal, 10% open area	1	12.0		2,2,4 TMP	114.23	60	0.00337	2,2,4 TMP	114.23	60	0.00346	2,2,4 TMP	114.23	60	0.00378
Vacuum Breaker Weighted mechanical actuation, gasketed	1	6.2		toluene	92.14	60	0.00306	toluene	92.14	60	0.00316	toluene	92.14	60	0.00351
Deck drain Stub drain (1-inch diameter)	20	1.2		ethylbenzene	106.17	60	0.00017	ethylbenzene	106.17	60	0.00018	ethylbenzene	106.17	60	0.00020
Legs (IFR type) IFR type, Adjustable	0	7.9		xylenes	106.17	60	0.00074	xylenes	106.17	60	0.00077	xylenes	106.17	60	0.00088
Rim Vent Weighted mechanical actuation, gasketed	0	0.7		naphthalene	128.17	60	0.00000	naphthalene	128.17	60	0.00000	naphthalene	128.17	60	0.00000
Ladder Sliding cover, gasketed	1	56.0		cumene	120.19	60	0.00003	cumene	120.19	60	0.00003	cumene	120.19	60	0.00003
Ladder / Guide-Pole Combin Ladder sleeve, ungasketed sliding cover	0	65.0		Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{VA}$				Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{VA}$				Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{VA}$			
Monthly deck fitting loss factor	F_F	12.12	per month	hexane	0.009680	4.713	0.00205	hexane	0.010314	4.922	0.00210	hexane	0.012697	5.681	0.00224
				benzene	0.011169	4.713	0.00237	benzene	0.011951	4.922	0.00243	benzene	0.014919	5.681	0.00263
				2,2,4 TMP	0.008362	4.713	0.00177	2,2,4 TMP	0.008971	4.922	0.00182	2,2,4 TMP	0.011297	5.681	0.00199
				toluene	0.009416	4.713	0.00200	toluene	0.010156	4.922	0.00206	toluene	0.013018	5.681	0.00229
				ethylbenzene	0.000455	4.713	0.00010	ethylbenzene	0.000495	4.922	0.00010	ethylbenzene	0.000655	5.681	0.00012
				xylenes	0.001965	4.713	0.00042	xylenes	0.002141	4.922	0.00044	xylenes	0.002839	5.681	0.00050
				naphthalene	0.000002	4.713	0.00000	naphthalene	0.000002	4.922	0.00000	naphthalene	0.000003	5.681	0.00000
				cumene	0.000061	4.713	0.00001	cumene	0.000067	4.922	0.00001	cumene	0.000090	5.681	0.00002
				Liquid Mole Fraction Eq. 40-4 $X_i = (Z_{Li} M_i) / M_L$				Liquid Mole Fraction Eq. 40-4 $X_i = (Z_{Li} M_i) / M_L$				Liquid Mole Fraction Eq. 40-4 $X_i = (Z_{Li} M_i) / M_L$			
				hexane	0.01	96	0.01114	hexane	0.01	96	0.01114	hexane	0.01	96	0.01114
				benzene	0.018	96	0.02212	benzene	0.018	96	0.02212	benzene	0.018	96	0.02212
				2,2,4 TMP	0.04	96	0.03362	2,2,4 TMP	0.04	96	0.03362	2,2,4 TMP	0.04	96	0.03362
				toluene	0.07	96	0.07293	toluene	0.07	96	0.07293	toluene	0.07	96	0.07293
				ethylbenzene	0.014	96	0.01266	ethylbenzene	0.014	96	0.01266	ethylbenzene	0.014	96	0.01266
				xylenes	0.07	96	0.06329	xylenes	0.07	96	0.06329	xylenes	0.07	96	0.06329
				naphthalene	0.00415	96	0.00311	naphthalene	0.00415	96	0.00311	naphthalene	0.00415	96	0.00311
				cumene	0.005	96	0.00399	cumene	0.005	96	0.00399	cumene	0.005	96	0.00399
				Component Vapor pressure $P_{VA} = (0.019337)10^4(A - (B/(TLA+C)))$				Component Vapor pressure $P_{VA} = (0.019337)10^4(A - (B/(TLA+C)))$				Component Vapor pressure $P_{VA} = (0.019337)10^4(A - (B/(TLA+C)))$			
				hexane	6.878	1171.5	224.37	hexane	6.878	1171.5	224.37	hexane	6.878	1171.5	224.37
				benzene	6.906	1211	220.79	benzene	6.906	1211	220.79	benzene	6.906	1211	220.79
				2,2,4 TMP	6.812	1257.8	220.74	2,2,4 TMP	6.812	1257.8	220.74	2,2,4 TMP	6.812	1257.8	220.74

MONTH April				MONTH May				MONTH June			
ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units
Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D + L_S$)		LT	211.33 lb/month	Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D + L_S$)		LT	166.86 lb/month	Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D + L_S$)		LT	211.69 lb/month
			0.11 tons/month				0.08 tons/month				0.11 tons/month
Product Type		Gasoline - RVP 13.5		Product Type		Gasoline - RVP 9		Product Type		Gasoline - RVP 9	
Monthly Throughput (only change if actual is known)		Q_{month}	20,923.85 barrels/month	Monthly Throughput (only change if actual is known)		Q_{month}	20,923.85 barrels/month	Monthly Throughput (only change if actual is known)		Q_{month}	20,923.85 barrels/month
Vapor Molecular weight		M_v	62.00	Vapor Molecular weight		M_v	68.00	Vapor Molecular weight		M_v	68.00
Vapor Pressure Equation Constant A		A	11.63	Vapor Pressure Equation Constant A		A	11.76	Vapor Pressure Equation Constant A		A	11.76
Vapor Pressure Equation Constant B		B	5015.72 °R	Vapor Pressure Equation Constant B		B	5315.06 °R	Vapor Pressure Equation Constant B		B	5315.06 °R
Daily total solar insolation on a horizontal surface		I	1490.0 Btu/ft ² -day	Daily total solar insolation on a horizontal surface		I	1750.0 Btu/ft ² -day	Daily total solar insolation on a horizontal surface		I	1862.0 Btu/ft ² -day
Average Daily Ambient Temperature Eq. 1-30				Average Daily Ambient Temperature Eq. 1-30				Average Daily Ambient Temperature Eq. 1-30			
TAA = ((TAX+TAN)/2)		T_{AA}	509.15 °R	TAA = ((TAX+TAN)/2)		T_{AA}	518.65 °R	TAA = ((TAX+TAN)/2)		T_{AA}	528.60 °R
Average daily maximum ambient temperature, Table 7.1		T_{AX}	516.80 °R	Average daily maximum ambient temperature, Table 7.1-7		T_{AX}	526.50 °R	Average daily maximum ambient temperature, Table 7.1-7		T_{AX}	536.10 °R
Average daily minimum ambient temperature, Table 7.1		T_{AN}	501.50 °R	Average daily minimum ambient temperature, Table 7.1-7		T_{AN}	510.80 °R	Average daily minimum ambient temperature, Table 7.1-7		T_{AN}	521.10 °R
Liquid Bulk Temperature Eq. 1-31:				Liquid Bulk Temperature Eq. 1-31:				Liquid Bulk Temperature Eq. 1-31:			
TB = TAA + 0.003 cs I		T_B	510.27	TB = TAA + 0.003 cs I		T_B	519.96	TB = TAA + 0.003 cs I		T_B	530.00
Average Daily Liquid Surface Temperature Eq. 1-28				Average Daily Liquid Surface Temperature Eq. 1-28				Average Daily Liquid Surface Temperature Eq. 1-28			
TLA = 0.3*TAA + 0.7*TB + 0.004*α ¹		T_{LA}	511.42 °R	TLA = 0.3*TAA + 0.7*TB + 0.004*α ¹		T_{LA}	521.32 °R	TLA = 0.3*TAA + 0.7*TB + 0.004*α ¹		T_{LA}	531.44 °R
True Vapor Pressure Eq. 1-25:				True Vapor Pressure Eq. 1-25:				True Vapor Pressure Eq. 1-25:			
PvA = exp(A-(B/TLA))		P_{vA}	6.201 psia	PvA = exp(A-(B/TLA))		P_{vA}	4.763 psia	PvA = exp(A-(B/TLA))		P_{vA}	5.783 psia
Vapor pressure function Eq. 2-4:				Vapor pressure function Eq. 2-4:				Vapor pressure function Eq. 2-4:			
$P^* = P_{vA}/P_A/(1+(1-(P_{vA}/P_A))^{0.5})^2$		P^*	0.136 NA	$P^* = P_{vA}/P_A/(1+(1-(P_{vA}/P_A))^{0.5})^2$		P^*	0.098 NA	$P^* = P_{vA}/P_A/(1+(1-(P_{vA}/P_A))^{0.5})^2$		P^*	0.124 NA
Rim Seal Losses Eq. 2-3:				Rim Seal Losses Eq. 2-3:				Rim Seal Losses Eq. 2-3:			
$L_R = ((K_{R1} + K_{R2} \sqrt{V})/DP^* M_v K_c)/12$ months		L_R	56.32 lb/month	$L_R = ((K_{R1} + K_{R2} \sqrt{V})/DP^* M_v K_c)/12$ months		L_R	44.27 lb/month	$L_R = ((K_{R1} + K_{R2} \sqrt{V})/DP^* M_v K_c)/12$ months		L_R	56.41 lb/month
Withdrawal losses Eq. 2-19:				Withdrawal losses Eq. 2-19:				Withdrawal losses Eq. 2-19:			
$L_W = ((0.943)QC(W)/D)^{0.75} * (1 + (N_c F_w/D))$		L_W	3.38 lb/month	$L_W = ((0.943)QC(W)/D)^{0.75} * (1 + (N_c F_w/D))$		L_W	3.38 lb/month	$L_W = ((0.943)QC(W)/D)^{0.75} * (1 + (N_c F_w/D))$		L_W	3.38 lb/month
Deck Fitting Losses Eq. 2-13:				Deck Fitting Losses Eq. 2-13:				Deck Fitting Losses Eq. 2-13:			
$L_F = F_r P^* M_v K_c$		LF	102.36 lb/month	$L_F = F_r P^* M_v K_c$		LF	80.46 lb/month	$L_F = F_r P^* M_v K_c$		LF	102.53 lb/month
Deck Seam Losses Eq. 2-18:				Deck Seam Losses Eq. 2-18:				Deck Seam Losses Eq. 2-18:			
$L_D = K_D S_D P^* M_v K_c/12$ months		LD	49.28 lb/month	$L_D = K_D S_D P^* M_v K_c/12$ months		LD	38.74 lb/month	$L_D = K_D S_D P^* M_v K_c/12$ months		LD	49.36 lb/month
HAPS Speciation				HAPS Speciation				HAPS Speciation			
Product - same as January		Gasoline		Product - same as January		Gasoline		Product - same as January		Gasoline	
Total HAP Monthly Emissions			4.493 lb/month	Total HAP Monthly Emissions			5.421 lb/month	Total HAP Monthly Emissions			7.262 lb/month
Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{Li}L_W$				Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{Li}L_W$				Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{Li}L_W$			
hexane		L_{Ti}	0.7984 lb/month	hexane		L_{Ti}	0.9608 lb/month	hexane		L_{Ti}	1.2898 lb/month
benzene			0.8915 lb/month	benzene			1.0852 lb/month	benzene			1.4720 lb/month
2,2,4 TMP			1.0665 lb/month	2,2,4 TMP			1.2964 lb/month	2,2,4 TMP			1.7518 lb/month
toluene			1.1248 lb/month	toluene			1.3692 lb/month	toluene			1.8486 lb/month
ethylbenzene			0.1012 lb/month	ethylbenzene			0.1187 lb/month	ethylbenzene			0.1528 lb/month
xylenes			0.4708 lb/month	xylenes			0.5478 lb/month	xylenes			0.6975 lb/month
naphthalene			0.0144 lb/month	naphthalene			0.0145 lb/month	naphthalene			0.0148 lb/month
cumene			0.0256 lb/month	cumene			0.0287 lb/month	cumene			0.0348 lb/month
Vapor Weight Concentrations Eq. 40-4 $Z_{vi} = y_i M_i / M_v$				Vapor Weight Concentrations Eq. 40-4 $Z_{vi} = y_i M_i / M_v$				Vapor Weight Concentrations Eq. 40-4 $Z_{vi} = y_i M_i / M_v$			
hexane		M_i	86.18	hexane		M_i	86.18	hexane		M_i	86.18
benzene		M_v	62	benzene		M_v	68	benzene		M_v	68
2,2,4 TMP		Z_{vi}	0.00368	2,2,4 TMP		Z_{vi}	0.00567	2,2,4 TMP		Z_{vi}	0.00603
toluene			0.00399	toluene			0.00627	toluene			0.00677
ethylbenzene			0.00448	ethylbenzene			0.00710	ethylbenzene			0.00776
xylenes			0.00427	xylenes			0.00693	xylenes			0.00774
naphthalene			0.00026	naphthalene			0.00044	naphthalene			0.00051
cumene			0.00113	cumene			0.00190	cumene			0.00221
			0.00000				0.00000				0.00000
			0.00004				0.00007				0.00009
Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{vA}$				Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{vA}$				Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{vA}$			
hexane		$P_i = P_{vA}(x_i)$	6.201	hexane		$P_i = P_{vA}(x_i)$	4.763	hexane		$P_i = P_{vA}(x_i)$	5.783
benzene		P_{vA}	0.00265	benzene		P_{vA}	0.00447	benzene		P_{vA}	0.00476
2,2,4 TMP			0.00317	2,2,4 TMP			0.00546	2,2,4 TMP			0.00590
toluene			0.00243	toluene			0.00423	toluene			0.00462
ethylbenzene			0.00287	ethylbenzene			0.00511	ethylbenzene			0.00571
xylenes			0.00015	xylenes			0.00028	xylenes			0.00032
naphthalene			0.00066	naphthalene			0.00122	naphthalene			0.00142
cumene			0.00000	cumene			0.00000	cumene			0.00000
			0.00002				0.00004				0.00005
Liquid Mole Fraction Eq. 40-4 $x_i = (Z_{Li} M_i) / M_i$				Liquid Mole Fraction Eq. 40-4 $x_i = (Z_{Li} M_i) / M_i$				Liquid Mole Fraction Eq. 40-4 $x_i = (Z_{Li} M_i) / M_i$			
hexane		Z_{Li}	0.01	hexane		Z_{Li}	0.01	hexane		Z_{Li}	0.01
benzene		M_i	86.18	benzene		M_i	86.18	benzene		M_i	86.18
2,2,4 TMP		M_v	62	2,2,4 TMP		M_v	68	2,2,4 TMP		M_v	68
toluene		X_i	0.01068	toluene		X_i	0.01068	toluene		X_i	0.01068
ethylbenzene			0.02120	ethylbenzene			0.02120	ethylbenzene			0.02120
xylenes			0.03222	xylenes			0.03222	xylenes			0.03222
naphthalene			0.06989	naphthalene			0.06989	naphthalene			0.06989
cumene			0.01213	cumene			0.01213	cumene			0.01213
			0.06066				0.06066				0.06066
			0.00298				0.00298				0.00298
			0.00383				0.00383				0.00383
Component Vapor pressure $P_{vA} = (0.019337)10^4(A-(B/(TLA+C)))$				Component Vapor pressure $P_{vA} = (0.019337)10^4(A-(B/(TLA+C)))$				Component Vapor pressure $P_{vA} = (0.019337)10^4(A-(B/(TLA+C)))$			
hexane		A	6.878	hexane		A	6.878	hexane		A	6.878
benzene		B	1171.5	benzene		B	1171.5	benzene		B	1171.5
2,2,4 TMP		C	224.37	2,2,4 TMP		C	224.37	2,2,4 TMP		C	224.37
toluene		P_{vA}	1.5366	toluene		P_{vA}	1.9962	toluene		P_{vA}	2.5773
ethylbenzene			0.9273	ethylbenzene			1.2255	ethylbenzene			1.6087
xylenes			0.4679	xylenes			0.6251	xylenes			0.8293
naphthalene			0.2550	naphthalene			0.3484	naphthalene			0.4725
cumene			0.0773	cumene			0.1098	cumene			0.1546
			0.0672				0.0957				0.1351
			0.0016				0.0026				0.0040
			0.0349				0.0509				0.0735

MONTH July				MONTH August				MONTH September			
ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units
Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D$)		LT	240.75 lb/month	Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D$)		LT	234.81 lb/month	Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D$)		LT	325.88 lb/month
			0.12 tons/month				0.12 tons/month				0.16 tons/month
Product Type			Gasoline - RVP 9	Product Type			Gasoline - RVP 9	Product Type			Gasoline - RVP 13.5
Monthly Throughput (only change if actual is known)		Q_{month}	20,923.85 barrels/month	Monthly Throughput (only change if actual is known)		Q_{month}	20,923.85 barrels/month	Monthly Throughput (only change if actual is known)		Q_{month}	20,923.85 barrels/month
Vapor Molecular weight		M_v	68.00	Vapor Molecular weight		M_v	68.00	Vapor Molecular weight		M_v	62.00
Vapor Pressure Equation Constant A		A	11.76	Vapor Pressure Equation Constant A		A	11.76	Vapor Pressure Equation Constant A		A	11.63
Vapor Pressure Equation Constant B		B	5315.06	Vapor Pressure Equation Constant B		B	5315.06	Vapor Pressure Equation Constant B		B	5015.72
Daily total solar insolation on a horizontal surface		I	1904.0 Btu/ft ² -day	Daily total solar insolation on a horizontal surface		I	1685.0 Btu/ft ² -day	Daily total solar insolation on a horizontal surface		I	1320.0 Btu/ft ² -day
Average Daily Ambient Temperature Eq. 1-30				Average Daily Ambient Temperature Eq. 1-30				Average Daily Ambient Temperature Eq. 1-30			
TAA = ((TAX+TAN)/2)		T_{AA}	533.90 °R	TAA = ((TAX+TAN)/2)		T_{AA}	533.20 °R	TAA = ((TAX+TAN)/2)		T_{AA}	526.15 °R
Average daily maximum ambient temperature, Table 7.1-7		T_{AX}	541.10 °R	Average daily maximum ambient temperature, Table 7.1-7		T_{AX}	540.10 °R	Average daily maximum ambient temperature, Table 7.1-7		T_{AX}	533.40 °R
Average daily minimum ambient temperature, Table 7.1-7		T_{AN}	526.70 °R	Average daily minimum ambient temperature, Table 7.1-7		T_{AN}	526.30 °R	Average daily minimum ambient temperature, Table 7.1-7		T_{AN}	518.90 °R
Liquid Bulk Temperature Eq. 1-31:				Liquid Bulk Temperature Eq. 1-31:				Liquid Bulk Temperature Eq. 1-31:			
TB = TAA + 0.003 cs I		T_B	535.33	TB = TAA + 0.003 cs I		T_B	534.46	TB = TAA + 0.003 cs I		T_B	527.14
Average Daily Liquid Surface Temperature Eq. 1-28				Average Daily Liquid Surface Temperature Eq. 1-28				Average Daily Liquid Surface Temperature Eq. 1-28			
TLA = 0.3TAA + 0.7TB + 0.004αI		T_{LA}	536.80 °R	TLA = 0.3TAA + 0.7TB + 0.004αI		T_{LA}	535.77 °R	TLA = 0.3TAA + 0.7TB + 0.004αI		T_{LA}	528.16 °R
True Vapor Pressure Eq. 1-25:				True Vapor Pressure Eq. 1-25:				True Vapor Pressure Eq. 1-25:			
PVA = exp(A-(B/TLA))		P_{VA}	6.391 psia	PVA = exp(A-(B/TLA))		P_{VA}	6.270 psia	PVA = exp(A-(B/TLA))		P_{VA}	8.462 psia
Vapor pressure function Eq. 2-4:				Vapor pressure function Eq. 2-4:				Vapor pressure function Eq. 2-4:			
$P^* = P_{VA}/P_A(1+(1-(P_{VA}/P_A))^{0.5})^2$		P^*	0.142 NA	$P^* = P_{VA}/P_A(1+(1-(P_{VA}/P_A))^{0.5})^2$		P^*	0.138 NA	$P^* = P_{VA}/P_A(1+(1-(P_{VA}/P_A))^{0.5})^2$		P^*	0.211 NA
Rim Seal Losses Eq. 2-3:				Rim Seal Losses Eq. 2-3:				Rim Seal Losses Eq. 2-3:			
$L_R = ((K_{R1} + K_{R2} \sqrt{DP})^2 M_v K_c) / 12 \text{ months}$		L_R	64.28 lb/month	$L_R = ((K_{R1} + K_{R2} \sqrt{DP})^2 M_v K_c) / 12 \text{ months}$		L_R	62.68 lb/month	$L_R = ((K_{R1} + K_{R2} \sqrt{DP})^2 M_v K_c) / 12 \text{ months}$		L_R	87.34 lb/month
Withdrawal losses Eq. 2-19:				Withdrawal losses Eq. 2-19:				Withdrawal losses Eq. 2-19:			
$L_W = ((0.943)QC_s W_v) / D [1 + (N_e F_e / D)]$		L_W	3.38 lb/month	$L_W = ((0.943)QC_s W_v) / D [1 + (N_e F_e / D)]$		L_W	3.38 lb/month	$L_W = ((0.943)QC_s W_v) / D [1 + (N_e F_e / D)]$		L_W	3.38 lb/month
Deck Fitting Losses Eq.2-13:				Deck Fitting Losses Eq.2-13:				Deck Fitting Losses Eq.2-13:			
$L_F = F_f P^* M_v K_c$		LF	116.84 lb/month	$L_F = F_f P^* M_v K_c$		LF	113.91 lb/month	$L_F = F_f P^* M_v K_c$		LF	158.74 lb/month
Deck Seam Losses Eq. 2-18:				Deck Seam Losses Eq. 2-18:				Deck Seam Losses Eq. 2-18:			
$L_D = K_D S_D^2 P^* M_v K_c / 12 \text{ months}$		LD	56.25 lb/month	$L_D = K_D S_D^2 P^* M_v K_c / 12 \text{ months}$		LD	54.84 lb/month	$L_D = K_D S_D^2 P^* M_v K_c / 12 \text{ months}$		LD	76.42 lb/month
HAPS Speciation				HAPS Speciation				HAPS Speciation			
Product - same as January			Gasoline	Product - same as January			Gasoline	Product - same as January			Gasoline
Total HAP Monthly Emissions			8.518 lb/month	Total HAP Monthly Emissions			8.258 lb/month	Total HAP Monthly Emissions			7.647 lb/month
Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{Li}L_W$				Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{Li}L_W$				Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{Li}L_W$			
hexane		L_{Ti}	1.5097 lb/month	hexane		L_{Ti}	1.4644 lb/month	hexane		L_{Ti}	1.3773 lb/month
benzene			1.7331 lb/month	benzene			1.6792 lb/month	benzene			1.5624 lb/month
2,2,4 TMP			2.0614 lb/month	2,2,4 TMP			1.9974 lb/month	2,2,4 TMP			1.8496 lb/month
toluene			2.1792 lb/month	toluene			2.1105 lb/month	toluene			1.9341 lb/month
ethylbenzene			0.1768 lb/month	ethylbenzene			0.1718 lb/month	ethylbenzene			0.1571 lb/month
xylenes			0.8034 lb/month	xylenes			0.7813 lb/month	xylenes			0.7159 lb/month
naphthalene			0.0151 lb/month	naphthalene			0.0150 lb/month	naphthalene			0.0148 lb/month
cumene			0.0392 lb/month	cumene			0.0383 lb/month	cumene			0.0354 lb/month
Vapor Weight Concentrations Eq. 40-5 $Z_{vi} = y_i M_i / M_v$				Vapor Weight Concentrations Eq. 40-5 $Z_{vi} = y_i M_i / M_v$				Vapor Weight Concentrations Eq. 40-5 $Z_{vi} = y_i M_i / M_v$			
hexane		Z_{vi}	0.00622	hexane		Z_{vi}	0.00618	hexane		Z_{vi}	0.00417
benzene			0.00704	benzene			0.00699	benzene			0.00466
2,2,4 TMP			0.00811	2,2,4 TMP			0.00805	2,2,4 TMP			0.00532
toluene			0.00818	toluene			0.00810	toluene			0.00526
ethylbenzene			0.00055	ethylbenzene			0.00054	ethylbenzene			0.00034
xylenes			0.00239	xylenes			0.00235	xylenes			0.00149
naphthalene			0.00000	naphthalene			0.00000	naphthalene			0.00000
cumene			0.00009	cumene			0.00009	cumene			0.00006
Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{VA}$				Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{VA}$				Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{VA}$			
hexane		y_i	0.00491	hexane		y_i	0.00488	hexane		y_i	0.00300
benzene			0.00613	benzene			0.00609	benzene			0.00370
2,2,4 TMP			0.00483	2,2,4 TMP			0.00479	2,2,4 TMP			0.00289
toluene			0.00604	toluene			0.00598	toluene			0.00354
ethylbenzene			0.00035	ethylbenzene			0.00034	ethylbenzene			0.00020
xylenes			0.00153	xylenes			0.00151	xylenes			0.00087
naphthalene			0.00000	naphthalene			0.00000	naphthalene			0.00000
cumene			0.00005	cumene			0.00005	cumene			0.00003
Liquid Mole Fraction Eq. 40-4 $X_i = (Z_{Li} M_i) / M_L$				Liquid Mole Fraction Eq. 40-4 $X_i = (Z_{Li} M_i) / M_L$				Liquid Mole Fraction Eq. 40-4 $X_i = (Z_{Li} M_i) / M_L$			
hexane		X_i	0.01068	hexane		X_i	0.01068	hexane		X_i	0.01068
benzene			0.02120	benzene			0.02120	benzene			0.02120
2,2,4 TMP			0.03222	2,2,4 TMP			0.03222	2,2,4 TMP			0.03222
toluene			0.06989	toluene			0.06989	toluene			0.06989
ethylbenzene			0.01213	ethylbenzene			0.01213	ethylbenzene			0.01213
xylenes			0.06066	xylenes			0.06066	xylenes			0.06066
naphthalene			0.00298	naphthalene			0.00298	naphthalene			0.00298
cumene			0.00383	cumene			0.00383	cumene			0.00383
Component Vapor pressure $P_{VA} = (0.019337)10^6 (A - (B/(TLA+C)))$				Component Vapor pressure $P_{VA} = (0.019337)10^6 (A - (B/(TLA+C)))$				Component Vapor pressure $P_{VA} = (0.019337)10^6 (A - (B/(TLA+C)))$			
hexane		A	6.878	hexane		A	6.878	hexane		A	6.878
benzene		B	1171.5	benzene		B	1171.5	benzene		B	1171.5
2,2,4 TMP		C	224.37	2,2,4 TMP		C	224.37	2,2,4 TMP		C	224.37
toluene		P_{VA}	2.9373	toluene		P_{VA}	2.8649	toluene		P_{VA}	2.3757
ethylbenzene			6.906	ethylbenzene			6.906	ethylbenzene			6.906
xylenes			1211	xylenes			1211	xylenes			1211
naphthalene			220.79	naphthalene			220.79	naphthalene			220.79
cumene			0.9583	cumene			0.9322	cumene			0.7579
hexane			7.017	hexane			7.017	hexane			7.017
ethylbenzene			1377.6	ethylbenzene			1377.6	ethylbenzene			1377.6
xylenes			222.64	xylenes			222.64	xylenes			222.64
naphthalene			0.5361	naphthalene			0.5361	naphthalene			0.5361
cumene			0.1781	cumene			0.1781	cumene			0.1781
hexane			6.95	hexane			6.95	hexane			6.95
ethylbenzene			1419.3	ethylbenzene			1419.3	ethylbenzene			1419.3
xylenes			212.61	xylenes			212.61	xylenes			212.61
naphthalene			0.1611	naphthalene			0.1558	naphthalene			0.1211
cumene			0.0050	cumene			0.0048	cumene			0.0035
hexane			6.929	hexane			6.929	hexane			6.929
ethylbenzene			1455.8	ethylbenzene			1455.8	ethylbenzene			1455.8
xylenes			207.2	xylenes			207.2	xylenes			207.2
naphthalene			0.0887	naphthalene			0.0856	naphthalene			0.0654
cumene				cumene				cumene			

MONTH October				MONTH November				MONTH December							
ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units				
Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D + L_P$)		LT	238.18	lb/month	Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D + L_P$)		LT	211.11	lb/month	Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D + L_P$)		LT	164.68	lb/month	
			0.12	tons/month				0.11	tons/month				0.08	tons/month	
Product Type			Gasoline - RVP 13.5		Product Type			Gasoline - RVP 15		Product Type			Gasoline - RVP 15		
Monthly Throughput (only change if actual is known)		Q_{month}	20,923.85	barrels/month	Monthly Throughput (only change if actual is known)		Q_{month}	20,923.85	barrels/month	Monthly Throughput (only change if actual is known)		Q_{month}	20,923.85	barrels/month	
Vapor Molecular weight		M_v	62.00		Vapor Molecular weight		M_v	60.15		Vapor Molecular weight		M_v	60.15		
Vapor Pressure Equation Constant A		A	11.63		Vapor Pressure Equation Constant A		A	11.60		Vapor Pressure Equation Constant A		A	11.60		
Vapor Pressure Equation Constant B		B	5015.72	$^{\circ}R$	Vapor Pressure Equation Constant B		B	4937.93	$^{\circ}R$	Vapor Pressure Equation Constant B		B	4937.93	$^{\circ}R$	
Daily total solar insolation on a horizontal surface		I	948.0	Btu/ft ² -day	Daily total solar insolation on a horizontal surface		I	621.0	Btu/ft ² -day	Daily total solar insolation on a horizontal surface		I	501.0	Btu/ft ² -day	
Average Daily Ambient Temperature Eq. 1-30					Average Daily Ambient Temperature Eq. 1-30					Average Daily Ambient Temperature Eq. 1-30					
TAA = ((TAX+TAN)/2)		T_{AA}	514.75	$^{\circ}R$	TAA = ((TAX+TAN)/2)		T_{AA}	505.35	$^{\circ}R$	TAA = ((TAX+TAN)/2)		T_{AA}	495.50	$^{\circ}R$	
Average daily maximum ambient temperature, Table 7.1-7		T_{AX}	522.40	$^{\circ}R$	Average daily maximum ambient temperature, Table 7.1-7		T_{AX}	512.10	$^{\circ}R$	Average daily maximum ambient temperature, Table 7.1-7		T_{AX}	501.80	$^{\circ}R$	
Average daily minimum ambient temperature, Table 7.1-7		T_{AN}	507.10	$^{\circ}R$	Average daily minimum ambient temperature, Table 7.1-7		T_{AN}	498.60	$^{\circ}R$	Average daily minimum ambient temperature, Table 7.1-7		T_{AN}	489.20	$^{\circ}R$	
Liquid Bulk Temperature Eq 1-31:					Liquid Bulk Temperature Eq 1-31:					Liquid Bulk Temperature Eq 1-31:					
TB = TAA + 0.003 as I		T_B	515.46		TB = TAA + 0.003 as I		T_B	505.82		TB = TAA + 0.003 as I		T_B	495.88		
Average Daily Liquid Surface Temperature Eq. 1-28					Average Daily Liquid Surface Temperature Eq. 1-28					Average Daily Liquid Surface Temperature Eq. 1-28					
TLA = 0.3*TAA + 0.7*TB + 0.004* α 1		T_{LA}	516.20	$^{\circ}R$	TLA = 0.3*TAA + 0.7*TB + 0.004* α 1		T_{LA}	506.30	$^{\circ}R$	TLA = 0.3*TAA + 0.7*TB + 0.004* α 1		T_{LA}	496.26	$^{\circ}R$	
True Vapor Pressure Eq. 1-25:					True Vapor Pressure Eq. 1-25:					True Vapor Pressure Eq. 1-25:					
PVA = exp(A-(B/TLA))		P_{VA}	6.790	psia	PVA = exp(A-(B/TLA))		P_{VA}	6.340	psia	PVA = exp(A-(B/TLA))		P_{VA}	5.205	psia	
Vapor pressure function Eq. 2-4:					Vapor pressure function Eq. 2-4:					Vapor pressure function Eq. 2-4:					
$P^* = P_{VA}/P_A/(1+(1-(P_{VA}/P_A))^{0.5})^2$		P^*	0.154	NA	$P^* = P_{VA}/P_A/(1+(1-(P_{VA}/P_A))^{0.5})^2$		P^*	0.140	NA	$P^* = P_{VA}/P_A/(1+(1-(P_{VA}/P_A))^{0.5})^2$		P^*	0.109	NA	
Rim Seal Losses Eq. 2-3:					Rim Seal Losses Eq. 2-3:					Rim Seal Losses Eq. 2-3:					
$L_R = ((K_{GA} + K_{GB}) \sqrt{DP^* M_v K_c}) / 12$ months		L_R	63.59	lb/month	$L_R = ((K_{GA} + K_{GB}) \sqrt{DP^* M_v K_c}) / 12$ months		L_R	56.26	lb/month	$L_R = ((K_{GA} + K_{GB}) \sqrt{DP^* M_v K_c}) / 12$ months		L_R	43.68	lb/month	
Withdrawal losses Eq. 2-19:					Withdrawal losses Eq. 2-19:					Withdrawal losses Eq. 2-19:					
$L_W = ((0.943)OCsW_j/D)^{1.1} (N_c F_j/D)$		L_W	3.38	lb/month	$L_W = ((0.943)OCsW_j/D)^{1.1} (N_c F_j/D)$		L_W	3.38	lb/month	$L_W = ((0.943)OCsW_j/D)^{1.1} (N_c F_j/D)$		L_W	3.38	lb/month	
Deck Fitting Losses Eq.2-13:					Deck Fitting Losses Eq.2-13:					Deck Fitting Losses Eq.2-13:					
$L_F = F_r P^* M_v K_c$		LF	115.57	lb/month	$L_F = F_r P^* M_v K_c$		LF	102.25	lb/month	$L_F = F_r P^* M_v K_c$		LF	79.39	lb/month	
Deck Seam Losses Eq. 2-18:					Deck Seam Losses Eq. 2-18:					Deck Seam Losses Eq. 2-18:					
$L_D = K_D S_D P^* M_v K_c / 12$ months		LD	55.64	lb/month	$L_D = K_D S_D P^* M_v K_c / 12$ months		LD	49.22	lb/month	$L_D = K_D S_D P^* M_v K_c / 12$ months		LD	38.22	lb/month	
HAPS Speciation				HAPS Speciation				HAPS Speciation							
Product - same as January			Gasoline	Product - same as January			Gasoline	Product - same as January			Gasoline	Product - same as January			Gasoline
Total HAP Monthly Emissions			5.196	lb/month	Total HAP Monthly Emissions			4.117	lb/month	Total HAP Monthly Emissions			3.077	lb/month	
Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{vi}L_W$					Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{vi}L_W$					Individual HAP Monthly Em Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{vi}L_W$					
	hexane	L_{Ti}	0.9297	lb/month		hexane	0.7321	lb/month		hexane	0.5305	lb/month			
	benzene	L_{Ti}	1.0423	lb/month		benzene	0.8124	lb/month		benzene	0.5853	lb/month			
	2,2,4 TMP	L_{Ti}	1.2415	lb/month		2,2,4 TMP	0.9730	lb/month		2,2,4 TMP	0.7129	lb/month			
	toluene	L_{Ti}	1.3032	lb/month		toluene	1.0260	lb/month		toluene	0.7679	lb/month			
	ethylbenzene	L_{Ti}	0.1133	lb/month		ethylbenzene	0.0942	lb/month		ethylbenzene	0.0776	lb/month			
	xylenes	L_{Ti}	0.5236	lb/month		xylenes	0.4401	lb/month		xylenes	0.3675	lb/month			
	naphthalene	L_{Ti}	0.0145	lb/month		naphthalene	0.0143	lb/month		naphthalene	0.0142	lb/month			
	cumene	L_{Ti}	0.0277	lb/month		cumene	0.0244	lb/month		cumene	0.0216	lb/month			
Vapor Weight Concentrations Eq. 40-6 $Z_{vi} = y_i M_i / M_v$					Vapor Weight Concentrations Eq. 40-6 $Z_{vi} = y_i M_i / M_v$					Vapor Weight Concentration $Z_{vi} = y_i M_i / M_v$					
	hexane	M_i	86.18			hexane	86.18			hexane	86.18				
	benzene	M_i	78.11			benzene	78.11			benzene	78.11				
	2,2,4 TMP	M_i	114.23			2,2,4 TMP	114.23			2,2,4 TMP	114.23				
	toluene	M_i	92.14			toluene	92.14			toluene	92.14				
	ethylbenzene	M_i	106.17			ethylbenzene	106.17			ethylbenzene	106.17				
	xylenes	M_i	106.17			xylenes	106.17			xylenes	106.17				
	naphthalene	M_i	128.17			naphthalene	128.17			naphthalene	128.17				
	cumene	M_i	120.19			cumene	120.19			cumene	120.19				
Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{VA}$					Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{VA}$					Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{VA}$					
	hexane	$P_i = P_{VA}(x_i)$	0.018638			hexane	0.014875			hexane	0.011186				
	benzene	P_{VA}	0.022527			benzene	0.017664			benzene	0.013033				
	2,2,4 TMP	y_i	0.017363			2,2,4 TMP	0.013463			2,2,4 TMP	0.009817				
	toluene	P_{VA}	0.020754			toluene	0.015726			toluene	0.011191				
	ethylbenzene	y_i	0.001114			ethylbenzene	0.000811			ethylbenzene	0.000553				
	xylenes	P_{VA}	0.004845			xylenes	0.003518			xylenes	0.002391				
	naphthalene	y_i	0.000006			naphthalene	0.000004			naphthalene	0.000002				
	cumene	P_{VA}	0.000161			cumene	0.000114			cumene	0.000075				
Liquid Mole Fraction Eq. 40-4 $x_i = (Z_{vi} M_i) / M_i$					Liquid Mole Fraction Eq. 40-4 $x_i = (Z_{vi} M_i) / M_i$					Liquid Mole Fraction Eq. 40-4 $x_i = (Z_{vi} M_i) / M_i$					
	hexane	Z_{vi}	0.01			hexane	0.01			hexane	0.01				
	benzene	M_i	0.018			benzene	0.018			benzene	0.018				
	2,2,4 TMP	M_i	0.04			2,2,4 TMP	0.04			2,2,4 TMP	0.04				
	toluene	M_i	0.07			toluene	0.07			toluene	0.07				
	ethylbenzene	M_i	0.014			ethylbenzene	0.014			ethylbenzene	0.014				
	xylenes	M_i	0.07			xylenes	0.07			xylenes	0.07				
	naphthalene	M_i	0.00415			naphthalene	0.00415			naphthalene	0.00415				
	cumene	M_i	0.005			cumene	0.005			cumene	0.005				
Component Vapor pressure $P_{VA} = (0.019337)10^4(A-(B/(TLA+C)))$					Component Vapor pressure $P_{VA} = (0.019337)10^4(A-(B/(TLA+C)))$					Component Vapor pressure $P_{VA} = (0.019337)10^4(A-(B/(TLA+C)))$					
	hexane	A	6.878			hexane	6.878			hexane	6.878				
	benzene	B	1171.5			benzene	1211			benzene	1211				
	2,2,4 TMP	C	220.79			2,2,4 TMP	220.79			2,2,4 TMP	220.79				
	toluene	P_{VA}	6.812			toluene	6.812			toluene	6.812				
	ethylbenzene	A	7.017			ethylbenzene	7.017			ethylbenzene	7.017				
	xylenes	B	1377.6			xylenes	1462.3			xylenes	1462.3				
	naphthalene	C	211.82			naphthalene	211.82			naphthalene	211.82				
	cumene	P_{VA}	6.929			cumene	6.929			cumene	6.929				

MONTHLY IFR TANK VOC AND HAP ESTIMATIONS

INPUT DATA				MONTH January				MONTH February				MONTH March			
Tank No.	Symbol	Units		Symbol	Units	Symbol	Units	Symbol	Units	Symbol	Units	Symbol	Units		
30535															
Nearest US Location		Bridgeport, CT		Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D + L_C$)	LT	711.12	lb/month	Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D + L_C$)	LT	749.37	lb/month	Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D + L_C$)	LT	894.55	lb/month
Absolute Pressure	P_A	14.69	psi	Product Type		Gasoline - RVP 15		Product Type		Gasoline - RVP 15		Product Type		Gasoline - RVP 15	
Product Information				Monthly Throughput (only change if actual is known)	Q_{month}	147,043.02	barrels/month	Monthly Throughput (only change if actual is known)	Q_{month}	147,043.02	barrels/month	Monthly Throughput (only change if actual is known)	Q_{month}	147,043.02	barrels/month
Average organic liquid density	W_L	5.60	lb/gal	Vapor Molecular weight	M_v	60.15		Vapor Molecular weight	M_v	60.15		Vapor Molecular weight	M_v	60.15	
Average Reid Vapor Pressure	RVP	13.00		Vapor Pressure Equation Constant A	A	11.60		Vapor Pressure Equation Constant A	A	11.60		Vapor Pressure Equation Constant A	A	11.60	
Product factor, 0.4 for crude oils or 1 for other organic liquids	K_c	1.00		Vapor Pressure Equation Constant B	B	4937.93	$^{\circ}R$	Vapor Pressure Equation Constant B	B	4937.93	$^{\circ}R$	Vapor Pressure Equation Constant B	B	4937.93	$^{\circ}R$
Tank design data				Daily total solar insolation on a horizontal surface	I	560.0	Btu/ft ² -day	Daily total solar insolation on a horizontal surface	I	847.0	Btu/ft ² -day	Daily total solar insolation on a horizontal surface	I	1156.0	Btu/ft ² -day
Shell height	Hs	48.00	ft	Average Daily Ambient Temperature Eq. 1-30	T_{AA}	490.50	$^{\circ}R$	Average Daily Ambient Temperature Eq. 1-30	T_{AA}	492.20	$^{\circ}R$	Average Daily Ambient Temperature Eq. 1-30	T_{AA}	498.90	$^{\circ}R$
Diameter	D	134.00	ft	$T_{AA} = ((TAX+TAN)/2)$				$T_{AA} = ((TAX+TAN)/2)$				$T_{AA} = ((TAX+TAN)/2)$			
Throughput	Q	6,175,807	gal/month	Average daily maximum ambient temperature, Table 7.1-7	T_{AX}	496.90	$^{\circ}R$	Average daily maximum ambient temperature, Table 7.1-7	T_{AX}	498.80	$^{\circ}R$	Average daily maximum ambient temperature, Table 7.1-7	T_{AX}	506.00	$^{\circ}R$
Maximum Filling Height (use Hs-1 if unknown)	H_{Lx}	47.00	ft	Average daily minimum ambient temperature, Table 7.1-7	T_{AN}	484.10	$^{\circ}R$	Average daily minimum ambient temperature, Table 7.1-7	T_{AN}	485.60	$^{\circ}R$	Average daily minimum ambient temperature, Table 7.1-7	T_{AN}	491.80	$^{\circ}R$
Minimum Filling Height (use Hs-1 if unknown)	H_{Lx}	1.00	ft	Liquid Bulk Temperature Eq. 1-31:	T_B	490.92		Liquid Bulk Temperature Eq. 1-31:	T_B	492.84		Liquid Bulk Temperature Eq. 1-31:	T_B	499.77	
Liquid height (assume 1/2 Hs)	H_L	24.00	ft	$T_B = T_{AA} + 0.003 \text{ as I}$				$T_B = T_{AA} + 0.003 \text{ as I}$				$T_B = T_{AA} + 0.003 \text{ as I}$			
Tank Construction (pick from drop down list)		Welded		Average Daily Liquid Surface Temperature Eq. 2-6	T_{LA}	491.35	$^{\circ}R$	Average Daily Liquid Surface Temperature Eq. 1-28	T_{LA}	493.49	$^{\circ}R$	Average Daily Liquid Surface Temperature Eq. 1-28	T_{LA}	500.66	$^{\circ}R$
Tank Color (pick from drop down list)		White		$T_{LA} = 0.3T_{AA} + 0.7T_B + 0.004 \alpha^1$				$T_{LA} = 0.3T_{AA} + 0.7T_B + 0.004 \alpha^1$				$T_{LA} = 0.3T_{AA} + 0.7T_B + 0.004 \alpha^1$			
Tank Shell Condition (pick from drop down list)		Average		True Vapor Pressure Eq. 1-25:	P_{VA}	4.713	psia	True Vapor Pressure Eq. 1-25:	P_{VA}	4.922	psia	True Vapor Pressure Eq. 1-25:	P_{VA}	5.681	psia
Tank Interior Condition (pick from drop down list)		Light Rust		$P_{VA} = \exp(A - (B/TLA))$				$P_{VA} = \exp(A - (B/TLA))$				$P_{VA} = \exp(A - (B/TLA))$			
Tank paint solar absorptance, dimensionless, Table 7.1-6	α	0.25		Vapor pressure function Eq. 2-4:	P^*	0.096	NA	Vapor pressure function Eq. 2-4:	P^*	0.102	NA	Vapor pressure function Eq. 2-4:	P^*	0.122	NA
				$P^* = P_{VA}/P_A / (1 + (1 - (P_{VA}/P_A))^{0.5})^2$				$P^* = P_{VA}/P_A / (1 + (1 - (P_{VA}/P_A))^{0.5})^2$				$P^* = P_{VA}/P_A / (1 + (1 - (P_{VA}/P_A))^{0.5})^2$			
Internal floating roof design data				Rim Seal Losses Eq. 2-3:	L_R	103.61	lb/month	Rim Seal Losses Eq. 2-3:	L_R	109.26	lb/month	Rim Seal Losses Eq. 2-3:	L_R	130.71	lb/month
Rim Seal Type:		Mechanical-shoe seal		$L_R = ((K_{S1} + K_{S2}) \sqrt{DP^* M_v K_c}) / 12 \text{ months}$				$L_R = ((K_{S1} + K_{S2}) \sqrt{DP^* M_v K_c}) / 12 \text{ months}$				$L_R = ((K_{S1} + K_{S2}) \sqrt{DP^* M_v K_c}) / 12 \text{ months}$			
Rim Seal Fit (Average or Tight fitting)		Average		Withdrawal losses Eq. 2-19:	L_W	9.73	lb/month	Withdrawal losses Eq. 2-19:	L_W	9.73	lb/month	Withdrawal losses Eq. 2-19:	L_W	9.73	lb/month
Number of fixed roof support columns	Nc	16.00	NA	$L_W = (((0.943)OCsW_v) / D) [1 + (N_F/D)]$				$L_W = (((0.943)OCsW_v) / D) [1 + (N_F/D)]$				$L_W = (((0.943)OCsW_v) / D) [1 + (N_F/D)]$			
Effective column diameter (1.1 for 8x7 in. built up columns; 0.7 for 8 in. pipe columns; 1.0 for 8 in. pipe columns)	Fc	1.00	ft	Deck Fitting Losses Eq. 2-13:	LF	354.81	lb/month	Deck Fitting Losses Eq. 2-13:	LF	374.16	lb/month	Deck Fitting Losses Eq. 2-13:	LF	447.60	lb/month
Deck seam loss per unit seam length factor, 0.0 or 0.14	KD	0.14	lb-mole/ft-yr	$L_F = F_F P^* M_v K_c$				$L_F = F_F P^* M_v K_c$				$L_F = F_F P^* M_v K_c$			
Zero wind speed LR factor, see Table 7.1-8	KRa	1.6	lb-mole/ft-yr	Deck Seam Losses Eq. 2-18:	LD	242.97	lb/month	Deck Seam Losses Eq. 2-18:	LD	256.22	lb/month	Deck Seam Losses Eq. 2-18:	LD	306.51	lb/month
Wind speed dependent LR factor, see Table 7.1-8	KRb	0.3	lb-mole/(mph) ^{1.75} yr	$L_D = K_D S_D^2 P^* M_v K_c / 12 \text{ months}$				$L_D = K_D S_D^2 P^* M_v K_c / 12 \text{ months}$				$L_D = K_D S_D^2 P^* M_v K_c / 12 \text{ months}$			
Average ambient wind speed at tank site, for IFR use Zero	v	0.0	mph	HAPS Speciation				HAPS Speciation				HAPS Speciation			
Seal-related wind speed exponent, see Table 7.1-8	n	1.6	NA	Product - select from list		Gasoline		Product - same as January		Gasoline		Product - same as January		Gasoline	
Shell clingage factor, see Table 7.1-10	Cs	0.0015	bb/1,000 ft ²	Total HAP Monthly Emissions		11.636	lb/month	Total HAP Monthly Emissions		12.419	lb/month	Total HAP Monthly Emissions		15.537	lb/month
Deck Design Data				Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{Li}L_W$	L_{Ti}			Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{Li}L_W$	L_{Ti}			Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{Li}L_W$	L_{Ti}		
Deck Seam (choose Welded or Bolted)		Bolted		hexane	2.1615	lb/month		hexane	2.3177	lb/month		hexane	2.9307	lb/month	
Select Deck Construction Type		Continuous sheet		benzene	2.3338	lb/month		benzene	2.5071	lb/month		benzene	3.1927	lb/month	
If bolted continuous sheet or panel, enter width		5	ft	TMP	2.7526	lb/month		TMP	2.9492	lb/month		TMP	3.7307	lb/month	
If bolted panel, also enter length		0	ft	toluene	2.8278	lb/month		toluene	3.0189	lb/month		toluene	3.7871	lb/month	
Deck seam length factor: Length of Seam / Area of Deck	SD	0.20	ft/ft ²	ethylbenzene	0.2557	lb/month		ethylbenzene	0.2676	lb/month		ethylbenzene	0.3164	lb/month	
Deck Fitting Data				xylenes	1.1972	lb/month		xylenes	1.2490	lb/month		xylenes	1.4616	lb/month	
Access Hatch Bolted cover, gasketed	Qty	2	1.6	naphthalene	0.0410	lb/month		naphthalene	0.0410	lb/month		naphthalene	0.0414	lb/month	
Column Well Bolted cover, gasketed sliding cover	16	33.0		cumene	0.0668	lb/month		cumene	0.0687	lb/month		cumene	0.0768	lb/month	
Unslotted Guidepole and Well Gasketed sliding cover w/pole sleeve	0	8.6		Vapor Weight Concentrations Eq. 40-4 $Z_{vi} = y_i M_i / M_v$				Vapor Weight Concentrations Eq. 40-4 $Z_{vi} = y_i M_i / M_v$				Vapor Weight Concentrations Eq. 40-4 $Z_{vi} = y_i M_i / M_v$			
Slotted guidepole/sample well Gasketed sliding cover, with pole sleeve	0	11.0		hexane	86.18	60	0.00294	hexane	86.18	60	0.00300	hexane	86.18	60	0.00320
Gauge-float well (automatic g) Bolted cover, gasketed	0	2.8		benzene	78.11	60	0.00308	benzene	78.11	60	0.00315	benzene	78.11	60	0.00341
Gauge-hatch/sample port Slit fabric seal, 10% open area	2	12.0		2,2,4 TMP	114.23	60	0.00337	2,2,4 TMP	114.23	60	0.00346	2,2,4 TMP	114.23	60	0.00378
Vacuum Breaker Weighted mechanical actuation, gasketed	1	6.2		toluene	92.14	60	0.00306	toluene	92.14	60	0.00316	toluene	92.14	60	0.00351
Deck drain Stub drain (1-inch diameter)	144	1.2		ethylbenzene	106.17	60	0.00017	ethylbenzene	106.17	60	0.00018	ethylbenzene	106.17	60	0.00020
Legs (IFR type) IFR type, Adjustable	0	7.9		xylenes	106.17	60	0.00074	xylenes	106.17	60	0.00077	xylenes	106.17	60	0.00088
Rim Vent Weighted mechanical actuation, gasketed	0	0.7		naphthalene	128.17	60	0.00000	naphthalene	128.17	60	0.00000	naphthalene	128.17	60	0.00000
Ladder Sliding cover, gasketed	0	56.0		cumene	120.19	60	0.00003	cumene	120.19	60	0.00003	cumene	120.19	60	0.00003
Ladder / Guide-Pole Combin Ladder sleeve, gasketed sliding cover	0	60.0		Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{VA}$				Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{VA}$				Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{VA}$			
Monthly deck fitting loss factor	F_F	61.18	per month	hexane	0.009680	4.713	0.00205	hexane	0.010314	4.922	0.00210	hexane	0.012697	5.681	0.00224
				benzene	0.011169	4.713	0.00237	benzene	0.011951	4.922	0.00243	benzene	0.014919	5.681	0.00263
				2,2,4 TMP	0.008362	4.713	0.00177	2,2,4 TMP	0.008971	4.922	0.00182	2,2,4 TMP	0.011297	5.681	0.00199
				toluene	0.009416	4.713	0.00200	toluene	0.010156	4.922	0.00206	toluene	0.013018	5.681	0.00229
				ethylbenzene	0.000455	4.713	0.00010	ethylbenzene	0.000495	4.922	0.00010	ethylbenzene	0.000655	5.681	0.00012
				xylenes	0.001965	4.713	0.00042	xylenes	0.002141	4.922	0.00044	xylenes	0.002839	5.681	0.00050
				naphthalene	0.000002	4.713	0.00000	naphthalene	0.000002	4.922	0.00000	naphthalene	0.000003	5.681	0.00000
				cumene	0.000061	4.713	0.00001	cumene	0.000067	4.922	0.00001	cumene	0.000090	5.681	0.00002
				Liquid Mole Fraction Eq. 40-4 $X_i = (Z_{Li} M_i) / M_L$				Liquid Mole Fraction Eq. 40-4 $X_i = (Z_{Li} M_i) / M_L$				Liquid Mole Fraction Eq. 40-4 $X_i = (Z_{Li} M_i) / M_L$			
				hexane	0.01	96	0.01114	hexane	0.01	96	0.01114	hexane	0.01	96	0.01114
				benzene	0.018	96	0.02212	benzene	0.018	96	0.02212	benzene	0.018	96	0.02212
				2,2,4 TMP	0.04	96	0.03362	2,2,4 TMP	0.04	96	0.03362	2,2,4 TMP	0.04	96	0.03362
				toluene	0.07	96	0.07293	toluene	0.07	96	0.07293	toluene	0.07	96	0.07293
				ethylbenzene	0.014	96	0.01266	ethylbenzene	0.014	96	0.01266	ethylbenzene	0.014	96	0.01266
				xylenes	0.07	96	0.06329	xylenes	0.07	96	0.06329	xylenes	0.07	96	0.06329
				naphthalene	0.00415	96	0.00311	naphthalene	0.00415	96	0.00311	naphthalene	0.00415	96	0.00311
				cumene	0.005	96	0.00399	cumene	0.005	96	0.00399	cumene	0.005	96	0.00399
				Component Vapor pressure $P_{VA} = (0.019337)10^4(A - (B/(TLA+C)))$				Component Vapor pressure $P_{VA} = (0.019337)10^4(A - (B/(TLA+C)))$				Component Vapor pressure $P_{VA} = (0.019337)10^4(A - (B/(TLA+C)))$			
				hexane	6.878	1171.5	224.37	hexane	6.878	1171.5	224.37	hexane	6.878	1171.5	224.37
				benzene	6.906	1211	220.79	benzene	6.906	1211	220.79	benzene	6.906	1211	220.79
				2,2,4 TMP	6.812	1257.8	220.74	2,2,4 TMP	6.812	1257.8	220.74	2,2,4 TMP	6.812	1257.8	220.74

MONTH April				MONTH May				MONTH June			
ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units
Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_F + L_D$)		LT	1,031.45 lb/month	Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_F + L_D$)		LT	812.92 lb/month	Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_F + L_D$)		LT	1,033.22 lb/month
			0.52 tons/month				0.41 tons/month				0.52 tons/month
Product Type		Gasoline - RVP 13.5		Product Type		Gasoline - RVP 9		Product Type		Gasoline - RVP 9	
Monthly Throughput (only change if actual is known)		Q_{month}	147,043.02 barrels/month	Monthly Throughput (only change if actual is known)		Q_{month}	147,043.02 barrels/month	Monthly Throughput (only change if actual is known)		Q_{month}	147,043.02 barrels/month
Vapor Molecular weight		M_v	62.00	Vapor Molecular weight		M_v	68.00	Vapor Molecular weight		M_v	68.00
Vapor Pressure Equation Constant A		A	11.63	Vapor Pressure Equation Constant A		A	11.76	Vapor Pressure Equation Constant A		A	11.76
Vapor Pressure Equation Constant B		B	5015.72 °R	Vapor Pressure Equation Constant B		B	5315.06 °R	Vapor Pressure Equation Constant B		B	5315.06 °R
Daily total solar insolation on a horizontal surface		I	1490.0 Btu/ft ² -day	Daily total solar insolation on a horizontal surface		I	1750.0 Btu/ft ² -day	Daily total solar insolation on a horizontal surface		I	1862.0 Btu/ft ² -day
Average Daily Ambient Temperature Eq. 1-30				Average Daily Ambient Temperature Eq. 1-30				Average Daily Ambient Temperature Eq. 1-30			
TAA = ((TAX+TAN)/2)		T_{AA}	509.15 °R	TAA = ((TAX+TAN)/2)		T_{AA}	518.65 °R	TAA = ((TAX+TAN)/2)		T_{AA}	528.60 °R
Average daily maximum ambient temperature, Table 7.1		T_{AX}	516.80 °R	Average daily maximum ambient temperature, Table 7.1-7		T_{AX}	526.50 °R	Average daily maximum ambient temperature, Table 7.1-7		T_{AX}	536.10 °R
Average daily minimum ambient temperature, Table 7.1		T_{AN}	501.50 °R	Average daily minimum ambient temperature, Table 7.1-7		T_{AN}	510.80 °R	Average daily minimum ambient temperature, Table 7.1-7		T_{AN}	521.10 °R
Liquid Bulk Temperature Eq. 1-31:				Liquid Bulk Temperature Eq. 1-31:				Liquid Bulk Temperature Eq. 1-31:			
TB = TAA + 0.003 cs I		T_B	510.27	TB = TAA + 0.003 cs I		T_B	519.96	TB = TAA + 0.003 cs I		T_B	530.00
Average Daily Liquid Surface Temperature Eq. 1-28				Average Daily Liquid Surface Temperature Eq. 1-28				Average Daily Liquid Surface Temperature Eq. 1-28			
TLA = 0.3*TAA + 0.7*TB + 0.004*αI		T_{LA}	511.42 °R	TLA = 0.3*TAA + 0.7*TB + 0.004*αI		T_{LA}	521.32 °R	TLA = 0.3*TAA + 0.7*TB + 0.004*αI		T_{LA}	531.44 °R
True Vapor Pressure Eq. 1-25:				True Vapor Pressure Eq. 1-25:				True Vapor Pressure Eq. 1-25:			
PvA = exp(A-(B/TLA))		P_{vA}	6.201 psia	PvA = exp(A-(B/TLA))		P_{vA}	4.763 psia	PvA = exp(A-(B/TLA))		P_{vA}	5.783 psia
Vapor pressure function Eq. 2-4:				Vapor pressure function Eq. 2-4:				Vapor pressure function Eq. 2-4:			
$P^* = P_{vA}/P_A/(1+(1-(P_{vA}/P_A))^{0.5})^2$		P^*	0.136 NA	$P^* = P_{vA}/P_A/(1+(1-(P_{vA}/P_A))^{0.5})^2$		P^*	0.098 NA	$P^* = P_{vA}/P_A/(1+(1-(P_{vA}/P_A))^{0.5})^2$		P^*	0.124 NA
Rim Seal Losses Eq. 2-3:				Rim Seal Losses Eq. 2-3:				Rim Seal Losses Eq. 2-3:			
$L_R = ((K_{R1} + K_{R2} \sqrt{V})/DP^* M_v K_c)/12$ months		L_R	150.93 lb/month	$L_R = ((K_{R1} + K_{R2} \sqrt{V})/DP^* M_v K_c)/12$ months		L_R	118.65 lb/month	$L_R = ((K_{R1} + K_{R2} \sqrt{V})/DP^* M_v K_c)/12$ months		L_R	151.19 lb/month
Withdrawal losses Eq. 2-19:				Withdrawal losses Eq. 2-19:				Withdrawal losses Eq. 2-19:			
$L_W = (((0.943)QC/W)/D)^{0.5} * (1 + (N_c F_w/D))$		L_W	9.73 lb/month	$L_W = (((0.943)QC/W)/D)^{0.5} * (1 + (N_c F_w/D))$		L_W	9.73 lb/month	$L_W = (((0.943)QC/W)/D)^{0.5} * (1 + (N_c F_w/D))$		L_W	9.73 lb/month
Deck Fitting Losses Eq. 2-13:				Deck Fitting Losses Eq. 2-13:				Deck Fitting Losses Eq. 2-13:			
$L_F = F_r P^* M_v K_c$		LF	516.85 lb/month	$L_F = F_r P^* M_v K_c$		LF	406.31 lb/month	$L_F = F_r P^* M_v K_c$		LF	517.75 lb/month
Deck Seam Losses Eq. 2-18:				Deck Seam Losses Eq. 2-18:				Deck Seam Losses Eq. 2-18:			
$L_D = K_c S_r D^2 P^* M_v K_c/12$ months		LD	353.93 lb/month	$L_D = K_c S_r D^2 P^* M_v K_c/12$ months		LD	278.23 lb/month	$L_D = K_c S_r D^2 P^* M_v K_c/12$ months		LD	354.55 lb/month
HAPS Speciation				HAPS Speciation				HAPS Speciation			
Product - same as January		Gasoline		Product - same as January		Gasoline		Product - same as January		Gasoline	
Total HAP Monthly Emissions			20.485 lb/month	Total HAP Monthly Emissions			25.046 lb/month	Total HAP Monthly Emissions			34.090 lb/month
Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{Li}L_W$				Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{Li}L_W$				Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{Li}L_W$			
hexane		L_{Ti}	3.8540 lb/month	hexane		L_{Ti}	4.6517 lb/month	hexane		L_{Ti}	6.2681 lb/month
benzene			4.2561 lb/month	benzene			5.2081 lb/month	benzene			7.1082 lb/month
2,2,4 TMP			4.9648 lb/month	2,2,4 TMP			6.0941 lb/month	2,2,4 TMP			8.3318 lb/month
toluene			5.0444 lb/month	toluene			6.2452 lb/month	toluene			8.6007 lb/month
ethylbenzene			0.4010 lb/month	ethylbenzene			0.4871 lb/month	ethylbenzene			0.6544 lb/month
xylenes			1.8313 lb/month	xylenes			2.2098 lb/month	xylenes			2.9454 lb/month
naphthalene			0.0420 lb/month	naphthalene			0.0428 lb/month	naphthalene			0.0444 lb/month
cumene			0.0913 lb/month	cumene			0.1067 lb/month	cumene			0.1367 lb/month
Vapor Weight Concentrations Eq. 40-4 $Z_{vi} = y_i M_i / M_v$				Vapor Weight Concentrations Eq. 40-4 $Z_{vi} = y_i M_i / M_v$				Vapor Weight Concentrations Eq. 40-4 $Z_{vi} = y_i M_i / M_v$			
hexane		M_i	86.18	hexane		M_i	86.18	hexane		M_i	86.18
benzene		M_v	62	benzene		M_v	68	benzene		M_v	68
2,2,4 TMP		Z_{vi}	0.00368	2,2,4 TMP		Z_{vi}	0.00567	2,2,4 TMP		Z_{vi}	0.00603
toluene			0.00399	toluene			0.00627	toluene			0.00677
ethylbenzene			0.00448	ethylbenzene			0.00710	ethylbenzene			0.00776
xylenes			0.00427	xylenes			0.00693	xylenes			0.00774
naphthalene			0.00026	naphthalene			0.00044	naphthalene			0.00051
cumene			0.00113	cumene			0.00190	cumene			0.00221
			0.00000				0.00000				0.00000
			0.00004				0.00007				0.00009
Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{vA}$				Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{vA}$				Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{vA}$			
hexane		$P_i = P_{vA}(x_i)$	6.201	hexane		$P_i = P_{vA}(x_i)$	4.763	hexane		$P_i = P_{vA}(x_i)$	5.783
benzene		P_{vA}	0.00265	benzene		P_{vA}	0.00447	benzene		P_{vA}	0.00476
2,2,4 TMP		y_i	0.00317	2,2,4 TMP		y_i	0.00546	2,2,4 TMP		y_i	0.00590
toluene			0.00243	toluene			0.00423	toluene			0.00462
ethylbenzene			0.00287	ethylbenzene			0.00511	ethylbenzene			0.00571
xylenes			0.00015	xylenes			0.00028	xylenes			0.00032
naphthalene			0.00066	naphthalene			0.00122	naphthalene			0.00142
cumene			0.00000	cumene			0.00000	cumene			0.00000
			0.00002				0.00004				0.00005
Liquid Mole Fraction Eq. 40-4 $x_i = (Z_{Li} M_i) / M_i$				Liquid Mole Fraction Eq. 40-4 $x_i = (Z_{Li} M_i) / M_i$				Liquid Mole Fraction Eq. 40-4 $x_i = (Z_{Li} M_i) / M_i$			
hexane		Z_{Li}	0.01	hexane		Z_{Li}	0.01	hexane		Z_{Li}	0.01
benzene		M_i	92	benzene		M_i	92	benzene		M_i	92
2,2,4 TMP		M_i	86.18	2,2,4 TMP		M_i	86.18	2,2,4 TMP		M_i	86.18
toluene		X_i	0.01068	toluene		X_i	0.01068	toluene		X_i	0.01068
ethylbenzene			0.02120	ethylbenzene			0.02120	ethylbenzene			0.02120
xylenes			0.03222	xylenes			0.03222	xylenes			0.03222
naphthalene			0.06989	naphthalene			0.06989	naphthalene			0.06989
cumene			0.01213	cumene			0.01213	cumene			0.01213
			0.06066				0.06066				0.06066
			0.00298				0.00298				0.00298
			0.00000				0.00000				0.00000
			0.00005				0.00005				0.00005
			0.00383				0.00383				0.00383
Component Vapor pressure $P_{vA} = (0.019337)10^4(A-(B/(TLA+C)))$				Component Vapor pressure $P_{vA} = (0.019337)10^4(A-(B/(TLA+C)))$				Component Vapor pressure $P_{vA} = (0.019337)10^4(A-(B/(TLA+C)))$			
hexane		A	6.878	hexane		A	6.878	hexane		A	6.878
benzene		B	1171.5	benzene		B	1171.5	benzene		B	1171.5
2,2,4 TMP		C	224.37	2,2,4 TMP		C	224.37	2,2,4 TMP		C	224.37
toluene		P_{vA}	1.5366	toluene		P_{vA}	1.9962	toluene		P_{vA}	2.5773
ethylbenzene			0.9273	ethylbenzene			1.2255	ethylbenzene			1.6087
xylenes			0.4679	xylenes			0.6251	xylenes			0.8293
naphthalene			0.2550	naphthalene			0.3484	naphthalene			0.4725
cumene			0.0773	cumene			0.1098	cumene			0.1546
			0.0672				0.0957				0.1351
			0.0016				0.0026				0.0040
			0.0349				0.0509				0.0735

MONTH July				MONTH August				MONTH September			
ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units
Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D$)		LT	1,175.98 lb/month	Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D$)		LT	1,146.81 lb/month	Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D$)		LT	1,594.22 lb/month
			0.59 tons/month				0.57 tons/month				0.80 tons/month
Product Type			Gasoline - RVP 9	Product Type			Gasoline - RVP 9	Product Type			Gasoline - RVP 13.5
Monthly Throughput (only change if actual is known)		Q_{month}	147,043.02 barrels/month	Monthly Throughput (only change if actual is known)		Q_{month}	147,043.02 barrels/month	Monthly Throughput (only change if actual is known)		Q_{month}	147,043.02 barrels/month
Vapor Molecular weight		M_v	68.00	Vapor Molecular weight		M_v	68.00	Vapor Molecular weight		M_v	62.00
Vapor Pressure Equation Constant A		A	11.76	Vapor Pressure Equation Constant A		A	11.76	Vapor Pressure Equation Constant A		A	11.63
Vapor Pressure Equation Constant B		B	5315.06	Vapor Pressure Equation Constant B		B	5315.06	Vapor Pressure Equation Constant B		B	5015.72
Daily total solar insolation on a horizontal surface		I	1904.0 Btu/ft ² -day	Daily total solar insolation on a horizontal surface		I	1685.0 Btu/ft ² -day	Daily total solar insolation on a horizontal surface		I	1320.0 Btu/ft ² -day
Average Daily Ambient Temperature Eq. 1-30				Average Daily Ambient Temperature Eq. 1-30				Average Daily Ambient Temperature Eq. 1-30			
TAA = ((TAX+TAN)/2)		T_{AA}	533.90 °R	TAA = ((TAX+TAN)/2)		T_{AA}	533.20 °R	TAA = ((TAX+TAN)/2)		T_{AA}	526.15 °R
Average daily maximum ambient temperature, Table 7.1-7		T_{AX}	541.10 °R	Average daily maximum ambient temperature, Table 7.1-7		T_{AX}	540.10 °R	Average daily maximum ambient temperature, Table 7.1-7		T_{AX}	533.40 °R
Average daily minimum ambient temperature, Table 7.1-7		T_{AN}	526.70 °R	Average daily minimum ambient temperature, Table 7.1-7		T_{AN}	526.30 °R	Average daily minimum ambient temperature, Table 7.1-7		T_{AN}	518.90 °R
Liquid Bulk Temperature Eq. 1-31:				Liquid Bulk Temperature Eq. 1-31:				Liquid Bulk Temperature Eq. 1-31:			
TB = TAA + 0.003 as l		T_B	535.33	TB = TAA + 0.003 as l		T_B	534.46	TB = TAA + 0.003 as l		T_B	527.14
Average Daily Liquid Surface Temperature Eq. 1-28				Average Daily Liquid Surface Temperature Eq. 1-28				Average Daily Liquid Surface Temperature Eq. 1-28			
TLA = 0.3TAA + 0.7TB + 0.004αl		T_{LA}	536.80 °R	TLA = 0.3TAA + 0.7TB + 0.004αl		T_{LA}	535.77 °R	TLA = 0.3TAA + 0.7TB + 0.004αl		T_{LA}	528.16 °R
True Vapor Pressure Eq. 1-25:				True Vapor Pressure Eq. 1-25:				True Vapor Pressure Eq. 1-25:			
PvA = exp(A-(B/TLA))		P_{vA}	6.391 psia	PvA = exp(A-(B/TLA))		P_{vA}	6.270 psia	PvA = exp(A-(B/TLA))		P_{vA}	8.462 psia
Vapor pressure function Eq. 2-4:				Vapor pressure function Eq. 2-4:				Vapor pressure function Eq. 2-4:			
$P^* = P_{vA}/P_A/(1+(1-(P_{vA}/P_A))^{0.5})^2$		P^*	0.142 NA	$P^* = P_{vA}/P_A/(1+(1-(P_{vA}/P_A))^{0.5})^2$		P^*	0.138 NA	$P^* = P_{vA}/P_A/(1+(1-(P_{vA}/P_A))^{0.5})^2$		P^*	0.211 NA
Rim Seal Losses Eq. 2-3:				Rim Seal Losses Eq. 2-3:				Rim Seal Losses Eq. 2-3:			
$L_R = ((K_{RB} + K_{RB} V^2) DP^* M_v K_v) / 12 \text{ months}$		L_R	172.28 lb/month	$L_R = ((K_{RB} + K_{RB} V^2) DP^* M_v K_v) / 12 \text{ months}$		L_R	167.97 lb/month	$L_R = ((K_{RB} + K_{RB} V^2) DP^* M_v K_v) / 12 \text{ months}$		L_R	234.06 lb/month
Withdrawal losses Eq. 2-19:				Withdrawal losses Eq. 2-19:				Withdrawal losses Eq. 2-19:			
$L_W = ((0.943/QCsw) D^3) [1 + (N_v F_v D)]$		L_W	9.73 lb/month	$L_W = ((0.943/QCsw) D^3) [1 + (N_v F_v D)]$		L_W	9.73 lb/month	$L_W = ((0.943/QCsw) D^3) [1 + (N_v F_v D)]$		L_W	9.73 lb/month
Deck Fitting Losses Eq.2-13:				Deck Fitting Losses Eq.2-13:				Deck Fitting Losses Eq.2-13:			
$L_F = F_f P^* M_v K_v$		LF	589.97 lb/month	$L_F = F_f P^* M_v K_v$		LF	575.21 lb/month	$L_F = F_f P^* M_v K_v$		LF	801.54 lb/month
Deck Seam Losses Eq. 2-18:				Deck Seam Losses Eq. 2-18:				Deck Seam Losses Eq. 2-18:			
$L_D = K_v S_v D^2 P^* M_v K_v / 12 \text{ months}$		LD	404.00 lb/month	$L_D = K_v S_v D^2 P^* M_v K_v / 12 \text{ months}$		LD	393.89 lb/month	$L_D = K_v S_v D^2 P^* M_v K_v / 12 \text{ months}$		LD	548.88 lb/month
HAPS Speciation				HAPS Speciation				HAPS Speciation			
Product - same as January			Gasoline	Product - same as January			Gasoline	Product - same as January			Gasoline
Total HAP Monthly Emissions			40.260 lb/month	Total HAP Monthly Emissions			38.982 lb/month	Total HAP Monthly Emissions			35.979 lb/month
Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{vi}L_W$				Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{vi}L_W$				Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{vi}L_W$			
hexane		L_{Ti}	7.3489 lb/month	hexane		L_{Ti}	7.1263 lb/month	hexane		L_{Ti}	6.6982 lb/month
benzene			8.3912 lb/month	benzene			8.1262 lb/month	benzene			7.5525 lb/month
2,2,4 TMP			9.8529 lb/month	2,2,4 TMP			9.5382 lb/month	2,2,4 TMP			8.8122 lb/month
toluene			10.2250 lb/month	toluene			9.8876 lb/month	toluene			9.0208 lb/month
ethylbenzene			0.7725 lb/month	ethylbenzene			0.7478 lb/month	ethylbenzene			0.6756 lb/month
xylenes			3.4655 lb/month	xylenes			3.3568 lb/month	xylenes			3.0356 lb/month
naphthalene			0.0455 lb/month	naphthalene			0.0453 lb/month	naphthalene			0.0444 lb/month
cumene			0.1581 lb/month	cumene			0.1536 lb/month	cumene			0.1395 lb/month
Vapor Weight Concentrations Eq. 40-6 $Z_{vi} = y_i M_i / M_v$				Vapor Weight Concentrations Eq. 40-6 $Z_{vi} = y_i M_i / M_v$				Vapor Weight Concentrations Eq. 40-6 $Z_{vi} = y_i M_i / M_v$			
hexane		M_i	86.18	hexane		M_i	86.18	hexane		M_i	86.18
benzene		M_v	68	benzene		M_v	68	benzene		M_v	62
2,2,4 TMP		Z_{vi}	0.00622	2,2,4 TMP		Z_{vi}	0.00618	2,2,4 TMP		Z_{vi}	0.00417
toluene			0.00704	toluene			0.00699	toluene			0.00466
ethylbenzene			0.00811	ethylbenzene			0.00805	ethylbenzene			0.00532
xylenes			0.00811	xylenes			0.00810	xylenes			0.00526
naphthalene			0.00055	naphthalene			0.00054	naphthalene			0.00034
cumene			0.00239	cumene			0.00235	cumene			0.00149
			0.00000				0.00000				0.00000
			0.00009				0.00009				0.00006
Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{vA}$				Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{vA}$				Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{vA}$			
hexane		$P_i = P_{vA}(x_i)$	6.391	hexane		$P_i = P_{vA}(x_i)$	6.270	hexane		$P_i = P_{vA}(x_i)$	8.462
benzene		P_{vA}	0.00491	benzene		P_{vA}	0.00488	benzene		P_{vA}	0.00300
2,2,4 TMP		y_i	0.00613	2,2,4 TMP		y_i	0.00609	2,2,4 TMP		y_i	0.00370
toluene			0.00483	toluene			0.00479	toluene			0.00289
ethylbenzene			0.00604	ethylbenzene			0.00598	ethylbenzene			0.00354
xylenes			0.00035	xylenes			0.00034	xylenes			0.00020
naphthalene			0.00153	naphthalene			0.00151	naphthalene			0.00087
cumene			0.00000	cumene			0.00000	cumene			0.00000
			0.00000				0.00000				0.00000
			0.00005				0.00005				0.00003
Liquid Mole Fraction Eq. 40-4 $x_i = (Z_{vi} M_i) / M_i$				Liquid Mole Fraction Eq. 40-4 $x_i = (Z_{vi} M_i) / M_i$				Liquid Mole Fraction Eq. 40-4 $x_i = (Z_{vi} M_i) / M_i$			
hexane		Z_{vi}	0.01	hexane		Z_{vi}	0.01	hexane		Z_{vi}	0.01
benzene		M_i	92	benzene		M_i	92	benzene		M_i	92
2,2,4 TMP		x_i	0.01068	2,2,4 TMP		x_i	0.01068	2,2,4 TMP		x_i	0.01068
toluene			0.02120	toluene			0.02120	toluene			0.02120
ethylbenzene			0.03222	ethylbenzene			0.03222	ethylbenzene			0.03222
xylenes			0.06989	xylenes			0.06989	xylenes			0.06989
naphthalene			0.01213	naphthalene			0.01213	naphthalene			0.01213
cumene			0.06066	cumene			0.06066	cumene			0.06066
			0.00298				0.00298				0.00298
			0.00383				0.00383				0.00383
Component Vapor pressure $P_{vA} = (0.019337) 10^6 (A - (B/(TLA+C)))$				Component Vapor pressure $P_{vA} = (0.019337) 10^6 (A - (B/(TLA+C)))$				Component Vapor pressure $P_{vA} = (0.019337) 10^6 (A - (B/(TLA+C)))$			
hexane		A	6.878	hexane		A	6.878	hexane		A	6.878
benzene		B	1171.5	benzene		B	1171.5	benzene		B	1171.5
2,2,4 TMP		C	224.37	2,2,4 TMP		C	224.37	2,2,4 TMP		C	224.37
toluene		P_{vA}	2.9373	toluene		P_{vA}	2.8649	toluene		P_{vA}	2.3757
ethylbenzene			1.8489	ethylbenzene			1.8004	ethylbenzene			1.4751
xylenes			0.9583	xylenes			0.9322	xylenes			0.7579
naphthalene			0.5523	naphthalene			0.5361	naphthalene			0.4288
cumene			0.1841	cumene			0.1781	cumene			0.1387
			0.1611				0.1558				0.1211
			0.0050				0.0048				0.0035
			0.0887				0.0856				0.0654

MONTH October				MONTH November				MONTH December			
ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units
Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D + L_{LD}$)		LT	1,163.35 lb/month	Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D + L_{LD}$)		LT	1,030.33 lb/month	Total VOC Losses (Eq.2-1 & 2-2: $L_T = L_R + L_W + L_D + L_{LD}$)		LT	802.24 lb/month
			0.58 tons/month				0.52 tons/month				0.40 tons/month
Product Type			Gasoline - RVP 13.5	Product Type			Gasoline - RVP 15	Product Type			Gasoline - RVP 15
Monthly Throughput (only change if actual is known)		Q_{month}	147,043.02 barrels/month	Monthly Throughput (only change if actual is known)		Q_{month}	147,043.02 barrels/month	Monthly Throughput (only change if actual is known)		Q_{month}	147,043.02 barrels/month
Vapor Molecular weight		M_v	62.00	Vapor Molecular weight		M_v	60.15	Vapor Molecular weight		M_v	60.15
Vapor Pressure Equation Constant A		A	11.63	Vapor Pressure Equation Constant A		A	11.60	Vapor Pressure Equation Constant A		A	11.60
Vapor Pressure Equation Constant B		B	5015.72 °R	Vapor Pressure Equation Constant B		B	4937.93 °R	Vapor Pressure Equation Constant B		B	4937.93 °R
Daily total solar insolation on a horizontal surface		I	948.0 Btu/ft ² -day	Daily total solar insolation on a horizontal surface		I	621.0 Btu/ft ² -day	Daily total solar insolation on a horizontal surface		I	501.0 Btu/ft ² -day
Average Daily Ambient Temperature Eq. 1-30				Average Daily Ambient Temperature Eq. 1-30				Average Daily Ambient Temperature Eq. 1-30			
TAA = ((TAX+TAN)/2)		T_{AA}	514.75 °R	TAA = ((TAX+TAN)/2)		T_{AA}	505.35 °R	TAA = ((TAX+TAN)/2)		T_{AA}	495.50 °R
Average daily maximum ambient temperature, Table 7.1-7		T_{AX}	522.40 °R	Average daily maximum ambient temperature, Table 7.1-7		T_{AX}	512.10 °R	Average daily maximum ambient temperature, Table 7.1-7		T_{AX}	501.80 °R
Average daily minimum ambient temperature, Table 7.1-7		T_{AN}	507.10 °R	Average daily minimum ambient temperature, Table 7.1-7		T_{AN}	498.60 °R	Average daily minimum ambient temperature, Table 7.1-7		T_{AN}	489.20 °R
Liquid Bulk Temperature Eq 1-31:				Liquid Bulk Temperature Eq 1-31:				Liquid Bulk Temperature Eq 1-31:			
TB = TAA + 0.003 as I		T_B	515.46	TB = TAA + 0.003 as I		T_B	505.82	TB = TAA + 0.003 as I		T_B	495.88
Average Daily Liquid Surface Temperature Eq. 1-28				Average Daily Liquid Surface Temperature Eq. 1-28				Average Daily Liquid Surface Temperature Eq. 1-28			
TLA = 0.3*TAA + 0.7*TB + 0.004*α ¹		T_{LA}	516.20 °R	TLA = 0.3*TAA + 0.7*TB + 0.004*α ¹		T_{LA}	506.30 °R	TLA = 0.3*TAA + 0.7*TB + 0.004*α ¹		T_{LA}	496.26 °R
True Vapor Pressure Eq. 1-25:				True Vapor Pressure Eq. 1-25:				True Vapor Pressure Eq. 1-25:			
PVA = exp(A-(B/TLA))		P_{VA}	6.790 psia	PVA = exp(A-(B/TLA))		P_{VA}	6.340 psia	PVA = exp(A-(B/TLA))		P_{VA}	5.205 psia
Vapor pressure function Eq. 2-4:				Vapor pressure function Eq. 2-4:				Vapor pressure function Eq. 2-4:			
$P^* = P_{VA}/P_A/(1+(1-(P_{VA}/P_A))^{0.5})^2$		P^*	0.154 NA	$P^* = P_{VA}/P_A/(1+(1-(P_{VA}/P_A))^{0.5})^2$		P^*	0.140 NA	$P^* = P_{VA}/P_A/(1+(1-(P_{VA}/P_A))^{0.5})^2$		P^*	0.109 NA
Rim Seal Losses Eq. 2-3:				Rim Seal Losses Eq. 2-3:				Rim Seal Losses Eq. 2-3:			
$L_R = ((K_{GA} + K_{GB})/DP^* M_v K_c)/12$ months		L_R	170.42 lb/month	$L_R = ((K_{GA} + K_{GB})/DP^* M_v K_c)/12$ months		L_R	150.77 lb/month	$L_R = ((K_{GA} + K_{GB})/DP^* M_v K_c)/12$ months		L_R	117.07 lb/month
Withdrawal losses Eq. 2-19:				Withdrawal losses Eq. 2-19:				Withdrawal losses Eq. 2-19:			
$L_W = ((0.943)OCsW_j/D)^{1.1} * (N_{F,D})$		L_W	9.73 lb/month	$L_W = ((0.943)OCsW_j/D)^{1.1} * (N_{F,D})$		L_W	9.73 lb/month	$L_W = ((0.943)OCsW_j/D)^{1.1} * (N_{F,D})$		L_W	9.73 lb/month
Deck Fitting Losses Eq.2-13:				Deck Fitting Losses Eq.2-13:				Deck Fitting Losses Eq.2-13:			
$L_F = F_r P^* M_v K_c$		LF	583.58 lb/month	$L_F = F_r P^* M_v K_c$		LF	516.29 lb/month	$L_F = F_r P^* M_v K_c$		LF	400.91 lb/month
Deck Seam Losses Eq. 2-18:				Deck Seam Losses Eq. 2-18:				Deck Seam Losses Eq. 2-18:			
$L_D = K_D S_D P^* M_v K_c/12$ months		LD	399.62 lb/month	$L_D = K_D S_D P^* M_v K_c/12$ months		LD	353.55 lb/month	$L_D = K_D S_D P^* M_v K_c/12$ months		LD	274.53 lb/month
HAPS Speciation				HAPS Speciation				HAPS Speciation			
Product - same as January			Gasoline	Product - same as January			Gasoline	Product - same as January			Gasoline
Total HAP Monthly Emissions			23.937 lb/month	Total HAP Monthly Emissions			18.635 lb/month	Total HAP Monthly Emissions			13.529 lb/month
Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{vi}L_W$				Individual HAP Monthly Emissions Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{vi}L_W$				Individual HAP Monthly Em Eq. 40-2 $L_{Ti} = Z_{vi}(L_R + L_F + L_D) + Z_{vi}L_W$			
hexane		L_{Ti}	4.4990 lb/month	hexane		L_{Ti}	3.5282 lb/month	hexane		L_{Ti}	2.5375 lb/month
benzene			4.9970 lb/month	benzene			3.8677 lb/month	benzene			2.7520 lb/month
2,2,4 TMP			5.8243 lb/month	2,2,4 TMP			4.5052 lb/month	2,2,4 TMP			3.2276 lb/month
toluene			5.9213 lb/month	toluene			4.5592 lb/month	toluene			3.2911 lb/month
ethylbenzene			0.4602 lb/month	ethylbenzene			0.3666 lb/month	ethylbenzene			0.2847 lb/month
xylenes			2.0907 lb/month	xylenes			1.6807 lb/month	xylenes			1.3236 lb/month
naphthalene			0.0425 lb/month	naphthalene			0.0417 lb/month	naphthalene			0.0412 lb/month
cumene			0.1015 lb/month	cumene			0.0852 lb/month	cumene			0.0715 lb/month
Vapor Weight Concentrations Eq. 40-6 $Z_{vi} = y_i M_i / M_v$				Vapor Weight Concentrations Eq. 40-6 $Z_{vi} = y_i M_i / M_v$				Vapor Weight Concentration $Z_{vi} = y_i M_i / M_v$			
hexane		M_i	86.18	hexane		M_i	86.18	hexane		M_i	86.18
benzene		M_v	62	benzene		M_v	60	benzene		M_v	60
2,2,4 TMP		Z_{vi}	0.00382	2,2,4 TMP		Z_{vi}	0.00336	2,2,4 TMP		Z_{vi}	0.00308
toluene			0.00418	toluene			0.00362	toluene			0.00325
ethylbenzene			0.00471	ethylbenzene			0.00403	ethylbenzene			0.00358
xylenes			0.00454	xylenes			0.00380	xylenes			0.00329
naphthalene			0.00028	naphthalene			0.00023	naphthalene			0.00019
cumene			0.00122	cumene			0.00098	cumene			0.00081
			0.00071				0.00055				0.00046
			0.00000				0.00000				0.00000
			0.00005				0.00004				0.00003
Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{VA}$				Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{VA}$				Vapor Mole Fraction Eq. 40-5 $y_i = P_i / P_{VA}$			
hexane		$P_i = P_{VA}(x_i)$	0.018638	hexane		$P_i = P_{VA}(x_i)$	0.014875	hexane		$P_i = P_{VA}(x_i)$	0.011186
benzene		P_{VA}	6.790	benzene		P_{VA}	6.340	benzene		P_{VA}	5.205
2,2,4 TMP		y_i	0.00275	2,2,4 TMP		y_i	0.00235	2,2,4 TMP		y_i	0.00215
toluene			0.00332	toluene			0.00279	toluene			0.00250
ethylbenzene			0.00256	ethylbenzene			0.00212	ethylbenzene			0.00189
xylenes			0.00306	xylenes			0.00248	xylenes			0.00215
naphthalene			0.00016	naphthalene			0.00013	naphthalene			0.00011
cumene			0.00071	cumene			0.00055	cumene			0.00046
			0.00000				0.00000				0.00000
			0.00002				0.00002				0.00001
Liquid Mole Fraction Eq. 40-4 $x_i = (Z_{vi} M_i) / M_i$				Liquid Mole Fraction Eq. 40-4 $x_i = (Z_{vi} M_i) / M_i$				Liquid Mole Fraction Eq. 40-4 $x_i = (Z_{vi} M_i) / M_i$			
hexane		Z_{vi}	0.01	hexane		Z_{vi}	0.01	hexane		Z_{vi}	0.01
benzene		M_i	92	benzene		M_i	96	benzene		M_i	96
2,2,4 TMP		x_i	0.01068	2,2,4 TMP		x_i	0.01114	2,2,4 TMP		x_i	0.01114
toluene			0.02120	toluene			0.02212	toluene			0.02212
ethylbenzene			0.03222	ethylbenzene			0.03362	ethylbenzene			0.03362
xylenes			0.06989	xylenes			0.07293	xylenes			0.07293
naphthalene			0.01213	naphthalene			0.01266	naphthalene			0.01266
cumene			0.06066	cumene			0.06329	cumene			0.06329
			0.00298				0.00311				0.00311
			0.00238				0.00311				0.00311
			0.00383				0.00399				0.00399
Component Vapor pressure $P_{VA} = (0.019337)10^4(A-(B/(TLA+C)))$				Component Vapor pressure $P_{VA} = (0.019337)10^4(A-(B/(TLA+C)))$				Component Vapor pressure $P_{VA} = (0.019337)10^4(A-(B/(TLA+C)))$			
hexane		A	6.878	hexane		A	6.878	hexane		A	6.878
benzene		B	1171.5	benzene		B	1171.5	benzene		B	1171.5
2,2,4 TMP		C	224.37	2,2,4 TMP		C	224.37	2,2,4 TMP		C	224.37
toluene		P_{VA}	1.7459	toluene		P_{VA}	1.3354	toluene		P_{VA}	1.0042
ethylbenzene			6.906	ethylbenzene			6.906	ethylbenzene			6.906
xylenes			1211	xylenes			1211	xylenes			1211
naphthalene			220.79	naphthalene			220.79	naphthalene			220.79
cumene			0.5390	cumene			0.4005	cumene			0.2920
			0.2969				0.2156				0.1534
			0.0918				0.0641				0.0436
			0.0799				0.0556				0.0378
			0.0020				0.0013				0.0008
			0.0420				0.0285				0.0188

Monthly Calculations - JANUARY

Tank No.	17413	Symbol	Units	ROUTINE EMISSIONS CALCULATIONS	Symbol	Units	HAPS Speciation	ib/month	Vapor Weight Concentrations	Vapor Mole Fraction								
ROUTINE EMISSIONS CALCULATIONS																		
Total Losses (Eq. 1-1: LT = LS+LW)	LT		192.30	ib/month	Standing Losses: Eq. 1-2, $LS = 365 (Vv \cdot Wv \cdot KE \cdot Ks)$	LS	9.14	ib/month	Total HAP Emissions = 16.404	Vapor Weight Concentrations								
			9.62E-02	ton/month	Vapor Space Volume	Vv	206626.8	ft ³	Eq. 40-6 $ZVi = y_i M_i / MV$	Vapor Mole Fraction								
			1.01E-01	ton/month	Stock Vapor Density	Wv	0.0001	lb/ft ³	Eq. 40-2 $ZVi = y_i M_i / MV$	Vapor Mole Fraction								
			1.01E-01	ton/month	Vapor Space Expansion Factor (0 < KE <= 1); Eq. 1-5	KE	0.024	per day	Individual HAPS	Eq. 40-5 $y_i = P_i / PVA$								
Nearest US Location	Bridgeport, CT				Vented Vapor Saturation Factor	Ks	1.00	NA	hexane	0.1000	86.18	130	0.00052	0.000002	0.002	0.00078		
Daily total solar insolation on a horizontal surface; Table 7.1-7	I		560.0	Btu/ft ² -day	Constant: Number of Daily Events in a Year	365		days/month	benzene	0.5813	78.11	130	0.00302	0.000012	0.002	0.00503		
Absolute Pressure	Pa		14.69	psi					2,2,4 TMP	0.0000	114.23	130	0.00000	0.000000	0.002	-		
Ideal Gas Constant	R		10.73	psia ft ³ /lb-mole R	Working Losses: Eq. 1-35, $Lw = VQ \cdot KN \cdot Kp \cdot Wv \cdot KB$	Lw	183.17	lb/month	toluene	4.7588	92.14	130	0.02475	0.000085	0.002	0.03491		
Product Information					Net Working Loss Throughput (Eq. 1-39: $VQ=5.614 \cdot Q$)	VQ	12,829.821	ft ³ /month	ethylbenzene	0.5380	106.17	130	0.00280	0.000008	0.002	0.00343		
Product Type	Distillate Fuel Oil No.2				Working Loss Turnover Factor (Eq. 1-35: $Kp=(180+N)/6N$ for N>36, else $Kp=1$)	Kp	0.2393		xylene	10.3736	106.17	130	0.05394	0.000160	0.002	0.06605		
Vapor Molecular weight	Mv		130	lb/lb-mole	Working Loss Product Factor	Kp	1.00		naphthalene	0.0524	128.17	130	2.72E-04	6.89E-07	0.002	2.76E-04		
Vapor organic liquid density	WL		7.10	lb/gal	Stock Vapor Density	Wv	0.0001	lb/ft ³	cumene	0.0000	120.19	130	0.00E+00	0.00E+00	0.002	0.00E+00		
Average Reid Vapor Pressure	RVP		0.02	psi	Vent Setting Correction Factor	KB	1.00											
Product factor: 0.4 for crude oils or 1 for other organic liquids	Kc		1.00						Liquid Mole Fraction									
Vapor Pressure Equation Constant A	A		12.10		Vented Vapor Saturation Factor: Eq. 1-21, $Ks = 1/(1+0.053 \cdot PVA^{1/3} \cdot Hvo)$	Ks	1.00		Individual HAPS	Z_i	M_i	M_i	X_i	Component Vapor Pressure				
Vapor Pressure Equation Constant B (Table 7.1-2)	B		8907.0	R	Vapor Pressure at Avg Daily Liq Surface Temp	PvA	0.0024	psia	Eq. 40-4 $x_i = (Z_i M_i) / M_i$	hexane	0.00000	188	86.18	0.00000	A	B	C	PvA
					Vapor Space Outage	Hvo	19.22	ft	Eq. 40-6 $ZVi = y_i M_i / MV$	benzene	0.00001	188	78.11	0.00002	6.878	1171.5	224.37	0.8715
										2,2,4 TMP	0.00000	188	114.23	0.00000	6.906	1211	220.79	0.5064
Tank design data					Vapor Space Expansion Factor (Eq. 1-5: $(\Delta T_v/TLA)+((\Delta P_v-\Delta P_B)/(PA-PvA))$)	KE	0.0240	per day	Eq. 40-5 $y_i = P_i / PVA$	toluene	0.00000	188	92.14	0.00065	6.812	1257.8	220.74	0.2495
Shell height	Hs		36.00	ft	Average Daily Vapor Temperature Range	ΔT_v	11.76	R	ethylbenzene	0.00032	188	92.14	0.00065	7.017	1377.6	222.64	0.1296	
Diameter	D		117.00	ft	Average Daily Vapor Pressure Range	ΔP_v	0.0006	psi	toluene	0.00013	188	106.17	0.00023	6.95	1419.3	212.61	0.0381	
Throughput	Q		95,983.697	gal/month	Breather Vent Pressure Setting Range (Equation 1-10: $\Delta P_B = PBP - PBV$)	ΔP_B	0.0000	psi	xylene	0.00290	188	106.17	0.00514	7.009	1462.3	215.11	0.0312	
Turnovers	N		413.25	per year	Vapor Pressure at Avg Daily Liq Surface Temp	PvA	0.0024	psia	naphthalene	0.00076	188	128.17	0.00111	7.146	1831.6	211.82	0.0006	
Roof Type:	Cone				Average Daily Liquid Surface Temperature	TLA	491.45	R	cumene	0.00000	188	120.19	0.00000	6.929	1455.8	207.2	0.0153	
Tank Cone Roof Slope (If unknown, use 0.0625)	SR		0.0625	ft/ft	Atmospheric Pressure	Pa	14.69	psia										
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR		NA	ft														
Maximum Filling Height (use Hs-1 if unknown)	HLX		35.00	ft														
Minimum Filling Height (use 1 if unknown)	HLN		1.00	ft	Average Daily Vapor Temperature Range (ΔT_v)													
Liquid height (assume 1/2 Hs)	HL		18.00	ft	Average daily ambient temperature range - Equation 1-11 ($\Delta T_A = T_{AX} - T_{AN}$)	ΔT_A	12.8	R										
Tank Insulation (pick from drop down list)	Not Insulated				Not Insulated - Equation 1-7 ($\Delta T_v = 0.7 \Delta T_A + 0.02 \text{ or } I$)	ΔT_v	11.76	R										
Tank Construction (pick from drop down list)	Riveted				Partially Insulated - Equation 1-8 ($\Delta T_v = 0.6 \Delta T_A + 0.02 \text{ or } I$)	ΔT_v	10.48	R										
Tank Shell Color (pick from drop down list)	White				Fully Insulated, constant temperature	ΔT_v	0.00	R										
Tank Shell Condition (pick from drop down list)	Average																	
Tank Interior Condition (pick from drop down list)	Light Rust				Average Daily Vapor Pressure Range (ΔP_v)													
Tank paint solar absorptance, dimensionless; Table 7.1-6	α		0.25		Not Insulated - Equation 1-9: $\Delta P_v = PVX - PVN$	ΔP_v	0.00053	psia										
Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP		0.03	psi	Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25: $PVX = \exp(PVN)$)	PVX	0.00270	psia										
	PBV		-0.03	psi	Vapor pressure at ave daily min liquid surface temp. (Eq. 1-25: $PVN = \exp(PVX)$)	PVN	0.00217	psia										
True Vapor Pressure; Eq. 1-25, $PvA = \exp(A-B/TLA)$					Average daily max. liquid surface temp.; Fig. 7.1-17: $TLX = TLA + 0.25 \Delta T_v$	TLX	494.39	R										
Not Insulated	PvA		0.002422766		Average daily min. liquid surface temp.; Fig. 7.1-17: $TLN = TLA - 0.25 \Delta T_v$	TLN	488.51	R										
Partially Insulated	PvA		0.002426522															
Fully Insulated	PvA		0.002375646		Partially Insulated - Equation 1-9: $\Delta P_v = PVX - PVN$	ΔP_v	0.00047	psia										
					Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25: use PVX)	PVX	0.00267	psia										
					Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25: use PVN)	PVN	0.002019	psia										
Average Daily Ambient Temperature (TAA) Eq. 1-30 $TAA = ((TAX+TAN)/2)$	TAA		490.50	R	Average daily maximum liquid surface temperature, deg R ($TLX = TLA + 0 \cdot TLX$)	TLX	494.11	R										
Average daily maximum ambient temperature; Table 7.1-7	TAX		486.90	R	Average daily minimum liquid surface temperature, deg R ($TLN = TLA - 0 \cdot TLN$)	TLN	488.87	R										
Average daily minimum ambient temperature; Table 7.1-7	TAN		484.10	R														
Liquid Bulk Temperature; Eq. 1-31: $TB = TAA + 0.003 \text{ or } I$	TB		490.92	R	Fully Insulated ($\Delta P_v = 0$)	ΔP_v	0.00	psia										
Average Daily Liquid Surface Temperature (TLA)					Vapor Space Volume (Eq. 1-3: $Vv = ((\pi / 4) D^2 Hvo)$)	Vv	206,626.84	ft ³										
Not Insulated; Eq. 1-28, $TLA = 0.4 \cdot TAA + 0.6 \cdot TB + 0.005 \cdot \alpha \cdot I$	TLA		491.45	R	Tank diameter	D	117.00	ft										
Partially Insulated; Eq. 1-29, $TLA = 0.3 \cdot TAA + 0.7 \cdot TB + 0.005 \cdot \alpha \cdot I$	TLA		491.49	R	Vapor Space Outage; see Equation 1-16	Hvo	19.22	ft										
Fully Insulated; $TLA = TB$	TLA		490.9	R														
					Vapor Space Outage (Eq. 1-16: $Hvo=Hs+HL+HRO$)	Hvo	19.22	ft										
Average Vapor Temperature (Tv)					Tank shell height	Hs	36.00	ft										
Not Insulated; Eq. 1-33, $Tv = 0.7 \cdot TAA + 0.3 \cdot TB + 0.009 \cdot \alpha \cdot I$	Tv		491.89	R	Liquid Height	HL	18.00	ft										
Partially Insulated; Eq. 1-34, $Tv = 0.6 \cdot TAA + 0.4 \cdot TB + 0.01 \cdot \alpha \cdot I$	Tv		492.07	R	Roof Outage (for a Cone Roof vs Dome Roof)	HRO	1.22	ft										
Fully Insulated; $Tv = TB$	Tv		490.92	R														
					Roof Outage - Cone Roof (Eq. 1-17 & 1-18: $HRO=(1/3)SR \cdot Rs$)	HRO	1.22	ft										
Stock Vapor Density; Eq. 1-22, $Wv = (Mv \cdot PvA) / (R \cdot Tv)$					Tank cone roof slope (If unknown, use 0.0625)	SR	0.0625	ft/ft										
Not Insulated	Wv		5.967E-05		Tank shell radius	Rs	58.50	ft										
Partially Insulated	Wv		5.974E-05															
Fully Insulated	Wv		5.862E-05		Roof Outage - Dome Roof (Eq. 1-19 & 1-20: $HRO=(RR \cdot (RR^2+Rs^2)^{0.5}) / (0.5+0.166 \cdot RR)$)	HRO	8.03	ft										
					Tank dome roof radius (If unknown, use tank diameter (D) or (2Rs))	RR	117.00	ft										
					Tank shell radius	Rs	58.50	ft										

Monthly Calculations (continued)

Tank No.	17413	Symbol	Units	ROUTINE EMISSIONS CALCULATIONS	Symbol	Units	HAPS Speciation	ib/month	Vapor Weight Concentrations	Vapor Mole Fraction						
ROUTINE EMISSIONS CALCULATIONS																
Total Losses (Eq. 1-1: LT = LS+LW)	LT		201.87	ib/month	Standing Losses: Eq. 1-2, $LS = 365 (Vv \cdot Wv \cdot KE \cdot Ks)$	LS	10.15	ib/month	Total HAP Emissions = 17.288	Vapor Weight Concentrations						
			1.01E-01	ton/month	Vapor Space Volume	Vv	206626.8	ft ³	Eq. 40-6 $ZVi = y_i M_i / MV$	Vapor Mole Fraction						
			1.01E-01	ton/month	Stock Vapor Density	Wv	0.0001	lb/ft ³	Eq. 40-2 $ZVi = y_i M_i / MV$	Vapor Mole Fraction						
			1.01E-01	ton/month	Vapor Space Expansion Factor (0 < KE <= 1); Eq. 1-5	KE	0.027	per day	Individual HAPS	Eq. 40-5 $y_i = P_i / PVA$						
Nearest US Location	Bridgeport, CT				Vented Vapor Saturation Factor	Ks	1.00	NA	hexane	0.1034	86.18	130	0.00051	0.000002	0.003	0.00077
Daily total solar insolation on a horizontal surface; Table 7.1-7	I		847.0	Btu/ft ² -day	Constant: Number of Daily Events in a Year	365		days/month	benzene	0.6035	78.11	130	0.00299	0.000013	0.003	0.00498
Absolute Pressure	Pa		14.69	psi					2,2,4 TMP	0.0000	114.23	130	0.00000	0.000000	0.003	-
Ideal Gas Constant	R		10.73	psia ft ³ /lb-mole R	Working Losses: Eq. 1-35, $Lw = VQ \cdot KN \cdot Kp \cdot Wv \cdot KB$	Lw	191.72	lb/month	toluene	4.9811	92.14	130	0.02467	0.000091	0.003	0.03481
Product Information					Net Working Loss Throughput (Eq. 1-39: $VQ=5.614 \cdot Q$)	VQ	12,829.821	ft ³ /month	ethylbenzene	0.5689	106.17	130	0.00282	0.000009	0.003	0.00345
Product Type	Distillate Fuel Oil No.2															

Monthly Calculations (continued)

JULY

Tank No.	17413	Symbol		Units	ROUTINE EMISSIONS CALCULATIONS	Symbol	Units	HAPS Speciation	lb/month	Vapor Mole Fraction						
ROUTINE EMISSIONS CALCULATIONS		Symbol		Units	ROUTINE EMISSIONS CALCULATIONS			Product	lb/month	Vapor Mole Fraction						
Total Losses (Eq. 1-1: $LT = LS+LW$)		LT		lb/month	Standing Losses; Eq. 1-2, $LS = 365 (Vv \cdot Wv \cdot KE \cdot Ks)$			Total HAP Emissions =			Eq. 40-6 $Zvi = yM / MV$			Eq. 40-5 $yi = Pi / PVA$		
Time Period		July		lb/month	Vapor Space Volume			Individual HAPS			Eq. 40-2 $L_i = Z_i(L_i)$			Eq. 40-5 $yi = Pi / PVA$		
Nearest US Location		Bridgeport, CT		ft	Vapor Space Expansion Factor ($0 < KE \leq 1$); Eq. 1-5			hexane			0.00000			0.00006		
Daily total solar insolation on a horizontal surface; Table 7.1-7		I		1904.0	Constant; Number of Daily Events in a Year			benzene			0.00000			0.00045		
Absolute Pressure		PA		14.69	Net Working Loss Throughput (Eq. 1-39: $VQ=5.614 \cdot Q$)			2,2,4 TMP			0.00000			0.00000		
Ideal Gas Constant		R		10.73	Working Losses; Eq. 1-35, $Lw = VQ \cdot KN \cdot Kp \cdot Wv \cdot KB$			toluene			0.00000			0.00036		
Product Information		Distillate Fuel Oil No.2			Net Working Loss Turnover Factor Eq. 1-35 $Kp=(180+N)/6N$ for $N \geq 36$, else $Kp=1$			ethylbenzene			0.00000			0.00003		
Vapor Molecular weight		Mv		130	Working Loss Product Factor			xylenes			0.00000			0.00036		
Average organic liquid density		WL		7.10	Stock Vapor Density			naphthalene			0.00000			0.00000		
Average Reid Vapor Pressure		RVP		0.02	Vent Setting Correction Factor			cumene			0.00000			0.00E+00		
Product factor; 0.4 for crude oils or 1 for other organic liquids		Kc		1.00	Vented Vapor Saturation Factor; Eq. 1-21, $Ks = 1/(1+0.053 \cdot PVA \cdot Hvo)$			Individual HAPS			Eq. 40-4 $xi = (Zi \cdot Mi) / M$			Component Vapor Pressure		
Vapor Pressure Equation Constant A		A		12.10	Vapor Pressure at Avg Daily Liq Surface Temp			hexane			0.00000			0.00000		
Vapor Pressure Equation Constant B (Table 7.1-2)		B		8907.0	Vapor Space Outage			benzene			0.00001			0.00002		
Tank design data					Vapor Space Expansion Factor (Eq. 1-5: $(\Delta T / TL) + ((\Delta Pv - \Delta P) / (PA - PVA))$)			2,2,4 TMP			0.00000			0.00000		
Shell height		Hs		36.00	Average Daily Vapor Temperature Range			toluene			0.00032			0.00065		
Diameter		D		117.00	Average Daily Vapor Pressure Range			ethylbenzene			0.00013			0.00023		
Throughput		Q		95,983,697	Breather Vent Pressure Setting Range (Equation 1-10: $\Delta P = PBP - PBV$)			xylenes			0.00290			0.00514		
Turnovers		N		413.25	Vapor Pressure at Avg Daily Liq Surface Temp			naphthalene			0.00076			0.00111		
Roof Type:		Cone			Average Daily Liquid Surface Temperature			cumene			0.00000			0.00000		
Tank Cone Roof Slope (If unknown, use 0.0625)		SR		0.0625	Atmospheric Pressure			Individual HAPS			Eq. 40-4 $xi = (Zi \cdot Mi) / M$			Component Vapor Pressure		
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))		RR		NA	Average Daily Vapor Temperature Range (ΔT)			hexane			0.00001			0.00000		
Maximum Filling Height (use Hs-1 if unknown)		HLX		35.00	Not Insulated - Equation 1-7 ($\Delta T = 0.7 \Delta TA + 0.02 \alpha$)			benzene			0.00001			0.00002		
Minimum Filling Height (use 1 ft if unknown)		HLN		1.00	Partially Insulated - Equation 1-8 ($\Delta T = 0.6 \Delta TA + 0.02 \alpha R$)			2,2,4 TMP			0.00000			0.00000		
Liquid height (assume 1/2 Hs)		HL		18.00	Fully Insulated, constant temperature			toluene			0.00000			0.00000		
Tank Insulation (pick from drop down list)		Not Insulated			Average Daily Vapor Pressure Range (ΔPv)			ethylbenzene			0.00032			0.00065		
Tank Construction (pick from drop down list)		Riveted			Not Insulated - Equation 1-9: $\Delta Pv = PVX - PVN$			xylenes			0.00290			0.00514		
Tank Shell Color (pick from drop down list)		White			Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25 $PVX = \exp(PVN)$)			naphthalene			0.00076			0.00111		
Tank Shell Condition (pick from drop down list)		Average			Vapor pressure at ave daily min liquid surface temp. (Eq. 1-25 $PVN = \exp(TLX)$)			cumene			0.00000			0.00E+00		
Tank Interior Condition (pick from drop down list)		Light Rust			Average daily max. liquid surface temp.; Fig. 7.1-17 $TLX = TLA + 0.25 \Delta T$			Individual HAPS			Eq. 40-4 $xi = (Zi \cdot Mi) / M$			Component Vapor Pressure		
Tank paint solar absorptance, dimensionless; Table 7.1-6		α		0.25	Average daily min. liquid surface temp.; Fig. 7.1-17 $TLN = TLA - 0.25 \Delta T$			hexane			0.00001			0.00000		
Breather Vent Setting Range (Default Assumption: +/- 0.03)		PBP		-0.03	Partially Insulated - Equation 1-9: $\Delta Pv = PVX - PVN$			benzene			0.00001			0.00002		
True Vapor Pressure; Eq. 1-25, $PVA = \exp(A/(B-TLA))$					Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25 use PVX)			2,2,4 TMP			0.00000			0.00000		
Not Insulated		PVA		0.011317921	Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25 use PVN)			toluene			0.00032			0.00065		
Partially Insulated		PVA		0.011367913	Average daily maximum liquid surface temperature, deg R ($TLX = TLA + 0$)			ethylbenzene			0.00013			0.00023		
Fully Insulated		PVA		0.010701221	Average daily minimum liquid surface temperature, deg R ($TLN = TLA - 0$)			xylenes			0.00290			0.00514		
Average Daily Ambient Temperature (TAA) Eq. 1-30 $TAA = ((TAX+TAN)/2)$		TAA		533.30	Fully Insulated ($\Delta Pv = 0$)			naphthalene			0.00076			0.00111		
Average daily maximum ambient temperature; Table 7.1-7		TAX		541.10	Vapor Space Volume (Eq. 1-3: $Vv = ((\pi/4) D^2 Hvo)$)			cumene			0.00000			0.00000		
Average daily minimum ambient temperature; Table 7.1-7		TAN		526.70	Tank diameter			Individual HAPS			Eq. 40-4 $xi = (Zi \cdot Mi) / M$			Component Vapor Pressure		
Liquid Bulk Temperature; Eq. 1-31: $TB = TAA + 0.003 \alpha s$		TB		535.33	Vapor Space Outage; see Equation 1-16			hexane			0.00001			0.00000		
Average Daily Liquid Surface Temperature (TLA)					Tank shell height			benzene			0.00001			0.00002		
Not Insulated; Eq. 1-28, $TLA = 0.4 \cdot TAA + 0.6 \cdot TB + 0.005 \cdot \alpha$		TLA		537.14	Liquid Height			2,2,4 TMP			0.00000			0.00000		
Partially Insulated; Eq. 1-29, $TLA = 0.3 \cdot TAA + 0.7 \cdot TB + 0.005 \cdot \alpha R$		TLA		537.28	Roof Outage (for a Cone Roof vs Dome Roof)			toluene			0.00032			0.00065		
Fully Insulated; $TLA = TB$		TLA		535.3	Roof Outage (for a Cone Roof vs Dome Roof)			ethylbenzene			0.00013			0.00023		
Average Vapor Temperature (Tv)					Roof Outage - Cone Roof (Eq. 1-17 & 1-18: $HRO = (1/3)SR \cdot Rs$)			xylenes			0.00290			0.00514		
Not Insulated; Eq. 1-33, $Tv = 0.7 \cdot TAA + 0.3 \cdot TB + 0.009 \cdot \alpha$		Tv		538.61	Tank cone roof slope (If unknown, use 0.0625)			naphthalene			0.00076			0.00111		
Partially Insulated; Eq. 1-34, $Tv = 0.6 \cdot TAA + 0.4 \cdot TB + 0.01 \cdot \alpha R$		Tv		539.23	Tank shell radius			cumene			0.00000			0.00000		
Fully Insulated; $Tv = TB$		Tv		535.33	Roof Outage - Dome Roof (Eq. 1-19 & 1-20: $HRO = (RR \cdot (RR^2 + Rs^2) \cdot 0.5) / (0.5 + 0.166 \cdot HRO)$)			Individual HAPS			Eq. 40-4 $xi = (Zi \cdot Mi) / M$			Component Vapor Pressure		
Stock Vapor Density; Eq. 1-22, $Wv = (Mv \cdot PVA) / (R \cdot Tv)$					Tank dome roof radius (If unknown, use tank diameter (D) or (2Rs))			hexane			0.00001			0.00000		
Not Insulated		Wv		2.546E-04	Tank shell radius			benzene			0.00001			0.00002		
Partially Insulated		Wv		2.554E-04	Roof Outage - Dome Roof (Eq. 1-19 & 1-20: $HRO = (RR \cdot (RR^2 + Rs^2) \cdot 0.5) / (0.5 + 0.166 \cdot HRO)$)			2,2,4 TMP			0.00000			0.00000		
Fully Insulated		Wv		2.422E-04	Tank dome roof radius (If unknown, use tank diameter (D) or (2Rs))			toluene			0.00032			0.00065		
					Tank shell radius			ethylbenzene			0.00013			0.00023		
								xylenes			0.00290			0.00514		
								naphthalene			0.00076			0.00111		
								cumene			0.00000			0.00E+00		

Monthly Calculations (continued)

AUGUST

Tank No.	17413	Symbol		Units	ROUTINE EMISSIONS CALCULATIONS	Symbol	Units	HAPS Speciation	lb/month	Vapor Mole Fraction						
ROUTINE EMISSIONS CALCULATIONS		Symbol		Units	ROUTINE EMISSIONS CALCULATIONS			Product	lb/month	Vapor Mole Fraction						
Total Losses (Eq. 1-1: $LT = LS+LW$)		LT		lb/month	Standing Losses; Eq. 1-2, $LS = 365 (Vv \cdot Wv \cdot KE \cdot Ks)$			Total HAP Emissions =			Eq. 40-6 $Zvi = yM / MV$			Eq. 40-5 $yi = Pi / PVA$		
Time Period		August		lb/month	Vapor Space Volume			Individual HAPS			Eq. 40-2 $L_i = Z_i(L_i)$			Eq. 40-5 $yi = Pi / PVA$		
Nearest US Location		Bridgeport, CT		ft	Vapor Space Expansion Factor ($0 < KE \leq 1$); Eq. 1-5			hexane			0.3090			0.00038		
Daily total solar insolation on a horizontal surface; Table 7.1-7		I		1685.0	Constant; Number of Daily Events in a Year			benzene			1.9427			0.00240		
Absolute Pressure		PA		14.69	Net Working Loss Throughput (Eq. 1-39: $VQ=5.614 \cdot Q$)			2,2,4 TMP			0.00000			0.00000		
Ideal Gas Constant		R		10.73	Working Losses; Eq. 1-35, $Lw = VQ \cdot KN \cdot Kp \cdot Wv \cdot KB$			toluene			18.5269			0.02285		
Product Information		Distillate Fuel Oil No.2			Net Working Loss Turnover Factor Eq. 1-35 $Kp=(180+N)/6N$ for $N \geq 36$, else $Kp=1$			ethylbenzene			2.5025			0.00309		
Vapor Molecular weight		Mv		130	Working Loss Product Factor			xylenes			48.8497			0.06025		
Average organic liquid density		WL		7.10	Stock Vapor Density			naphthalene			0.3943			4.86E-04		
Average Reid Vapor Pressure		RVP		0.02	Vent Setting Correction Factor			cumene			0.00000			120.19		
Product factor; 0.4 for crude oils or 1 for other organic liquids		Kc		1.00	Vented Vapor Saturation Factor; Eq. 1-21, $Ks = 1/(1+0.053 \cdot PVA \cdot Hvo)$			Individual HAPS			Eq. 40-4 $xi = (Zi \cdot Mi) / M$			Component Vapor Pressure		
Vapor Pressure Equation Constant A		A		12.10	Vapor Pressure at Avg Daily Liq Surface Temp			hexane			0.00001			0.00000		
Vapor Pressure Equation Constant B (Table 7.1-2)		B		8907.0	Vapor Space Outage			benzene			0.00001			0.00002		
Tank design data					Vapor Space Expansion Factor (Eq. 1-5: $(\Delta T / TL) + ((\Delta Pv - \Delta P) / (PA - PVA))$)			2,2,4 TMP			0.00000			0.00000		
Shell height		Hs		36.00	Average Daily Vapor Temperature Range			toluene			0.00032			0.00065		
Diameter		D		117.00	Average Daily Vapor Pressure Range			ethylbenzene			0.00013			0.00023		
Throughput		Q		95,983,697	Breather Vent Pressure Setting Range (Equation 1-10: $\Delta P = PBP - PBV$)			xylenes			0.00290			0.00514		
Turnovers		N		413.25	Vapor Pressure at Avg Daily Liq Surface Temp			naphthalene			0.00076			0.00111		
Roof Type:		Cone			Average Daily Liquid Surface Temperature			cumene			0.00000			0.00000		
Tank Cone Roof Slope (If unknown, use 0.0625)		SR		0.0625	Atmospheric Pressure			Individual HAPS			Eq. 40-4 $xi = (Zi \cdot Mi) / M$			Component Vapor Pressure		
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))		RR		NA	Average Daily Vapor Temperature Range (ΔT)			hexane			0.00001			0.00000		
Maximum Filling Height (use Hs-1 if unknown)		HLX		35.00	Not Insulated - Equation 1-7 ($\Delta T = 0.7 \Delta TA + 0.02 \alpha$)			benzene			0.00001			0.00002		
Minimum Filling Height (use 1 ft if unknown)		HLN		1.00	Partially Insulated - Equation 1-8 ($\Delta T = 0.6 \Delta TA + 0.02 \alpha R$)			2,2,4 TMP			0.00000			0.00000		
Liquid height (assume 1/2 Hs)		HL		18.00	Fully Insulated, constant temperature			toluene			0.00032			0.00065		
Tank Insulation (pick from drop down list)		Not Insulated			Average Daily Vapor Pressure Range (ΔPv)			ethylbenzene			0.00032			0.00065		
Tank Construction (pick from drop down list)		Riveted			Not Insulated - Equation 1-9: $\Delta Pv = PVX - PVN$			xylenes			0.00290			0.00514		
Tank Shell Color (pick from drop down list)		White			Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25 $PVX = \exp(PVN)$)			naphthalene			0.00076			0.00111		
Tank Shell Condition (pick from drop down list)		Average			Vapor pressure at ave daily min liquid surface temp. (Eq. 1-25 $PVN = \exp(TLX)$)			cumene			0.00000			0.00E+00		
Tank Interior Condition (pick from drop down list)		Light Rust			Average daily max. liquid surface temp.; Fig. 7.1-17 $TLX = TLA + 0.25 \Delta T$			Individual HAPS			Eq. 40-4 $xi = (Zi \cdot Mi) / M$			Component Vapor Pressure		
Tank paint solar absorptance, dimensionless; Table 7.1-6		α		0.25	Average daily min. liquid surface temp.; Fig. 7.1-17 $TLN = TLA - 0.25 \Delta T$			hexane			0.00001			0.00000		
Breather Vent Setting Range (Default Assumption: +/- 0.03)		PBP		-0.03	Partially Insulated - Equation 1-9: $\Delta Pv = PVX - PVN$			benzene			0.00001			0.00002		
True Vapor Pressure; Eq. 1-25, $PVA = \exp(A/(B-TLA))$					Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25 use PVX)			2,2,4 TMP			0.00000			0.00000		
Not Insulated		PVA		0.010948664	Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25 use PVN)			toluene			0.00032			0.00065		
Partially Insulated		PVA		0.010991624	Average daily maximum liquid surface temperature, deg R ($TLX = TLA + 0$)			ethylbenzene			0.00013			0.00023		
Fully Insulated		PVA		0.010417144	Average daily minimum liquid surface temperature, deg R ($TLN = TLA - 0$)			xylenes			0.00290			0.00514		
Average Daily Ambient Temperature (TAA) Eq. 1-30 $TAA = ((TAX+TAN)/2)$		TAA		533.20	Fully Insulated ($\Delta Pv = 0$)			naphthalene			0.00076			0.00111		
Average daily maximum ambient temperature; Table 7.1-7		TAX		540.10	Vapor Space Volume (Eq. 1-3: $Vv = ((\pi/4) D^2 Hvo)$)			cumene			0.00000			0.00000		
Average daily minimum ambient temperature; Table 7.1-7		TAN		526.30	Tank diameter			Individual HAPS			Eq. 40-4 $xi = (Zi \cdot Mi) / M$			Component Vapor Pressure		
Liquid Bulk Temperature; Eq. 1-31: $TB = TAA + 0.003 \alpha s$		TB		534.46	Vapor Space Outage; see Equation 1-16			hexane			0.00001			0.00000		
Average Daily Liquid Surface Temperature (TLA)					Tank shell height			benzene			0.00001			0.00002		
Not Insulated; Eq. 1-28, $TLA = 0.4 \cdot TAA + 0.6 \cdot TB + 0.005 \cdot \alpha$		TLA		536.06	Liquid Height			2,2,4 TMP			0.00000			0.00000		

Monthly Calculations (continued)

SEPTEMBER

Tank No.	17413	Symbol	Units	ROUTINE EMISSIONS CALCULATIONS	Symbol	Units	HAPS Speciation	lb/month	Product	lb/month	Vapor Weight Concentrations	Vapor Mole Fraction				
ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS			HAPS Speciation		Product	lb/month	Vapor Weight Concentrations		Vapor Mole Fraction			
Total Losses (Eq. 1-1: LT = LS+LW)		LT	636.86	lb/month	Standing Losses; Eq. 1-2, $LS = 365 (Vv \cdot Wv \cdot KE \cdot Ks)$	Ls	38.53	lb/month	Diesel	56.747	Eq. 40-6 $Zvi = y_i M_i / MV$		Eq. 40-5 $y_i = P_i / PVA$			
Time Period		September	3.18E-01	ton/month	Vapor Space Volume	Vv	206626.8	ft3	Total HAP Emissions =	56.747	Eq. 40-2 $L_i = Z_i(L_i)$		Eq. 40-5 $y_i = P_i / PVA$			
Nearest US Location		Bridgeport, CT			Stock Vapor Density	Wv	0.0002	lb/ft3	Individual HAPS	L_{ij} (lb/yr)	M_i	M_j	Z_{ij}	$P_i = P_{v,i}(X_i)$	PVA	y_i
Daily total solar insolation on a horizontal surface; Table 7.1-7		I	1320.0	Btu/ft ² -day	Vapor Space Expansion Factor ($0 < KE \leq 1$); Eq. 1-5	KE	0.032	per day	hexane	0.2558	86.18	130	0.00040	0.000005	0.009	0.00061
Absolute Pressure		Pa	14.69	psi	Vented Vapor Saturation Factor	Ks	0.99	NA	benzene	1.5891	78.11	130	0.00250	0.000036	0.009	0.00415
Ideal Gas Constant		R	10.73	psia ft ³ /lb-mole R	Constant; Number of Daily Events in a Year	365		days/month	2,2,4 TMP	0.0000	114.23	130	0.00000	0.000000	0.009	-
Product Information		Distillate Fuel Oil No.2			Working Losses; Eq. 1-35, $Lw = VQ \cdot KN \cdot Kp \cdot Wv \cdot KB$	Lw	598.32	lb/month	toluene	14.7923	92.14	130	0.02323	0.000282	0.009	0.03277
Product Type					Net Working Loss Throughput (Eq. 1-39: $VQ=5.614 \cdot Q$)	VQ	12,829.821	ft3/month	ethylbenzene	1.9448	106.17	130	0.00305	0.000032	0.009	0.00374
Vapor Molecular weight		Mv	130	lb/lb-mole	Working Loss Turnover Factor Eq. 1-35 $K_{v,i}=(180+N)/6N$ for $N \geq 36$, else $K_{v,i}$	KN	0.2369		xylenes	37.8805	106.17	130	0.05948	0.000627	0.009	0.07283
Average organic liquid density		WL	7.10	lb/gal	Working Loss Product Factor	Kp	1.00		naphthalene	0.2942	128.17	130	4.46E-04	3.89E-06	0.009	4.53E-04
Average Reid Vapor Pressure		RVP	0.02		Stock Vapor Density	Wv	0.0002	lb/ft3	cumene	0.0000	120.19	130	0.00E+00	0.00E+00	0.009	0.00E+00
Product factor; 0.4 for crude oils or 1 for other organic liquids		Kc	1.00		Vent Setting Correction Factor	KB	1.00		Liquid Mole Fraction		Component Vapor Pressure					
Vapor Pressure Equation Constant A		A	12.10		Vented Vapor Saturation Factor; Eq. 1-21, $Ks = 1/(1+0.053 \cdot PVA \cdot Hvo)$	Ks	0.99		Individual HAPS	Z_i	M_i	M_j	X_i	Eq. 40-4 $x_i = (Z_i M_i) / M_i$		
Vapor Pressure Equation Constant B (Table 7.1-2)		B	8907.0	°R	Vapor Pressure at Avg Daily Liq Surface Temp	PvA	0.0086	psia	hexane	0.000001	188	86.18	0.00000	6.878	1171.5	224.37
Tank design data					Vapor Space Outage	Hvo	19.22	ft	benzene	0.00001	188	78.11	0.00002	6.906	1211	220.79
Shell height		Hs	36.00	ft	Vapor Space Expansion Factor (Eq. 1-5: $(\Delta T_v/TLA) + ((\Delta P_v - \Delta P_B)/(PA - PVA))$)	KE	0.0319	per day	2,2,4 TMP	0.00000	188	114.23	0.00000	6.812	1257.8	220.74
Diameter		D	117.00	ft	Average Daily Vapor Temperature Range	ΔT_v	15.45	°R	toluene	0.00032	188	92.14	0.00065	7.017	1377.6	222.64
Throughput		Q	95,983,697	gal/month	Average Daily Vapor Pressure Range	ΔP_v	0.0015	psi	ethylbenzene	0.00013	188	106.17	0.00023	6.95	1419.3	212.61
Turnovers		N	427.02	per year	Average Daily Vapor Pressure Range	ΔP_v	0.0015	psi	xylenes	0.00290	188	106.17	0.00514	7.009	1462.3	215.11
Roof Type:		Cone			Breather Vent Pressure Setting Range (Equation 1-10: $\Delta P_B = PBP - PBV$)	ΔP_B	0.0000	psi	naphthalene	0.00076	188	128.17	0.00111	7.146	1831.6	211.82
Tank Cone Roof Slope (If unknown, use 0.0625)		SR	0.0625	ft/ft	Vapor Pressure at Avg Daily Liq Surface Temp	PvA	0.0086	psia	cumene	0.00000	188	120.19	0.00000	6.929	1455.8	207.2
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))		RR	NA	ft	Average Daily Liquid Surface Temperature	TLA	528.39	°R	Component Vapor Pressure							
Maximum Filling Height (use Hs-1 if unknown)		HLX	35.00	ft	Atmospheric Pressure	PA	14.69	psia	Eq. 40-4 $x_i = (Z_i M_i) / M_i$							
Minimum Filling Height (use 1 ft if unknown)		HLN	1.00	ft					Eq. 40-5 $y_i = P_i / PVA$							
Liquid height (assume 1/2 Hs)		HL	18.00	ft	Average Daily Vapor Temperature Range (ΔT_v)				Eq. 40-6 $Zvi = y_i M_i / MV$							
Tank Insulation (pick from drop down list)		Not Insulated			Average daily ambient temperature range - Equation 1-11 ($\Delta TA = TAX - TAN$)	ΔTA	14.5	°R	Eq. 40-5 $y_i = P_i / PVA$							
Tank Construction (pick from drop down list)		Riveted			Not Insulated - Equation 1-7 ($\Delta T_v = 0.7 \Delta TA + 0.02 \sigma I$)	ΔT_v	16.75	°R	Eq. 40-5 $y_i = P_i / PVA$							
Tank Shell Color (pick from drop down list)		White			Partially Insulated - Equation 1-8 ($\Delta T_v = 0.6 \Delta TA + 0.02 \sigma R I$)	ΔT_v	15.30	°R	Eq. 40-5 $y_i = P_i / PVA$							
Tank Shell Condition (pick from drop down list)		Average			Fully Insulated, constant temperature	ΔT_v	0.00	°R	Eq. 40-5 $y_i = P_i / PVA$							
Tank Interior Condition (pick from drop down list)		Light Rust			Average Daily Vapor Pressure Range (ΔP_v)				Eq. 40-5 $y_i = P_i / PVA$							
Tank paint solar absorptance, dimensionless; Table 7.1-6		α	0.25		Not Insulated - Equation 1-9: $\Delta P_v = PVX - PVN$	ΔP_v	0.00230	psia	Eq. 40-5 $y_i = P_i / PVA$							
Breather Vent Setting Range (Default Assumption: +/- 0.03)		PBP	0.03	psi	Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25 $PVX = \exp(PV)$)	PvX	0.00982	psia	Eq. 40-5 $y_i = P_i / PVA$							
Breather Vent Setting Range (Default Assumption: +/- 0.03)		PBP	-0.03	psi	Vapor pressure at ave daily min liquid surface temp. (Eq. 1-25 $PVN = \exp(PV)$)	PvN	0.00752	psia	Eq. 40-5 $y_i = P_i / PVA$							
True Vapor Pressure; Eq. 1-25, $PVA = \exp(A-(B/TLA))$					Average daily max. liquid surface temp.; Fig. 7.1-17 $TLX = TLA + 0.25 \Delta T_v$	TLX	532.58	°R	Eq. 40-5 $y_i = P_i / PVA$							
Not Insulated		PVA	0.008602181		Average daily min. liquid surface temp.; Fig. 7.1-17 $TLN = TLA - 0.25 \Delta T_v$	TLN	524.21	°R	Eq. 40-5 $y_i = P_i / PVA$							
Partially Insulated		PVA	0.008629387						Eq. 40-5 $y_i = P_i / PVA$							
Fully Insulated		PVA	0.008264058		Partially Insulated - Equation 1-9: $\Delta P_v = PVX - PVN$	ΔP_v	0.00211	psia	Eq. 40-5 $y_i = P_i / PVA$							
Average Daily Ambient Temperature (TAA) Eq. 1-30 $TAA = ((TAX+TAN)/2)$		TAA	526.15	°R	Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25 use PvX)	PvX	0.00974	psia	Eq. 40-5 $y_i = P_i / PVA$							
Average daily maximum ambient temperature; Table 7.1-7		TAX	533.40	°R	Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25 use PvN)	PvN	0.0076317	psia	Eq. 40-5 $y_i = P_i / PVA$							
Average daily minimum ambient temperature; Table 7.1-7		TAN	519.90	°R	Average daily maximum liquid surface temperature, deg R ($TLX = TLA + 0.25 \Delta T_v$)	TLX	532.32	°R	Eq. 40-5 $y_i = P_i / PVA$							
Liquid Bulk Temperature; Eq. 1-31: $TB = TAA + 0.003 \sigma I$		TB	527.14	°R	Average daily minimum liquid surface temperature, deg R ($TLN = TLA - 0.25 \Delta T_v$)	TLN	524.67	°R	Eq. 40-5 $y_i = P_i / PVA$							
Average Daily Liquid Surface Temperature (TLA)					Fully Insulated ($\Delta P_v = 0$)	ΔP_v	0.00	psia	Eq. 40-5 $y_i = P_i / PVA$							
Not Insulated; Eq. 1-28, $TLA = 0.4 \cdot TAA + 0.6 \cdot TB + 0.005 \sigma I$		TLA	528.39	°R	Vapor Space Volume (Eq. 1-3: $Vv = ((\pi/4) D^2 Hvo)$)	Vv	206,626.84	ft3	Eq. 40-5 $y_i = P_i / PVA$							
Partially Insulated; Eq. 1-29, $TLA = 0.3 \cdot TAA + 0.7 \cdot TB + 0.005 \sigma I$		TLA	528.49	°R	Tank diameter	D	117.00	ft	Eq. 40-5 $y_i = P_i / PVA$							
Fully Insulated; $TLA = TB$		TLA	527.1	°R	Vapor Space Outage; see Equation 1-16	Hvo	19.22	ft	Eq. 40-5 $y_i = P_i / PVA$							
Average Vapor Temperature (Tv)					Vapor Space Outage (Eq. 1-16: $Hvo = Hs + HL + HRO$)	Hvo	19.22	ft	Eq. 40-5 $y_i = P_i / PVA$							
Not Insulated; Eq. 1-33, $Tv = 0.7 \cdot TAA + 0.3 \cdot TB + 0.009 \sigma I$		Tv	529.42	°R	Tank shell height	Hs	36.00	ft	Eq. 40-5 $y_i = P_i / PVA$							
Partially Insulated; Eq. 1-34, $Tv = 0.6 \cdot TAA + 0.4 \cdot TB + 0.01 \sigma I$		Tv	529.85	°R	Liquid Height	HL	18.00	ft	Eq. 40-5 $y_i = P_i / PVA$							
Fully Insulated; $Tv = TB$		Tv	527.14	°R	Roof Outage (for a Cone Roof vs Dome Roof)	HRO	1.22	ft	Eq. 40-5 $y_i = P_i / PVA$							
Stock Vapor Density; Eq. 1-22, $Wv = (Mv \cdot PVA) / (R \cdot Tv)$					Roof Outage - Cone Roof (Eq. 1-17 & 1-18: $HRO = (1/3) SR \cdot Rs$)	HRO	1.22	ft	Eq. 40-5 $y_i = P_i / PVA$							
Not Insulated		Wv	1.968E-04		Tank cone roof slope (If unknown, use 0.0625)	SR	0.0625	ft/ft	Eq. 40-5 $y_i = P_i / PVA$							
Partially Insulated		Wv	1.973E-04		Tank shell radius	Rs	58.50	ft	Eq. 40-5 $y_i = P_i / PVA$							
Fully Insulated		Wv	1.899E-04		Roof Outage - Dome Roof (Eq. 1-19 & 1-20: $HRO = (RR \cdot (RR^2 + R_s^2)^{0.5}) / (0.5 + 0.166 RR)$)	HRO	8.03	ft	Eq. 40-5 $y_i = P_i / PVA$							
					Tank dome roof radius (If unknown, use tank diameter (D) or (2Rs))	RR	117.00	ft	Eq. 40-5 $y_i = P_i / PVA$							
					Tank shell radius	Rs	58.50	ft	Eq. 40-5 $y_i = P_i / PVA$							

Monthly Calculations (continued)

OCTOBER

Tank No.	17413	Symbol	Units	ROUTINE EMISSIONS CALCULATIONS	Symbol	Units	HAPS Speciation	lb/month	Product	lb/month	Vapor Weight Concentrations	Vapor Mole Fraction				
ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS			HAPS Speciation		Product	lb/month	Vapor Weight Concentrations		Vapor Mole Fraction			
Total Losses (Eq. 1-1: LT = LS+LW)		LT	443.69	lb/month	Standing Losses; Eq. 1-2, $LS = 365 (Vv \cdot Wv \cdot KE \cdot Ks)$	Ls	26.01	lb/month	Diesel	39.167	Eq. 40-6 $Zvi = y_i M_i / MV$		Eq. 40-5 $y_i = P_i / PVA$			
Time Period		October	2.22E-01	ton/month	Vapor Space Volume	Vv	206626.8	ft3	Total HAP Emissions =	39.167	Eq. 40-2 $L_i = Z_i(L_i)$		Eq. 40-5 $y_i = P_i / PVA$			
Nearest US Location		Bridgeport, CT			Stock Vapor Density	Wv	0.0001	lb/ft3	Individual HAPS	L_{ij} (lb/yr)	M_i	M_j	Z_{ij}	$P_i = P_{v,i}(X_i)$	PVA	y_i
Daily total solar insolation on a horizontal surface; Table 7.1-7		I	948.0	Btu/ft ² -day	Vapor Space Expansion Factor ($0 < KE \leq 1$); Eq. 1-5	KE	0.030	per day	hexane	0.1937	86.18	130	0.00044	0.000004	0.008	0.00066
Absolute Pressure		Pa	14.69	psi	Vented Vapor Saturation Factor	Ks	0.99	NA	benzene	1.1794	78.11	130	0.00256	0.000026	0.008	0.00442
Ideal Gas Constant		R	10.73	psia ft ³ /lb-mole R	Constant; Number of Daily Events in a Year	365		days/month	2,2,4 TMP	0.0000	114.23	130	0.00000	0.000000	0.008	-
Product Information		Distillate Fuel Oil No.2			Working Losses; Eq. 1-35, $Lw = VQ \cdot KN \cdot Kp \cdot Wv \cdot KB$	Lw	417.68	lb/month	toluene	10.5526	92.14	130	0.02378	0.000195	0.008	0.03556
Product Type					Net Working Loss Throughput (Eq. 1-39: $VQ=5.614 \cdot Q$)	VQ	12,829.821	ft3/month	ethylbenzene	1.3262	106.17	130	0.00299	0.000021	0.008	0.00366
Vapor Molecular weight		Mv	130	lb/lb-mole	Working Loss Turnover Factor Eq. 1-35 $K_{v,i}=(180+N)/6N$ for $N \geq 36$, else $K_{v,i}$	KN	0.2393		xylenes	25.7434	106.17	130	0.05802	0.000413	0.008	0.07104
Average organic liquid density		WL	7.10	lb/gal	Working Loss Product Factor	Kp	1.00		naphthalene	0.1712	128.17	130	3.86E-04	2.27E-06	0.008	3.91E-04
Average Reid Vapor Pressure		RVP	0.02		Stock Vapor Density	Wv	0.0001	lb/ft3	cumene	0.0000	120.19	130	0.00E+00	0.00E+00	0.008	0.00E+00
Product factor; 0.4 for crude oils or 1 for other organic liquids		Kc	1.00		Vent Setting Correction Factor	KB	1.00		Liquid Mole Fraction		Component Vapor Pressure					
Vapor Pressure Equation Constant A		A	12.10		Vented Vapor Saturation Factor; Eq. 1-21, $Ks = 1/(1+0.053 \cdot PVA \cdot Hvo)$	Ks	0.99		Individual HAPS	Z_i	M_i	M_j	X_i	Eq. 40-4 $x_i = (Z_i M_i) / M_i$		
Vapor Pressure Equation Constant B (Table 7.1-2)		B	8907.0	°R	Vapor Pressure at Avg Daily Liq Surface Temp	PvA	0.0086	psia	hexane	0.000001	188	86.18	0.00000	6.878	1171.5	224.37
Tank design data					Vapor Space Outage	Hvo	19.22	ft	benzene	0.00001	188	78.11	0.00002	6.906	1211	220.79
Shell height		Hs	36.00	ft	Vapor Space Expansion Factor (Eq. 1-5: $(\Delta T_v/TLA) + ((\Delta P_v - \Delta P_B)/(PA - PVA))$)	KE	0.0300	per day	2,2,4 TMP	0.00000	188	114.23	0.00000	6.812	1257.8	220.74
Diameter		D	117.00	ft	Average Daily Vapor Temperature Range	ΔT_v	15.45	°R	toluene	0.00032	188	92.14	0.00065	7.017	1377.6	222.64
Throughput		Q	95,983,697	gal/month	Average Daily Vapor Pressure Range	ΔP_v	0.0015	psi</								

Monthly Calculations (continued)

MARCH

Tank No.	17415		Units	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	HAPS Speciation	lb/month	
	ROUTINE EMISSIONS CALCULATIONS	Symbol		Symbol	Units					
	Total Losses (Eq. 1-1: LT = LS+LW)	LT	95.35	lb/month	Standing Losses: Eq. 1-2, $LS = 365 (Vv \cdot Wv \cdot KE \cdot Ks)$	LS	5.85	lb/month	Product	Diesel
			4.77E-02	ton/month	Vapor Space Volume	Vv	73168.7	ft ³	Total HAP Emissions =	8.261
					Stock Vapor Density	Wv	0.0001	lb/ft ³	Eq. 40-2 $L_{ij} = Z_{ij}(L_i)$	
					Vapor Space Expansion Factor ($0 < KE < 1$); Eq. 1-5	KE	0.031	per day	Individual HAPS	L_{ij} (lb/yr)
	Nearest US Location	Bridgeport, CT			Vented Vapor Saturation Factor	Ks	1.00	NA	hexane	0.0464
	Daily total solar insolation on a horizontal surface; Table 7.1-7	I	1156.0	Btu/ft ² -day	Constant; Number of Daily Events in a Year	365	31	days/month	benzene	0.2747
	Absolute Pressure	Pa	14.69	psi					2,2,4 TMP	0.0000
	Ideal Gas Constant	R	10.73	psia ft ³ /lb-mole R	Working Losses: Eq. 1-35, $Lw = VQ \cdot KN \cdot Kp \cdot Wv \cdot KB$	Lw	89.50	lb/month	toluene	2.3285
	Product Information				Net Working Loss Throughput (Eq. 1-39, $VQ=5.614 \cdot Q$)	VQ	4,558.096	ft ³ /month	ethylbenzene	0.2746
	Product Type	Distillate Fuel Oil No.2			Working Loss Turnover Factor Eq. 1-35 $K_{in}=(180+N)/6N$ for N>36, else $K_{in} = 1$	KN	0.2368		xylene	5.3073
	Vapor Molecular weight	Mv	130	lb/lb-mole	Working Loss Product Factor	Kp	1.00		naphthalene	0.0299
	Average organic liquid density	WL	7.10	lb/gal	Stock Vapor Density	Wv	0.0001	lb/ft ³	cumene	0.0000
	Average Reid Vapor Pressure	RVP	0.02	psi	Vent Setting Correction Factor	KB	1.00			
	Product factor; 0.4 for crude oils or 1 for other organic liquids	Kc	1.00							
	Vapor Pressure Equation Constant A	A	12.10		Vented Vapor Saturation Factor: Eq. 1-21, $Ks = 1/(1+0.053 \cdot PVA \cdot Hvo)$	Ks	1.00		Individual HAPS	Z_{ij}
	Vapor Pressure Equation Constant B (Table 7.1-2)	B	8907.0	°R	Vapor Pressure at Avg Daily Liq Surface Temp	PvA	0.0034	psia	hexane	0.00000
					Vapor Space Outage	Hvo	15.31	ft	benzene	0.00001
	Tank design data								2,2,4 TMP	0.00000
	Shell height	Hs	29.00	ft	Vapor Space Expansion Factor (Eq. 1-5: $(\Delta T_v/TLA) \cdot [(APv-\Delta PB)/(PA-PvA)]$)	KE	0.0315	per day	toluene	0.00032
	Diameter	D	78.00	ft	Average Daily Vapor Temperature Range	ΔT_v	15.72	°R	ethylbenzene	0.00013
	Throughput	Q	34,100,469	gal/month	Average Daily Vapor Pressure Range	ΔP_v	0.0010	psi	xylene	0.00290
	Turnovers	N	415.98	per year	Breather Vent Pressure Setting Range (Equation 1-10: $\Delta PB = PBP - PBV$)	ΔPB	0.0000	psi	naphthalene	0.00076
	Roof Type:	Cone			Vapor Pressure at Avg Daily Liq Surface Temp	PvA	0.0034	psia	cumene	0.00000
	Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft	Average Daily Liquid Surface Temperature	TLA	500.87	°R		
	Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA	ft	Atmospheric Pressure	Pa	14.69	psia		
	Maximum Filling Height (use Hs-1 if unknown)	HLX	28.00	ft						
	Minimum Filling Height (use 1 ft if unknown)	HLN	1.00	ft	Average Daily Vapor Temperature Range (ΔT_v)					
	Liquid height (assume 1/2 Hs)	HL	14.50	ft	Average daily ambient temperature range - Equation 1-11 ($\Delta TA = TAX - TAN$)	ΔTA	14.2	°R		
	Tank Insulation (pick from drop down list)		Not Insulated		Not Insulated - Equation 1-7 ($\Delta T_v = 0.7 \Delta TA + 0.02 \sigma$)	ΔT_v	15.72	°R		
	Tank Construction (pick from drop down list)		Riveted		Partially Insulated - Equation 1-8 ($\Delta T_v = 0.6 \Delta TA + 0.02 \sigma R$)	ΔT_v	14.30	°R		
	Tank Shell Color (pick from drop down list)		White		Fully Insulated, constant temperature	ΔT_v	0.00	°R		
	Tank Shell Condition (pick from drop down list)		Average							
	Tank Interior Condition (pick from drop down list)		Light Rust		Average Daily Vapor Pressure Range (ΔP_v)					
	Tank paint solar absorptance, dimensionless; Table 7.1-6	α	0.25		Not Insulated - Equation 1-9: $\Delta P_v = PVX - PVN$	ΔP_v	0.00095	psia		
	Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	-0.03	psi	Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25 $PvX = exp$)	PvX	0.00391	psia		
					Vapor pressure at ave daily min liquid surface temp. (Eq. 1-25 $PvN = exp$)	PvN	0.00296	psia		
	True Vapor Pressure; Eq. 1-25, $PvA = exp(A-B/TLA)$				Average daily max. liquid surface temp.; Fig. 7.1-17 $TLX = TLA + 0.25 \Delta T_v$	TLX	504.80	°R		
	Not Insulated	PvA	0.003405962		Average daily min. liquid surface temp.; Fig. 7.1-17 $TLN = TLA - 0.25 \Delta T_v$	TLN	496.94	°R		
	Partially Insulated	PvA	0.003416461							
	Fully Insulated	PvA	0.003275433		Partially Insulated - Equation 1-9: $\Delta P_v = PVX - PVN$	ΔP_v	0.00087	psia		
					Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25 usl)	PvX	0.00388	psia		
	Average Daily Ambient Temperature (TAA) Eq. 1-30 $TAA = ((TAX+TAN)/2)$	TAA	498.90	°R	Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25 usl)	PvN	0.0030066	psia		
	Average daily maximum ambient temperature; Table 7.1-7	TAX	506.00	°R						
	Average daily minimum ambient temperature; Table 7.1-7	TAN	491.80	°R						
	Liquid Bulk Temperature; Eq. 1-31: $TB = TAA + 0.003 \sigma$	TB	499.77	°R	Fully Insulated ($\Delta P_v = 0$)	ΔP_v	0.00	psia		
	Average Daily Liquid Surface Temperature (TLA)				Vapor Space Volume (Eq. 1-3: $Vv = (PI/4) D^2 Hvo$)	Vv	73,168.67	ft ³		
	Not Insulated; Eq. 1-28, $TLA = 0.4 \cdot TAA + 0.6 \cdot TB + 0.005 \cdot \sigma$	TLA	500.87	°R	Tank diameter	D	78.00	ft		
	Partially Insulated; Eq. 1-29, $TLA = 0.3 \cdot TAA + 0.7 \cdot TB + 0.005 \cdot \sigma R$	TLA	500.95	°R	Vapor Space Outage; see Equation 1-16	Hvo	15.31	ft		
	Fully Insulated; $TLA = TB$	TLA	499.8	°R						
					Vapor Space Outage (Eq. 1-16: $Hvo=Hs-HL+HRO$)	Hvo	15.31	ft		
	Average Vapor Temperature (Tv)				Tank shell height	Hs	29.00	ft		
	Not Insulated; Eq. 1-33, $Tv = 0.7 \cdot TAA + 0.3 \cdot TB + 0.009 \cdot \sigma$	Tv	501.76	°R	Liquid Height	HL	14.50	ft		
	Partially Insulated; Eq. 1-34, $Tv = 0.6 \cdot TAA + 0.4 \cdot TB + 0.01 \cdot \sigma R$	Tv	502.14	°R	Roof Outage (for a Cone Roof vs Dome Roof)	HRO	0.81	ft		
	Fully Insulated; $Tv = TB$	Tv	499.77	°R						
					Roof Outage - Cone Roof (Eq. 1-17 & 1-18: $HRO=(1/3)SR \cdot Rs$)	HRO	0.81	ft		
	Stock Vapor Density; Eq. 1-22, $Wv = (Mv \cdot PvA)/(R \cdot Tv)$				Tank cone roof slope (If unknown, use 0.0625)	SR	0.0625	ft/ft		
	Not Insulated	Wv	8.223E-05		Tank shell radius	Rs	39.00	ft		
	Partially Insulated	Wv	8.242E-05							
	Fully Insulated	Wv	7.940E-05		Roof Outage - Dome Roof (Eq. 1-19 & 1-20: $HRO=(RR \cdot (RR^2+Rs^2)^{0.5})/(0.5+0.166R)$)	HRO	5.35	ft		
					Tank dome roof radius (If unknown, use tank diameter (D) or (2Rs))	RR	78.00	ft		
					Tank shell radius	Rs	39.00	ft		

Monthly Calculations (continued)

APRIL

Tank No.	17415		Units	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	HAPS Speciation	lb/month	
	ROUTINE EMISSIONS CALCULATIONS	Symbol		Symbol	Units					
	Total Losses (Eq. 1-1: LT = LS+LW)	LT	135.41	lb/month	Standing Losses: Eq. 1-2, $LS = 365 (Vv \cdot Wv \cdot KE \cdot Ks)$	LS	9.12	lb/month	Product	Diesel
			6.77E-02	ton/month	Vapor Space Volume	Vv	73168.7	ft ³	Total HAP Emissions =	11.896
					Stock Vapor Density	Wv	0.0001	lb/ft ³	Eq. 40-2 $L_{ij} = Z_{ij}(L_i)$	
					Vapor Space Expansion Factor ($0 < KE < 1$); Eq. 1-5	KE	0.036	per day	Individual HAPS	L_{ij} (lb/yr)
	Nearest US Location	Bridgeport, CT			Vented Vapor Saturation Factor	Ks	1.00	NA	hexane	0.0611
	Daily total solar insolation on a horizontal surface; Table 7.1-7	I	1490.0	Btu/ft ² -day	Constant; Number of Daily Events in a Year	365	30	days/month	benzene	0.3689
	Absolute Pressure	Pa	14.69	psi					2,2,4 TMP	0.0000
	Ideal Gas Constant	R	10.73	psia ft ³ /lb-mole R	Working Losses: Eq. 1-35, $Lw = VQ \cdot KN \cdot Kp \cdot Wv \cdot KB$	Lw	126.29	lb/month	toluene	3.2481
	Product Information				Net Working Loss Throughput (Eq. 1-39, $VQ=5.614 \cdot Q$)	VQ	4,558.096	ft ³ /month	ethylbenzene	0.4007
	Product Type	Distillate Fuel Oil No.2			Working Loss Turnover Factor Eq. 1-35 $K_{in}=(180+N)/6N$ for N>36, else $K_{in} = 1$	KN	0.2365		xylene	7.7682
	Vapor Molecular weight	Mv	130	lb/lb-mole	Working Loss Product Factor	Kp	1.00		naphthalene	0.0492
	Average organic liquid density	WL	7.10	lb/gal	Stock Vapor Density	Wv	0.0001	lb/ft ³	cumene	0.0000
	Average Reid Vapor Pressure	RVP	0.02	psi	Vent Setting Correction Factor	KB	1.00			
	Product factor; 0.4 for crude oils or 1 for other organic liquids	Kc	1.00							
	Vapor Pressure Equation Constant A	A	12.10		Vented Vapor Saturation Factor: Eq. 1-21, $Ks = 1/(1+0.053 \cdot PVA \cdot Hvo)$	Ks	1.00		Individual HAPS	Z_{ij}
	Vapor Pressure Equation Constant B (Table 7.1-2)	B	8907.0	°R	Vapor Pressure at Avg Daily Liq Surface Temp	PvA	0.0050	psia	hexane	0.00000
					Vapor Space Outage	Hvo	15.31	ft	benzene	0.00001
	Tank design data								2,2,4 TMP	0.00000
	Shell height	Hs	29.00	ft	Vapor Space Expansion Factor (Eq. 1-5: $(\Delta T_v/TLA) \cdot [(APv-\Delta PB)/(PA-PvA)]$)	KE	0.0356	per day	toluene	0.00032
	Diameter	D	78.00	ft	Average Daily Vapor Temperature Range	ΔT_v	18.16	°R	ethylbenzene	0.00013
	Throughput	Q	34,100,469	gal/month	Average Daily Vapor Pressure Range	ΔP_v	0.0015	psi	xylene	0.00290
	Turnovers	N	429.85	per year	Breather Vent Pressure Setting Range (Equation 1-10: $\Delta PB = PBP - PBV$)	ΔPB	0.0000	psi	naphthalene	0.00076
	Roof Type:	Cone			Vapor Pressure at Avg Daily Liq Surface Temp	PvA	0.0050	psia	cumene	0.00000
	Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft	Average Daily Liquid Surface Temperature	TLA	511.68	°R		
	Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA	ft	Atmospheric Pressure	Pa	14.69	psia		
	Maximum Filling Height (use Hs-1 if unknown)	HLX	28.00	ft						
	Minimum Filling Height (use 1 ft if unknown)	HLN	1.00	ft	Average Daily Vapor Temperature Range (ΔT_v)					
	Liquid height (assume 1/2 Hs)	HL	14.50	ft	Average daily ambient temperature range - Equation 1-11 ($\Delta TA = TAX - TAN$)	ΔTA	15.3	°R		
	Tank Insulation (pick from drop down list)		Not Insulated		Not Insulated - Equation 1-7 ($\Delta T_v = 0.7 \Delta TA + 0.02 \sigma$)	ΔT_v	18.16	°R		
	Tank Construction (pick from drop down list)		Riveted		Partially Insulated - Equation 1-8 ($\Delta T_v = 0.6 \Delta TA + 0.02 \sigma R$)	ΔT_v	16.63	°R		
	Tank Shell Color (pick from drop down list)		White		Fully Insulated, constant temperature	ΔT_v	0.00	°R		
	Tank Shell Condition (pick from drop down list)		Average							
	Tank Interior Condition (pick from drop down list)		Light Rust		Average Daily Vapor Pressure Range (ΔP_v)					
	Tank paint solar absorptance, dimensionless; Table 7.1-6	α	0.25		Not Insulated - Equation 1-9: $\Delta P_v = PVX - PVN$	ΔP_v	0.00154	psia		
	Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	-0.03	psi	Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25 $PvX = exp$)	PvX	0.00578	psia		
					Vapor pressure at ave daily min liquid surface temp. (Eq. 1-25 $PvN = exp$)	PvN	0.00424	psia		
	True Vapor Pressure; Eq. 1-25, $PvA = exp(A-B/TLA)$				Average daily max. liquid surface temp.; Fig. 7.1-17 $TLX = TLA + 0.25 \Delta T_v$	TLX	516.22	°R		
	Not Insulated	PvA	0.004960435		Average daily min. liquid surface temp.; Fig. 7.1-17 $TLN = TLA - 0.25 \Delta T_v$	TLN	507.14	°R		
	Partially Insulated	PvA	0.004979324		Partially Insulated - Equation 1-9: $\Delta P_v = PVX - PVN$	ΔP_v	0.00141	psia		
	Fully Insulated	PvA	0.004726595		Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25 usl)	PvX	0.00573	psia		
					Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25 usl)	PvN	0.0043179	psia		
	Average Daily Ambient Temperature (TAA) Eq. 1-30 $TAA = ((TAX+TAN)/2)$	TAA	509.15	°R						
	Average daily									

Monthly Calculations (continued)

MAY

Tank No.	ROUTINE EMISSIONS CALCULATIONS		Units	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	HAPS Speciation	lb/month	Product	Diesel						
	Symbol	Value		Symbol	Value												
	Total Losses (Eq. 1-1: LT = LS+LW)	LT	187.99	lb/month	Standing Losses: Eq. 1-2, $LS = 365 (Vv \cdot Wv \cdot KE \cdot Ks)$	LS	13.72	lb/month	Total HAP Emissions =	16.671	lb/month						
			9.40E-02	ton/month	Vapor Space Volume	Vv	73168.7	ft ³	Eq. 40-2 $L_{ij} = Z_{ij}(L_i)$								
					Stock Vapor Density	Wv	0.0002	lb/ft ³	Eq. 40-6 $ZVi = y_iM_i / MV$								
					Vapor Space Expansion Factor ($0 < KE <= 1$); Eq. 1-5	KE	0.038	per day	Eq. 40-5 $y_i = P_i / PVA$								
	Nearest US Location	Bridgeport, CT			Vented Vapor Saturation Factor	Ks	0.99	NA	Individual HAPS	L_{ij} (lb/yr)	M_i	M_v	Z_{ij}	$P_i = PVA(x_i)$	PVA	y_i	
	Daily total solar insolation on a horizontal surface; Table 7.1-7	I	1750.0	Btu/ft ² -day	Constant; Number of Daily Events in a Year	365	31	days/month	hexane	0.0791	86.18	130	0.00042	0.00004	0.007	0.00063	
	Absolute Pressure	Pa	14.69	psi					benzene	0.4861	78.11	130	0.00259	0.00030	0.007	0.00430	
	Ideal Gas Constant	R	10.73	psia ft ³ /lb-mole R	Working Losses: Eq. 1-35, $Lw = VQ \cdot KN \cdot Kp \cdot Wv \cdot KB$	Lw	174.27	lb/month	2,2,4 TMP	0.0000	114.23	130	0.00000	0.00000	0.007	-	
	Product Information				Net Working Loss Throughput (Eq. 1-39; $VQ=5.614 \cdot Q$)	VQ	4,558.096	ft ³ /month	toluene	4.4264	92.14	130	0.02355	0.00023	0.007	0.03322	
	Product Type	Distillate Fuel Oil No.2			Working Loss Turnover Factor Eq. 1-35 $Kw=(180+N)/6N$ for N>36, else $Kw=$	KN	0.2388		ethylbenzene	0.5676	106.17	130	0.00302	0.00026	0.007	0.00370	
	Vapor Molecular weight	Mv	130	lb/lb-mole	Working Loss Product Factor	Kp	1.00		xylene	11.0346	106.17	130	0.05870	0.00049	0.007	0.07167	
	Average organic liquid density	WL	7.10	lb/gal	Stock Vapor Density	Wv	0.0002	lb/ft ³	naphthalene	0.0774	128.17	130	4.12E-04	2.89E-06	0.007	4.18E-04	
	Average Reid Vapor Pressure	RVP	0.02	psi	Vent Setting Correction Factor	KB	1.00		cumene	0.0000	120.19	130	0.00E+00	0.00E+00	0.007	0.00E+00	
	Product factor; 0.4 for crude oils or 1 for other organic liquids	Kc	1.00						Liquid Mole Fraction Eq. 40-4 $x_i = (Z_{i,j}M_i) / M$								
	Vapor Pressure Equation Constant A	A	12.10		Vented Vapor Saturation Factor: Eq. 1-21, $Ks = 1 / (1 + 0.053 \cdot PVA \cdot Hvo)$	Ks	0.99		Component Vapor Pressure $PVA = (0.019337)^{10} (A \cdot B \cdot (TLA + C))$								
	Vapor Pressure Equation Constant B (Table 7.1-2)	B	8907.0	°R	Vapor Pressure at Avg Daily Liq Surface Temp	PvA	0.0096	psia	Individual HAPS	Z_{ij}	M_i	M_v	X_i	A	B	C	PVA
					Vapor Space Outage	Hvo	15.31	ft	hexane	0.000001	188	86.18	0.00000	6.878	1171.5	224.37	2.0120
									benzene	0.00001	188	78.11	0.00002	6.906	1211	220.79	1.2359
									2,2,4 TMP	0.00000	188	114.23	0.00000	6.812	1257.8	220.74	0.6306
									toluene	0.00032	188	92.14	0.00065	7.017	1377.6	222.64	0.3517
									ethylbenzene	0.00013	188	106.17	0.00023	6.95	1419.3	212.61	0.1110
									xylene	0.00290	188	106.17	0.00514	7.009	1462.3	215.11	0.0967
									naphthalene	0.00076	188	128.17	0.00111	7.146	1831.6	211.82	0.0028
									cumene	0.00000	188	120.19	0.00000	6.929	1455.8	207.2	0.0515
	Tank design data				Vapor Space Expansion Factor (Eq. 1-5: $(\Delta T_v / TLA) + ((\Delta P_v - \Delta P_B) / (PVA - PVA))$)	KE	0.0380	per day									
	Shell height	Hs	29.00	ft	Average Daily Vapor Temperature Range	ΔT_v	19.74	°R									
	Diameter	D	78.00	ft	Average Daily Vapor Pressure Range	ΔP_v	0.0022	psia									
	Throughput	Q	34,100,469	gal/month	Net Working Loss Throughput (Eq. 1-39; $VQ=5.614 \cdot Q$)	VQ	4,558.096	ft ³ /month									
	Turnovers	N	415.98	per year	Breather Vent Pressure Setting Range (Equation 1-10; $\Delta P_B = PBP - PBV$)	ΔP_B	0.0000	psi									
	Roof Type:	Cone			Vapor Pressure at Avg Daily Liq Surface Temp	PvA	0.0096	psia									
	Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft	Average Daily Liquid Surface Temperature	TLA	521.63	°R									
	Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA	ft	Atmospheric Pressure	Pa	14.69	psia									
	Maximum Filling Height (use Hs-1 if unknown)	HLX	28.00	ft													
	Minimum Filling Height (use 1 if unknown)	HLN	1.00	ft	Average Daily Vapor Temperature Range (ΔT_v)												
	Liquid height (assume 1/2 Hs)	HL	14.50	ft	Average daily ambient temperature range - Equation 1-11 ($\Delta TA = TAX - TAN$)	ΔTA	15.7	°R									
	Tank Insulation (pick from drop down list)	Not Insulated			Not Insulated - Equation 1-7 ($\Delta T_v = 0.7 \Delta TA + 0.02 \sigma$)	ΔT_v	19.74	°R									
	Tank Construction (pick from drop down list)	Riveted			Partially Insulated - Equation 1-8 ($\Delta T_v = 0.6 \Delta TA + 0.02 \sigma R$)	ΔT_v	18.17	°R									
	Tank Shell Color (pick from drop down list)	White			Fully Insulated, constant temperature	ΔT_v	0.00	°R									
	Tank Shell Condition (pick from drop down list)	Average															
	Tank Interior Condition (pick from drop down list)	Light Rust			Average Daily Vapor Pressure Range (ΔP_v)												
	Tank paint solar absorptance, dimensionless; Table 7.1-6	α	0.25		Not Insulated - Equation 1-9: $\Delta P_v = PVX - PVN$	ΔP_v	0.00224	psia									
	Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	0.03	psi	Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25 $PvX = \exp$)	PvX	0.00811	psia									
					Vapor pressure at ave daily min liquid surface temp. (Eq. 1-25 $PvN = \exp$)	PvN	0.00587	psia									
					Average daily max. liquid surface temp.; Fig. 7.1-17 $TLX = TLA + 0.25 \Delta T_v$	TLX	526.56	°R									
					Average daily min. liquid surface temp.; Fig. 7.1-17 $TLN = TLA - 0.25 \Delta T_v$	TLN	516.69	°R									
	True Vapor Pressure; Eq. 1-25, $PvA = \exp(A - B/TLA)$																
	Not Insulated	PvA	0.006912076		Partially Insulated - Equation 1-9: $\Delta P_v = PVX - PVN$	ΔP_v	0.00207	psia									
	Partially Insulated	PvA	0.00694183		Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25 PvX)	PvX	0.00804	psia									
	Fully Insulated	PvA	0.006544819		Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25 PvN)	PvN	0.0059753	psia									
	Average Daily Ambient Temperature (TAA) Eq. 1-30 $TAA = ((TAX + TAN) / 2)$	TAA	518.65	°R													
	Average daily maximum ambient temperature; Table 7.1-7	TAX	526.50	°R													
	Average daily minimum ambient temperature; Table 7.1-7	TAN	510.80	°R													
	Liquid Bulk Temperature; Eq. 1-31: $TB = TAA + 0.003 \sigma$	TB	519.96	°R													
					Fully Insulated ($\Delta P_v = 0$)	ΔP_v	0.00	psia									
	Average Daily Liquid Surface Temperature (TLA)				Vapor Space Volume (Eq. 1-3: $Vv = ((\pi / 4) D^2 Hvo)$	Vv	73,168.67	ft ³									
	Not Insulated; Eq. 1-28, $TLA = 0.4 \cdot TAA + 0.6 \cdot TB + 0.005 \cdot \sigma$	TLA	521.63	°R	Tank diameter	D	78.00	ft									
	Partially Insulated; Eq. 1-29, $TLA = 0.3 \cdot TAA + 0.7 \cdot TB + 0.005 \cdot \sigma R$	TLA	521.76	°R	Vapor Space Outage; see Equation 1-16	Hvo	15.31	ft									
	Fully Insulated; $TLA = TB$	TLA	520.0	°R													
					Vapor Space Outage (Eq. 1-16: $Hvo = Hs - HL + HRO$)	Hvo	15.31	ft									
					Tank shell height	Hs	29.00	ft									
					Liquid Height	HL	14.50	ft									
					Roof Outage (for a Cone Roof vs Dome Roof)	HRO	0.81	ft									
					Roof Outage - Cone Roof (Eq. 1-17 & 1-18: $HRO = (1/3)SR \cdot Rs$)	HRO	0.81	ft									
					Tank cone roof slope (If unknown, use 0.0625)	SR	0.0625	ft/ft									
					Tank shell radius	Rs	39.00	ft									
					Roof Outage - Dome Roof (Eq. 1-19 & 1-20: $HRO = (RR \cdot (RR^2 + Rs^2)^{0.5}) / (0.5 + 0.166 RR)$)	HRO	5.35	ft									
					Tank dome roof radius (If unknown, use tank diameter (D) or (2Rs))	RR	78.00	ft									
					Tank shell radius	Rs	39.00	ft									

Monthly Calculations (continued)

JUNE

Tank No.	ROUTINE EMISSIONS CALCULATIONS		Units	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	HAPS Speciation	lb/month	Product	Diesel					
	Symbol	Value		Symbol	Value											
	Total Losses (Eq. 1-1: LT = LS+LW)	LT	252.15	lb/month	Standing Losses: Eq. 1-2, $LS = 365 (Vv \cdot Wv \cdot KE \cdot Ks)$	LS	17.74	lb/month	Total HAP Emissions =	22.510	lb/month					
			1.26E-01	ton/month	Vapor Space Volume	Vv	73168.7	ft ³	Eq. 40-2 $L_{ij} = Z_{ij}(L_i)$							
					Stock Vapor Density	Wv	0.0002	lb/ft ³	Eq. 40-6 $ZVi = y_iM_i / MV$							
					Vapor Space Expansion Factor ($0 < KE <= 1$); Eq. 1-5	KE	0.037	per day	Eq. 40-5 $y_i = P_i / PVA$							
	Nearest US Location	Bridgeport, CT			Vented Vapor Saturation Factor	Ks	0.99	NA	Individual HAPS	L_{ij} (lb/yr)	M_i	M_v	Z_{ij}	$P_i = PVA(x_i)$	PVA	y_i
	Daily total solar insolation on a horizontal surface; Table 7.1-7	I	1862.0	Btu/ft ² -day	Constant; Number of Daily Events in a Year	365	30	days/month	hexane	0.0990	86.18	130	0.00039	0.00006	0.010	0.00059
	Absolute Pressure	Pa	14.69	psi					benzene	0.8181	78.11	130	0.00245	0.00039	0.010	0.00408
	Ideal Gas Constant	R	10.73	psia ft ³ /lb-mole R	Working Losses: Eq. 1-35, $Lw = VQ \cdot KN \cdot Kp \cdot Wv \cdot KB$	Lw	234.41	lb/month	2,2,4 TMP	0.0000	114.23	130	0.00000	0.00000	0.010	-
	Product Information				Net Working Loss Throughput (Eq. 1-39; $VQ=5.614 \cdot Q$)	VQ	4,558.096	ft ³ /month	toluene							

Monthly Calculations (continued)

JULY

Tank No.	10454A	Symbol	Units	ROUTINE EMISSIONS CALCULATIONS	Symbol	Units
ROUTINE EMISSIONS CALCULATIONS						
Total Losses (Eq. 1-1: $LT = LS + LW$)	LT	5.35	lb/month	Standing Losses: Eq. 1-2, $LS = 365 (Vv \cdot Wv \cdot KE \cdot Ks)$	LS	2.10 lb/month
Nearest US Location	Bridgeport, CT			Vapor Space Volume	Vv	549.8 ft ³
Daily total solar insolation on a horizontal surface; Table 7.1-7	I	1904.0	Btu/ft ² -day	Stock Vapor Density	Wv	0.0038 lb/ft ³
Absolute Pressure	Pa	14.69	psia	Vapor Space Expansion Factor ($0 < KE \leq 1$); Eq. 1-5	KE	0.032 per day
Ideal Gas Constant	R	10.73	psia ft ³ /lb-mole R	Vented Vapor Saturation Factor	Ks	1.00 NA
Product Information						
Product Type	Diesel Additive			Constant: Number of Daily Events in a Year	365	31 days/month
Vapor Molecular weight	Mv	130	lb/lb-mole	Working Losses: Eq. 1-35, $LW = VQ \cdot KN \cdot Kp \cdot Wv \cdot KB$	LW	3.25 lb/month
Average organic liquid density	WL	6.10	lb/gal	Net Working Loss Throughput (Eq. 1-39: $VQ = 5.614 \cdot Q$)	VQ	855 ft ³ /month
Average Reid Vapor Pressure	RVP	0.00	psi	Working Loss Turnover Factor Eq. 1-35 $Ks = (180 + N)/N$ for $N > 36$, else $Ks = N$	KN	1.0000
Product factor: 0.4 for crude oils or 1 for other organic liquids	Kc	1.00		Working Loss Product Factor	Kp	1.00
Vapor Pressure Equation Constant A	A	0.00		Stock Vapor Density	Wv	0.0038 lb/ft ³
Vapor Pressure Equation Constant B (Table 7.1-2)	B	0.0	R	Vent Setting Correction Factor	KB	1.00
Tank design data						
Shell height	Hs	7.85	ft	Vented Vapor Saturation Factor; Eq. 1-21, $Ks = 1/(1+0.053 \cdot PVA \cdot Hvo)$	Ks	1.00
Diameter	D	13.35	ft	Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.1632 psia
Throughput	Q	6,400	gal/month	Vapor Space Outage	Hvo	0.00 ft
Turnovers	N	9.16	per year	Vapor Space Expansion Factor (Eq. 1-5: $(\Delta Tv/TLA) + ((\Delta Pv - \Delta Pb)/(PA - PVA))$)	KE	0.0296 per day
Roof Type:		0.00		Average Daily Vapor Temperature Range	ΔTv	18.09 °R
Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft	Average Daily Vapor Pressure Range	ΔPv	0.00000 psia
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA	ft	Breather Vent Pressure Setting Range (Equation 1-10: $\Delta Pb = PBP - PBV$)	ΔPb	0.0600 psi
Maximum Filling Height - use (Pi/4)D if unknown	HLX	6.85	ft	Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.1632 psia
Minimum Filling Height (use 0 if unknown)	HLN	1.00	ft	Average Daily Liquid Surface Temperature	TLA	537.14 °R
Liquid height (assume 1/2 H)	HL	3.93	ft	Atmospheric Pressure	PA	14.69 psia
Tank insulation (pick from drop down list)		Not Insulated		Average Daily Vapor Temperature Range (ΔTv)		
Tank Construction (pick from drop down list)		Welded		Not Insulated - Equation 1-7 ($\Delta Tv = 0.7 \Delta TA + 0.92 \alpha I$)	ΔTv	18.09 °R
Tank Shell Color (pick from drop down list)		White		Partially Insulated - Equation 1-8 ($\Delta Tv = 0.6 \Delta TA + 0.02 \alpha R I$)	ΔTv	18.16 °R
Tank Shell Condition (pick from drop down list)		Average		Fully Insulated, constant temperature	ΔTv	0.00 °R
Tank Interior Condition (pick from drop down list)		Light Rust		Average Daily Vapor Pressure Range (ΔPv)		
Tank paint solar absorptance, dimensionless; Table 7.1-6	α	0.25		Not Insulated - Equation 1-9: $\Delta Pv = PVX - PVN$	ΔPv	0.00000 psia
Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	0.03	psi	Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25: $PVX = \exp(PVA)$)	PVX	1.00000 psia
True Vapor Pressure: Eq. 1-25, $PVA = \exp(A \cdot (B/TLA))$						
Not Insulated	PVA	0.1632264	psi	Vapor pressure at ave. daily min liquid surface temp. (Eq. 1-25: $PVN = \exp(PVA)$)	PVN	1.00000 psia
Partially Insulated	PVA	0.163897	psi	Average daily max. liquid surface temp.; Fig. 7.1-17 $TLX = TLA + 0.25 \Delta T$	TLX	540.37 °R
Fully Insulated	PVA	0.1549333	psi	Average daily min. liquid surface temp.; Fig. 7.1-17 $TLN = TLA - 0.25 \Delta T$	TLN	533.91 °R
Average Daily Ambient Temperature (TAA) Eq. 1-30 $TAA = ((TAX + TAN) / 2)$						
Average daily maximum ambient temperature; Table 7.1-7	TAX	541.10	°R	Partially Insulated - Equation 1-9: $\Delta Pv = PVX - PVN$	ΔPv	0.00000 psia
Average daily minimum ambient temperature; Table 7.1-7	TAN	526.70	°R	Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25: PVX)	PVX	1.000000 psia
Liquid Bulk Temperature; Eq. 1-31: $TB = TAA + 0.003 \alpha s I$						
	TB	535.33	°R	Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25: PVN)	PVN	1.000000 psia
Average Daily Liquid Surface Temperature (TLA)						
Not Insulated; Eq. 1-28, $TLA = 0.4 \cdot TAA + 0.6 \cdot TB + 0.005 \cdot \alpha I$	TLA	537.14	°R	Vapor Space Volume (Eq. 1-3: $Vv = ((\pi/4) D^2 Hvo)$)	Vv	549.78 ft ³
Partially Insulated; Eq. 1-29, $TLA = 0.3 \cdot TAA + 0.7 \cdot TB + 0.005 \cdot \alpha R I$	TLA	537.28	°R	Effective Tank diameter	D _e	13.35 ft
Fully Insulated; $TLA = TB$	TLA	535.3	°R	Effective Tank Height	H _e	7.85 ft
Average Vapor Temperature (Tv)						
Not Insulated; Eq. 1-33, $Tv = 0.7 \cdot TAA + 0.3 \cdot TB + 0.009 \cdot \alpha I$	Tv	538.61	°R	Vapor Space Outage $Hvo = 1/2 H$	Hvo	3.93 ft
Partially Insulated; Eq. 1-34, $Tv = 0.6 \cdot TAA + 0.4 \cdot TB + 0.01 \cdot \alpha R I$	Tv	539.23	°R			
Fully Insulated; $Tv = TB$	Tv	535.33	°R			
Stock Vapor Density: Eq. 1-22, $Wv = (Mv/PVA)/(R \cdot Tv)$						
Not Insulated	Wv	3.801E-03				
Partially Insulated	Wv	3.814E-03				
Fully Insulated	Wv	3.606E-03				

Product	lb/month	Vapor Weight Concentration		Vapor Mole Fraction	
Total HAP Emissions =	5.348	Eq. 40-6 $Zvi = y_i M_i / MV$	Eq. 40-5 $y_i = P_i / PVA$		
Individual HAPS	L _{ij} (lb/month)	M _i	M _v	Z _{vi}	P _i = P _{va} (x _i)
hexane	0.0000	86.18	130	0.00000	0.00000
benzene	0.0000	78.11	130	0.00000	0.00000
2,2,4 TMP	0.0000	114.23	130	0.00000	0.00000
toluene	0.0000	92.14	130	0.00000	0.00000
ethylbenzene	1.5544	106.17	130	0.29067	0.060147
xylenes	3.7933	106.17	130	0.70933	0.146776
naphthalene	0.0000	128.17	130	0.00E+00	0.00E+00
cumene	0.0000	120.19	130	0.00E+00	0.00E+00

Component Vapor Pressure	Eq. 40-4 $x_i = (Z_i M_i) / M_i$	A	B	C	P _{va}
Individual HAPS	Z _i	M _i	M _v	X _i	P _{va}
hexane	0.00000	130	86.18	0.00000	6.878
benzene	0.00000	130	78.11	0.00000	6.906
2,2,4 TMP	0.00000	130	114.23	0.00000	6.812
toluene	0.00000	130	92.14	0.00000	7.017
ethylbenzene	0.26400	130	106.17	0.32326	6.95
xylenes	0.73600	130	106.17	0.90120	7.009
naphthalene	0.00000	130	128.17	0.00000	7.148
cumene	0.00000	130	120.19	0.00000	6.929

Monthly Calculations (continued)

AUGUST

Tank No.	10454A	Symbol	Units	ROUTINE EMISSIONS CALCULATIONS	Symbol	Units
ROUTINE EMISSIONS CALCULATIONS						
Total Losses (Eq. 1-1: $LT = LS + LW$)	LT	5.00	lb/month	Standing Losses: Eq. 1-2, $LS = 365 (Vv \cdot Wv \cdot KE \cdot Ks)$	LS	1.86 lb/month
Nearest US Location	Bridgeport, CT			Vapor Space Volume	Vv	549.8 ft ³
Daily total solar insolation on a horizontal surface; Table 7.1-7	I	1685.0	Btu/ft ² -day	Stock Vapor Density	Wv	0.0037 lb/ft ³
Absolute Pressure	Pa	14.69	psia	Vapor Space Expansion Factor ($0 < KE \leq 1$); Eq. 1-5	KE	0.030 per day
Ideal Gas Constant	R	10.73	psia ft ³ /lb-mole R	Vented Vapor Saturation Factor	Ks	1.00 NA
Product Information						
Product Type	Diesel Additive			Constant: Number of Daily Events in a Year	365	31 days/month
Vapor Molecular weight	Mv	130	lb/lb-mole	Working Losses: Eq. 1-35, $LW = VQ \cdot KN \cdot Kp \cdot Wv \cdot KB$	LW	3.15 lb/month
Average organic liquid density	WL	6.10	lb/gal	Net Working Loss Throughput (Eq. 1-39: $VQ = 5.614 \cdot Q$)	VQ	855 ft ³ /month
Average Reid Vapor Pressure	RVP	0.00	psi	Working Loss Turnover Factor Eq. 1-35 $Ks = (180 + N)/N$ for $N > 36$, else $Ks = N$	KN	1.0000
Product factor: 0.4 for crude oils or 1 for other organic liquids	Kc	1.00		Working Loss Product Factor	Kp	1.00
Vapor Pressure Equation Constant A	A	0.00		Stock Vapor Density	Wv	0.0037 lb/ft ³
Vapor Pressure Equation Constant B (Table 7.1-2)	B	0.0	R	Vent Setting Correction Factor	KB	1.00
Tank design data						
Shell height	Hs	7.85	ft	Vented Vapor Saturation Factor; Eq. 1-21, $Ks = 1/(1+0.053 \cdot PVA \cdot Hvo)$	Ks	1.00
Diameter	D	13.35	ft	Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.1632 psia
Throughput	Q	6,400	gal/month	Vapor Space Outage	Hvo	0.00 ft
Turnovers	N	9.16	per year	Vapor Space Expansion Factor (Eq. 1-5: $(\Delta Tv/TLA) + ((\Delta Pv - \Delta Pb)/(PA - PVA))$)	KE	0.0296 per day
Roof Type:		0.00		Average Daily Vapor Temperature Range	ΔTv	18.09 °R
Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft	Average Daily Vapor Pressure Range	ΔPv	0.00000 psia
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA	ft	Breather Vent Pressure Setting Range (Equation 1-10: $\Delta Pb = PBP - PBV$)	ΔPb	0.0600 psi
Maximum Filling Height - use (Pi/4)D if unknown	HLX	6.85	ft	Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.1632 psia
Minimum Filling Height (use 0 if unknown)	HLN	1.00	ft	Average Daily Liquid Surface Temperature	TLA	536.06 °R
Liquid height (assume 1/2 H)	HL	3.93	ft	Atmospheric Pressure	PA	14.69 psia
Tank insulation (pick from drop down list)		Not Insulated		Average Daily Vapor Temperature Range (ΔTv)		
Tank Construction (pick from drop down list)		Welded		Not Insulated - Equation 1-7 ($\Delta Tv = 0.7 \Delta TA + 0.92 \alpha I$)	ΔTv	18.09 °R
Tank Shell Color (pick from drop down list)		White		Partially Insulated - Equation 1-8 ($\Delta Tv = 0.6 \Delta TA + 0.02 \alpha R I$)	ΔTv	16.71 °R
Tank Shell Condition (pick from drop down list)		Average		Fully Insulated, constant temperature	ΔTv	0.00 °R
Tank Interior Condition (pick from drop down list)		Light Rust		Average Daily Vapor Pressure Range (ΔPv)		
Tank paint solar absorptance, dimensionless; Table 7.1-6	α	0.25		Not Insulated - Equation 1-9: $\Delta Pv = PVX - PVN$	ΔPv	0.00000 psia
Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	0.03	psi	Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25: $PVX = \exp(PVA)$)	PVX	1.00000 psia
True Vapor Pressure: Eq. 1-25, $PVA = \exp(A \cdot (B/TLA))$						
Not Insulated	PVA	0.1632264	psi	Vapor pressure at ave. daily min liquid surface temp. (Eq. 1-25: $PVN = \exp(PVA)$)	PVN	1.00000 psia
Partially Insulated	PVA	0.163897	psi	Average daily max. liquid surface temp.; Fig. 7.1-17 $TLX = TLA + 0.25 \Delta T$	TLX	540.59 °R
Fully Insulated	PVA	0.1549333	psi	Average daily min. liquid surface temp.; Fig. 7.1-17 $TLN = TLA - 0.25 \Delta T$	TLN	531.54 °R
Average Daily Ambient Temperature (TAA) Eq. 1-30 $TAA = ((TAX + TAN) / 2)$						
Average daily maximum ambient temperature; Table 7.1-7	TAX	540.10	°R	Partially Insulated - Equation 1-9: $\Delta Pv = PVX - PVN$	ΔPv	0.00000 psia
Average daily minimum ambient temperature; Table 7.1-7	TAN	526.30	°R	Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25: PVX)	PVX	1.000000 psia
Liquid Bulk Temperature; Eq. 1-31: $TB = TAA + 0.003 \alpha s I$						
	TB	534.46	°R	Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25: PVN)	PVN	1.000000 psia
Average Daily Liquid Surface Temperature (TLA)						
Not Insulated; Eq. 1-28, $TLA = 0.4 \cdot TAA + 0.6 \cdot TB + 0.005 \cdot \alpha I$	TLA	536.06	°R	Vapor Space Volume (Eq. 1-3: $Vv = ((\pi/4) D^2 Hvo)$)	Vv	549.78 ft ³
Partially Insulated; Eq. 1-29, $TLA = 0.3 \cdot TAA + 0.7 \cdot TB + 0.005 \cdot \alpha R I$	TLA	536.19	°R	Effective Tank diameter	D _e	13.35 ft
Fully Insulated; $TLA = TB$	TLA	534.5	°R	Effective Tank Height	H _e	7.85 ft
Average Vapor Temperature (Tv)						
Not Insulated; Eq. 1-33, $Tv = 0.7 \cdot TAA + 0.3 \cdot TB + 0.009 \cdot \alpha I$	Tv	537.37	°R	Vapor Space Outage $Hvo = 1/2 H$	Hvo	3.93 ft
Partially Insulated; Eq. 1-34, $Tv = 0.6 \cdot TAA + 0.4 \cdot TB + 0.01 \cdot \alpha R I$	Tv	537.92	°R			
Fully Insulated; $Tv = TB$	Tv	534.46	°R			
Stock Vapor Density: Eq. 1-22, $Wv = (Mv/PVA)/(R \cdot Tv)$						
Not Insulated	Wv	3.680E-03				
Partially Insulated	Wv	3.691E-03				
Fully Insulated	Wv	3.512E-03				

Product	lb/month	Vapor Weight Concentration		Vapor Mole Fraction	
Total HAP Emissions =	5.005	Eq. 40-6 $Zvi = y_i M_i / MV$	Eq. 40-5 $y_i = P_i / PVA$		
Individual HAPS	L _{ij} (lb/month)	M _i	M _v	Z _{vi}	P _i = P _{va} (x _i)
hexane	0.0000	86.18	130	0.00000	0.00000
benzene	0.0000	78.11	130	0.00000	0.00000
2,2,4 TMP	0.0000	114.23	130	0.00000	0.00000
toluene	0.0000	92.14	130	0.00000	0.00000
ethylbenzene	1.4550	106.17	130	0.29074	0.058108
xylenes	3.5496	106.17	130	0.70926	0.141755
naphthalene	0.0000	128.17	130	0.00E+00	0.00E+00
cumene	0.0000	120.19	130	0.00E+00	0.00E+00

Component Vapor Pressure	Eq. 40-4 $x_i = (Z_i M_i) / M_i$	A	B	C	P _{va}
Individual HAPS	Z _i	M _i	M _v	X _i	P _{va}
hexane	0.00000	130	86.18	0.00000	6.878
benzene	0.00000	130	78.11	0.00000	6.906
2,2,4 TMP	0.00000	130	114.23	0.00000	6.812
toluene	0.00000	130	92.14	0.00000	7.017
ethylbenzene	0.26400	130	106.17	0.32326	6.95
xylenes	0.73600	130	106.17	0.90120	7.009
naphthalene	0				

Monthly Calculations (continued)

NOVEMBER

Tank No.	10454A		UNITS		ROUTINE EMISSIONS CALCULATIONS		Symbol		UNITS		
ROUTINE EMISSIONS CALCULATIONS											
Total Losses (Eq. 1-1: $LT = LS + LW$)	LT	1.66	lb/month	Standing Losses: Eq. 1-2: $LS = 365 (Vv \cdot Wv \cdot KE \cdot Ks)$	LS	0.47	lb/month	Vapor Space Volume	Vv	549.8	ft ³
		8.30E-04	ton/month	Stock Vapor Density	Wv	0.0014	lb/ft ³	Stock Vapor Density	Wv	0.0014	lb/ft ³
	Time Period	November		Vapor Space Expansion Factor ($0 < KE \leq 1$): Eq. 1-5	KE	0.021	per day	Vapor Space Expansion Factor ($0 < KE \leq 1$): Eq. 1-5	KE	0.021	per day
	Nearest US Location	Bridgeport, CT		Vented Vapor Saturation Factor	Ks	1.00	NA	Vented Vapor Saturation Factor	Ks	1.00	NA
	Daily total solar insolation on a horizontal surface; Table 7.1-7	I	621.0	Constant: Number of Daily Events in a Year	365	30	days/month	Constant: Number of Daily Events in a Year	365	30	days/month
	Absolute Pressure	Pa	14.69	Working Losses: Eq. 1-3: $Lw = VQ \cdot KN \cdot Kp \cdot Wv \cdot KB$	Lw	1.19	lb/month	Working Losses: Eq. 1-3: $Lw = VQ \cdot KN \cdot Kp \cdot Wv \cdot KB$	Lw	1.19	lb/month
	Ideal Gas Constant	R	10.73	Net Working Loss Throughput (Eq. 1-39: $VQ = 5.614 \cdot Q$)	VQ	855	ft ³ /month	Net Working Loss Throughput (Eq. 1-39: $VQ = 5.614 \cdot Q$)	VQ	855	ft ³ /month
Product Information											
Product Type	Diesel Additive			Working Loss Turnover Factor Eq. 1-35: $Ks = (180 + N)/N$ for $N > 36$, else $Ks = KN$	KN	1.0000		Working Loss Turnover Factor Eq. 1-35: $Ks = (180 + N)/N$ for $N > 36$, else $Ks = KN$	KN	1.0000	
Vapor Molecular weight	Mv	130	lb/lb-mole	Working Loss Product Factor	Kp	1.00		Working Loss Product Factor	Kp	1.00	
Average organic liquid density	WL	6.10	lb/gal	Stock Vapor Density	Wv	0.0014	lb/ft ³	Stock Vapor Density	Wv	0.0014	lb/ft ³
Average Reid Vapor Pressure	RVP	0.00		Vent Setting Correction Factor	KB	1.00		Vent Setting Correction Factor	KB	1.00	
Product factor: 0.4 for crude oils or 1 for other organic liquids	Kc	1.00		Vented Vapor Saturation Factor: Eq. 1-21: $Ks = 1/(1 + 0.053 \cdot PVA \cdot Hvo)$	Ks	1.00		Vented Vapor Saturation Factor: Eq. 1-21: $Ks = 1/(1 + 0.053 \cdot PVA \cdot Hvo)$	Ks	1.00	
Vapor Pressure Equation Constant A	A	0.0		Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.0581	psia	Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.0581	psia
Vapor Pressure Equation Constant B (Table 7.1-2)	B	0.0		Vapor Space Outage	Hvo	0.00	ft	Vapor Space Outage	Hvo	0.00	ft
Tank design data											
Shell height	Hs	7.85	ft	Vapor Space Expansion Factor (Eq. 1-5: $(\Delta Tv/TLA) + ((\Delta Pv - \Delta Pb)/(PA - PVA))$)	KE	0.0207	per day	Vapor Space Expansion Factor (Eq. 1-5: $(\Delta Tv/TLA) + ((\Delta Pv - \Delta Pb)/(PA - PVA))$)	KE	0.0207	per day
Diameter	D	13.35	ft	Average Daily Vapor Temperature Range	ΔTv	12.56	°R	Average Daily Vapor Temperature Range	ΔTv	12.56	°R
Throughput	Q	6.400	gal/month	Average Daily Vapor Pressure Range	ΔPv	0.0000	psia	Average Daily Vapor Pressure Range	ΔPv	0.0000	psia
Turnovers	N	9.47	per year	Breather Vent Pressure Setting Range (Equation 1-10: $\Delta Pb = PBP - PBV$)	ΔPb	0.0600	psi	Breather Vent Pressure Setting Range (Equation 1-10: $\Delta Pb = PBP - PBV$)	ΔPb	0.0600	psi
Roof Type:		0.00		Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.0581	psia	Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.0581	psia
Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft	Average Daily Liquid Surface Temperature	TLA	506.41	°R	Average Daily Liquid Surface Temperature	TLA	506.41	°R
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA	ft	Atmospheric Pressure	PA	14.69	psia	Atmospheric Pressure	PA	14.69	psia
Maximum Filling Height - use (Pi/4)D if unknown	HLX	6.85	ft								
Minimum Filling Height (use 0 if unknown)	HLN	1.00	ft	Average Daily Vapor Temperature Range (ΔTv)				Average Daily Vapor Temperature Range (ΔTv)			
Liquid height (assume 1/2 H)	HL	3.93	ft	Average daily ambient temperature range - Equation 1-11 ($\Delta TA = TAX - TAA$)	ΔTA	13.5	°R	Average daily ambient temperature range - Equation 1-11 ($\Delta TA = TAX - TAA$)	ΔTA	13.5	°R
Tank insulation (pick from drop down list)		Not Insulated		Not Insulated - Equation 1-7 ($\Delta Tv = 0.7 \Delta TA + 0.92 \alpha I$)	ΔTv	12.56	°R	Not Insulated - Equation 1-7 ($\Delta Tv = 0.7 \Delta TA + 0.92 \alpha I$)	ΔTv	12.56	°R
Tank Construction (pick from drop down list)		Welded		Partially Insulated - Equation 1-8 ($\Delta Tv = 0.6 \Delta TA + 0.02 \alpha R I$)	ΔTv	11.21	°R	Partially Insulated - Equation 1-8 ($\Delta Tv = 0.6 \Delta TA + 0.02 \alpha R I$)	ΔTv	11.21	°R
Tank Shell Color (pick from drop down list)		White		Fully Insulated, constant temperature	ΔTv	0.00	°R	Fully Insulated, constant temperature	ΔTv	0.00	°R
Tank Shell Condition (pick from drop down list)		Average									
Tank Interior Condition (pick from drop down list)		Light Rust		Average Daily Vapor Pressure Range (ΔPv)				Average Daily Vapor Pressure Range (ΔPv)			
Tank paint solar absorptance, dimensionless; Table 7.1-6	α	0.25		Not Insulated - Equation 1-9: $\Delta Pv = PVX - PVN$	ΔPv	0.00000	psia	Not Insulated - Equation 1-9: $\Delta Pv = PVX - PVN$	ΔPv	0.00000	psia
Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	0.03	psi	Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25: $PvX = \alpha PVA$)	PvX	1.00000	psia	Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25: $PvX = \alpha PVA$)	PvX	1.00000	psia
		-0.03		Vapor pressure at ave. daily min liquid surface temp. (Eq. 1-25: $PvN = \alpha PVA$)	PvN	1.00000	psia	Vapor pressure at ave. daily min liquid surface temp. (Eq. 1-25: $PvN = \alpha PVA$)	PvN	1.00000	psia
True Vapor Pressure: Eq. 1-25: $PvA = \exp(A - (B/TLA))$											
Not Insulated	PvA	0.0580534		Average daily max. liquid surface temp.; Fig. 7.1-17: $TLX = TLA + 0.25 \Delta T$	TLX	509.54	°R	Average daily max. liquid surface temp.; Fig. 7.1-17: $TLX = TLA + 0.25 \Delta T$	TLX	509.54	°R
Partially Insulated	PvA	0.0581547		Average daily min. liquid surface temp.; Fig. 7.1-17: $TLN = TLA - 0.25 \Delta T$	TLN	503.27	°R	Average daily min. liquid surface temp.; Fig. 7.1-17: $TLN = TLA - 0.25 \Delta T$	TLN	503.27	°R
Fully Insulated	PvA	0.0567834		Partially Insulated - Equation 1-9: $\Delta Pv = PVX - PVN$	ΔPv	0.00000	psia	Partially Insulated - Equation 1-9: $\Delta Pv = PVX - PVN$	ΔPv	0.00000	psia
				Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25: PvX)	PvX	1.00000	psia	Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25: PvX)	PvX	1.00000	psia
				Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25: PvN)	PvN	1.000000	psia	Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25: PvN)	PvN	1.000000	psia
Average Daily Ambient Temperature (TAA) Eq. 1-30: $TAA = ((TAX + TAN) / 2) + 0.003 \alpha I$											
Average daily maximum ambient temperature; Table 7.1-7	TAX	512.10	°R	Average daily maximum liquid surface temperature, deg R ($TLX = TLA + TLX$)	TLX	509.25	°R	Average daily maximum liquid surface temperature, deg R ($TLX = TLA + TLX$)	TLX	509.25	°R
Average daily minimum ambient temperature; Table 7.1-7	TAN	498.60	°R	Average daily minimum liquid surface temperature, deg R ($TLN = TLA - TLN$)	TLN	503.65	°R	Average daily minimum liquid surface temperature, deg R ($TLN = TLA - TLN$)	TLN	503.65	°R
Liquid Bulk Temperature; Eq. 1-31: $TB = TAA + 0.003 \alpha I$											
	TB	505.82	°R	Fully Insulated ($\Delta Pv = 0$)	ΔPv	0.00	psia	Fully Insulated ($\Delta Pv = 0$)	ΔPv	0.00	psia
Average Daily Liquid Surface Temperature (TLA)											
Not Insulated; Eq. 1-28: $TLA = 0.4 \cdot TAA + 0.6 \cdot TB + 0.005 \cdot \alpha I$	TLA	506.41	°R	Vapor Space Volume (Eq. 1-3: $Vv = ((Pi/4) \cdot D^2 \cdot Hvo)$)	Vv	549.78	ft ³	Vapor Space Volume (Eq. 1-3: $Vv = ((Pi/4) \cdot D^2 \cdot Hvo)$)	Vv	549.78	ft ³
Partially Insulated; Eq. 1-29: $TLA = 0.3 \cdot TAA + 0.7 \cdot TB + 0.005 \cdot \alpha R I$	TLA	506.45	°R	Effective Tank diameter	Dt	13.35	ft	Effective Tank diameter	Dt	13.35	ft
Fully Insulated: $TLA = TB$	TLA	505.8	°R	Effective Tank Height	Ht	7.85	ft	Effective Tank Height	Ht	7.85	ft
				Vapor Space Outage $Hvo = 1/2 H$	Hvo	3.93	ft	Vapor Space Outage $Hvo = 1/2 H$	Hvo	3.93	ft
Average Vapor Temperature (Tv)											
Not Insulated; Eq. 1-33: $Tv = 0.7 \cdot TAA + 0.3 \cdot TB + 0.009 \cdot \alpha I$	Tv	506.89	°R								
Partially Insulated; Eq. 1-34: $Tv = 0.6 \cdot TAA + 0.4 \cdot TB + 0.01 \cdot \alpha R I$	Tv	507.09	°R								
Fully Insulated; $Tv = TB$	Tv	505.82	°R								
Stock Vapor Density: Eq. 1-22: $Wv = (Mv \cdot PVA) / (R \cdot Tv)$											
Not Insulated	Wv	1.387E-03									
Partially Insulated	Wv	1.389E-03									
Fully Insulated	Wv	1.360E-03									

HAPS Speciation		lb/month	
Product			additive
Total HAP Emissions =	1.660	Vapor Weight Concentration	
Eq. 40-2: $L_1 = \sum (L_i)$		Eq. 40-6: $Zv_i = y_i M_i / MV$	Eq. 40-5: $y_i = P_i / PVA$
Individual HAPS	L_{i1} (lb/month)	M_i	M_v
hexane	0.0000	86.18	130
benzene	0.0000	78.11	130
2,2,4 TMP	0.0000	114.23	130
toluene	0.0000	92.14	130
ethylbenzene	0.4856	106.17	130
xylenes	1.1748	106.17	130
naphthalene	0.0000	128.17	130
cumene	0.0000	120.19	130

Liquid Mole Fraction		Component Vapor Pressure	
Eq. 40-4: $x_i = (Z_{i1} M_i) / M_v$		Eq. 40-3: $PVA_i = (0.019377)^{10 \cdot (A_i - B_i) / (TLA - C_i)}$	
Individual HAPS	Z_{i1}	M_i	M_v
hexane	0.00000	130	86.18
benzene	0.00000	130	78.11
2,2,4 TMP	0.00000	130	114.23
toluene	0.00000	130	92.14
ethylbenzene	0.26400	130	106.17
xylenes	0.73600	130	106.17
naphthalene	0.00000	130	128.17
cumene	0.00000	130	120.19

Monthly Calculations (continued)

DECEMBER

Tank No.	10454A		UNITS		ROUTINE EMISSIONS CALCULATIONS		Symbol		UNITS		
ROUTINE EMISSIONS CALCULATIONS											
Total Losses (Eq. 1-1: $LT = LS + LW$)	LT	1.13	lb/month	Standing Losses: Eq. 1-2: $LS = 365 (Vv \cdot Wv \cdot KE \cdot Ks)$	LS	0.31	lb/month	Vapor Space Volume	Vv	549.8	ft ³
		5.65E-04	ton/month	Stock Vapor Density	Wv	0.0010	lb/ft ³	Stock Vapor Density	Wv	0.0010	lb/ft ³
	Time Period	December		Vapor Space Expansion Factor ($0 < KE \leq 1$): Eq. 1-5	KE	0.019	per day	Vapor Space Expansion Factor ($0 < KE \leq 1$): Eq. 1-5	KE	0.019	per day
	Nearest US Location	Bridgeport, CT		Vented Vapor Saturation Factor	Ks	1.00	NA	Vented Vapor Saturation Factor	Ks	1.00	NA
	Daily total solar insolation on a horizontal surface; Table 7.1-7	I	501.0	Constant: Number of Daily Events in a Year	365	31	days/month	Constant: Number of Daily Events in a Year	365	31	days/month
	Absolute Pressure	Pa	14.69	Working Losses: Eq. 1-3: $Lw = VQ \cdot KN \cdot Kp \cdot Wv \cdot KB$	Lw	0.82	lb/month	Working Losses: Eq. 1-3: $Lw = VQ \cdot KN \cdot Kp \cdot Wv \cdot KB$	Lw	0.82	lb/month
	Ideal Gas Constant	R	10.73	Net Working Loss Throughput (Eq. 1-39: $VQ = 5.614 \cdot Q$)	VQ	855	ft ³ /month	Net Working Loss Throughput (Eq. 1-39: $VQ = 5.614 \cdot Q$)	VQ	855	ft ³ /month
Product Information											
Product Type	Diesel Additive			Working Loss Turnover Factor Eq. 1-35: $Ks = (180 + N)/N$ for $N > 36$, else $Ks = KN$	KN	1.0000		Working Loss Turnover Factor Eq. 1-35: $Ks = (180 + N)/N$ for $N > 36$, else $Ks = KN$	KN	1.0000	
Vapor Molecular weight	Mv	130	lb/lb-mole	Working Loss Product Factor	Kp	1.00		Working Loss Product Factor	Kp	1.00	
Average organic liquid density	WL	6.10	lb/gal	Stock Vapor Density	Wv	0.0010	lb/ft ³	Stock Vapor Density	Wv	0.0010	lb/ft ³
Average Reid Vapor Pressure	RVP	0.00		Vent Setting Correction Factor	KB	1.00		Vent Setting Correction Factor	KB	1.00	
Product factor: 0.4 for crude oils or 1 for other organic liquids	Kc	1.00		Vented Vapor Saturation Factor: Eq. 1-21: $Ks = 1/(1 + 0.053 \cdot PVA \cdot Hvo)$	Ks	1.00		Vented Vapor Saturation Factor: Eq. 1-21: $Ks = 1/(1 + 0.053 \cdot PVA \cdot Hvo)$	Ks	1.00	
Vapor Pressure Equation Constant A	A	0.0		Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.0395	psia	Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.0395	psia
Vapor Pressure Equation Constant B (Table 7.1-2)	B	0.0		Vapor Space Outage	Hvo	0.00	ft	Vapor Space Outage	Hvo	0.00	ft
Tank design data											
Shell height	Hs	7.85	ft	Vapor Space Expansion Factor (Eq. 1-5: $(\Delta Tv/TLA) + ((\Delta Pv - \Delta Pb)/(PA - PVA))$)	KE	0.0187	per day	Vapor Space Expansion Factor (Eq. 1-5: $(\Delta Tv/TLA) + ((\Delta Pv - \Delta Pb)/(PA - PVA))$)	KE	0.0187	per day
Diameter	D	13.35	ft	Average Daily Vapor Temperature Range	ΔTv	11.33	°R	Average Daily Vapor Temperature Range	ΔTv	11.33	°R
Throughput	Q	6.400	gal/month	Average Daily Vapor Pressure Range	ΔPv	0.0000	psia	Average Daily Vapor Pressure Range	ΔPv	0.0000	psia
Turnovers	N	9.16	per year	Breather Vent Pressure Setting Range (Equation 1-10: $\Delta Pb = PBP - PBV$)	ΔPb	0.0600	psi	Breather Vent Pressure Setting Range (Equation 1-10: $\Delta Pb = PBP - PBV$)	ΔPb	0.0600	psi
Roof Type:		0.00		Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.0395	psia	Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.0395	psia
Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft	Average Daily Liquid Surface Temperature	TLA	496.35	°R	Average Daily Liquid Surface Temperature	TLA	496.35	°R
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA	ft	Atmospheric Pressure	PA	14.69	psia	Atmospheric Pressure	PA	14.69	psia
Maximum Filling Height - use (Pi/4)D if unknown	HLX	6.85	ft								
Minimum Filling Height (use 0 if unknown)	HLN	1.00	ft	Average Daily Vapor Temperature Range (ΔTv)				Average Daily Vapor Temperature Range (ΔTv)			
Liquid height (assume 1/2 H)	HL	3.93	ft	Average daily ambient							

Monthly Calculations - JANUARY

Tank No.	10455A			FEBRUARY			ROUTINE EMISSIONS CALCULATIONS			Symbol			Units			HAPS Speciation			lb/month		
	ROUTINE EMISSIONS CALCULATIONS			Symbol	Units	ROUTINE EMISSIONS CALCULATIONS			Symbol	Units	HAPS Speciation			lb/month							
	Standing Losses; Eq. 1-2, $L_s = 365 (V_v \cdot W \cdot K_e \cdot K_s)$			LS	0.27	lb/month	Product			Product			Product			Product					
Total Losses (Eq. 1-1: $L_T = L_s + L_W$)	LT	0.95	lb/month	Vapor Space Volume	Vv	549.8	ft ³	Total HAP Emissions =	0.954			Vapor Weight Concentration			Vapor Mole Fraction						
Daily total solar insolation on a horizontal surface; Table 7.1-7	I	563.0	Btu/ft ² -day	Stock Vapor Density	Wv	0.0008	lb/ft ³	Eq. 40-2 $Z_{vi} = Z_{vi}(L_i)$	Eq. 40-6 $Z_{vi} = y_i M_i / M_v$			Eq. 40-5 $y_i = P_i / P_{VA}$									
Nearest US Location	Bridgeport, CT			Vapor Space Expansion Factor ($0 < K_e \leq 1$); Eq. 1-5	KE	0.020	per day	Individual HAPS	L _{ij} (lb/month)			M _i			M _v						
Absolute Pressure	P _a	14.69	psi	Vented Vapor Saturation Factor	Ks	1.00	NA	hexane	0.0000	86.18	130	0.00000	0.00000	0.032	-	-					
Ideal Gas Constant	R	10.73	psia ft ³ /lb-mole R	Constant; Number of Daily Events in a Year	365	31	days/month	benzene	0.0000	114.23	130	0.00000	0.00000	0.032	-	-					
Product Information	Diesel Additive			Working Losses; Eq. 1-35, $L_w = VQ \cdot KN \cdot K_p \cdot W \cdot KB$	LW	0.68	lb/month	2,2,4 TMP	0.0000	92.14	130	0.00000	0.00000	0.032	-	-					
Product Type	Diesel Additive			Net Working Loss Throughput (Eq. 1-39: $VQ = 5.614 \cdot Q$)	VQ	855	ft ³ /month	ethylbenzene	0.2798	106.17	130	0.29329	0.01655	0.032	0.35912						
Vapor Molecular weight	Mv	130	lb/lb-mole	Working Loss Turnover Factor Eq. 1-35 $K_p = (180+N)/6N$ for N>36, else $K_p = KN$	KN	1.0000		xylene	0.6742	106.17	130	0.70671	0.02804	0.032	0.86533						
Average organic liquid density	WL	6.10	lb/gal	Working Loss Product Factor	Kp	1.00		naphthalene	0.0000	128.17	130	0.00E+00	0.00E+00	0.032	0.00E+00						
Average Reid Vapor Pressure	RVP	0.00	psi	Stock Vapor Density	Wv	0.0008	lb/ft ³	cumene	0.0000	120.19	130	0.00E+00	0.00E+00	0.032	0.00E+00						
Product factor; 0.4 for crude oils or 1 for other organic liquids	Kc	1.00		Vent Setting Correction Factor	KB	1.00		Liquid Mole Fraction			Component Vapor Pressure			PVAi = (0.019337)10 ³ (PA-B)/(TLA-C)							
Vapor Pressure Equation Constant A	A	0.00		Vented Vapor Saturation Factor; Eq. 1-21, $K_s = 1/(1+0.053 \cdot P_{VA} \cdot H_v)$	Ks	1.00		Eq. 40-4 $x_i = (Z_i M_i) / M_i$	Z _i	M _i	M _v	X _i	A	B	C	P _{vui}					
Vapor Pressure Equation Constant B (Table 7.1-2)	B	0.0	°R	Vapor Pressure at Avg Daily Liq Surface Temp	P _{VA}	0.0325	psia	hexane	0.00000	130	86.18	0.00000	6.878	1171.5	224.37	0.8715					
				Vapor Space Outage	H _{vo}	0.00	ft	benzene	0.00000	130	78.11	0.00000	6.906	1211	220.79	0.5064					
Tank design data				Vapor Space Expansion Factor (Eq. 1-5: $(\Delta T_v / TLA) \cdot [(P_{VA} - P_{VB}) / (P_{VA} - P_{VA})]$)	KE	0.0198	per day	2,2,4 TMP	0.00000	130	114.23	0.00000	6.812	1257.8	220.74	0.2495					
Shell height	Hs	7.85	ft	Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	toluene	0.00000	130	92.14	0.00000	7.017	1377.6	222.64	0.1296					
Diameter	D	13.35	ft	Not Insulated - Equation 1-7 ($\Delta T_v = 0.7 \Delta T_A + 0.02 \sigma I$)	ΔT _v	12.8	°R	ethylbenzene	0.26400	130	106.17	0.32326	6.95	1419.3	212.61	0.0361					
Throughput	Q	6.400	gal/month	Partially Insulated - Equation 1-8 ($\Delta T_v = 0.6 \Delta T_A + 0.02 \sigma R I$)	ΔT _v	10.48	°R	xylene	0.73600	130	106.17	0.90120	7.009	1462.3	215.11	0.0312					
Turnovers	N	9.16	per year	Fully Insulated, constant temperature	ΔT _v	0.00	°R	naphthalene	0.00000	130	128.17	0.00000	7.146	1831.6	211.82	0.0006					
Roof Type:								cumene	0.00000	130	120.19	0.00000	6.929	1455.8	207.2	0.0153					
Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft	Average Daily Vapor Pressure Range (ΔP _v)	ΔP _v	0.00000	psia	Eq. 40-4 $x_i = (Z_i M_i) / M_i$			Component Vapor Pressure			PVAi = (0.019337)10 ³ (PA-B)/(TLA-C)							
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA	ft	Not Insulated - Equation 1-9: $\Delta P_v = P_{VX} - P_{VN}$	ΔP _v	0.00000	psia	hexane	0.00000	130	86.18	0.00000	6.878	1171.5	224.37	0.8715					
Maximum Filling Height - use (Pi/4)D if unknown	HLX	6.85	ft	Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25 $P_{VX} = \exp(P_{VA} / (R \cdot T_{LX}))$)	P _{VX}	1.00000	psia	benzene	0.00000	130	78.11	0.00000	6.906	1211	220.79	0.5064					
Minimum Filling Height (use 0 if unknown)	HLN	1.00	ft	Vapor pressure at ave. daily min liquid surface temp. (Eq. 1-25 $P_{VN} = \exp(P_{VA} / (R \cdot T_{LN}))$)	P _{VN}	1.00000	psia	2,2,4 TMP	0.00000	130	114.23	0.00000	6.812	1257.8	220.74	0.2495					
Liquid height (assume 1/2 H)	HL	3.93	ft	Average daily max. liquid surface temp.; Fig. 7.1-17 $T_{LX} = TLA + 0.25 \Delta T_v$	T _{LX}	494.39	°R	toluene	0.00000	130	92.14	0.00000	7.017	1377.6	222.64	0.1400					
Tank Insulation (pick from drop down list)				Average daily min. liquid surface temp.; Fig. 7.1-17 $T_{LN} = TLA - 0.25 \Delta T_v$	T _{LN}	488.87	°R	ethylbenzene	0.26400	130	106.17	0.32326	6.95	1419.3	212.61	0.0361					
Tank Construction (pick from drop down list)								xylene	0.73600	130	106.17	0.90120	7.009	1462.3	215.11	0.0312					
Tank Shell Color (pick from drop down list)								naphthalene	0.00000	130	128.17	0.00000	7.146	1831.6	211.82	0.0007					
Tank Shell Condition (pick from drop down list)								cumene	0.00000	130	120.19	0.00000	6.929	1455.8	207.2	0.0153					
Tank Interior Condition (pick from drop down list)								Liquid Mole Fraction			Component Vapor Pressure			PVAi = (0.019337)10 ³ (PA-B)/(TLA-C)							
Tank paint solar absorptance, dimensionless; Table 7.1-6	σ	0.25		Average Daily Vapor Pressure Range (ΔP _v)	ΔP _v	0.00000	psia	Eq. 40-4 $x_i = (Z_i M_i) / M_i$	Z _i	M _i	M _v	X _i	A	B	C	P _{vui}					
Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	0.03	psi	Not Insulated - Equation 1-9: $\Delta P_v = P_{VX} - P_{VN}$	ΔP _v	0.00000	psia	hexane	0.00000	130	86.18	0.00000	6.878	1171.5	224.37	0.8715					
True Vapor Pressure; Eq. 1-25, $P_{VA} = \exp(A - (B/TLA))$				Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25 $P_{VX} = \exp(P_{VA} / (R \cdot T_{LX}))$)	P _{VX}	1.00000	psia	benzene	0.00000	130	78.11	0.00000	6.906	1211	220.79	0.5064					
Not Insulated	P _{VA}	0.032455		Vapor pressure at ave. daily min liquid surface temp. (Eq. 1-25 $P_{VN} = \exp(P_{VA} / (R \cdot T_{LN}))$)	P _{VN}	1.00000	psia	2,2,4 TMP	0.00000	130	114.23	0.00000	6.812	1257.8	220.74	0.2495					
Partially Insulated	P _{VA}	0.0325101						toluene	0.00000	130	92.14	0.00000	7.017	1377.6	222.64	0.1400					
Fully Insulated	P _{VA}	0.031764						ethylbenzene	0.26400	130	106.17	0.32326	6.95	1419.3	212.61	0.0361					
Average Daily Ambient Temperature (TAA) Eq. 1-30 $TAA = ((TAX + TAN) / 2)$	TAA	490.50	°R	Partially Insulated - Equation 1-9: $\Delta P_v = P_{VX} - P_{VN}$	ΔP _v	0.00000	psia	xylene	0.73600	130	106.17	0.90120	7.009	1462.3	215.11	0.0312					
Average daily maximum ambient temperature; Table 7.1-7	TAX	496.90	°R	Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25 $P_{VX} = \exp(P_{VA} / (R \cdot T_{LX}))$)	P _{VX}	1.00000	psia	naphthalene	0.00000	130	128.17	0.00000	7.146	1831.6	211.82	0.0007					
Average daily maximum ambient temperature; Table 7.1-7	TAN	484.10	°R	Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25 $P_{VN} = \exp(P_{VA} / (R \cdot T_{LN}))$)	P _{VN}	1.00000	psia	cumene	0.00000	130	120.19	0.00000	6.929	1455.8	207.2	0.0153					
Average daily minimum ambient temperature; Table 7.1-7	TAN	484.10	°R					Liquid Mole Fraction			Component Vapor Pressure			PVAi = (0.019337)10 ³ (PA-B)/(TLA-C)							
Liquid Bulk Temperature; Eq. 1-31: $T_B = TAA + 0.003 \sigma I$	TB	490.92	°R	Fully Insulated (ΔP _v = 0)	ΔP _v	0.00	psia	Eq. 40-4 $x_i = (Z_i M_i) / M_i$	Z _i	M _i	M _v	X _i	A	B	C	P _{vui}					
Average Daily Liquid Surface Temperature (TLA)								hexane	0.00000	130	86.18	0.00000	6.878	1171.5	224.37	0.8715					
Not Insulated; Eq. 1-28, $TLA = 0.4 \cdot TAA + 0.6 \cdot TB + 0.005 \cdot \sigma I$	TLA	491.45	°R	Vapor Space Volume (Eq. 1-3: $V_v = ((PI / 4) \cdot D^2 \cdot H_v)$)	Vv	549.78	ft ³	benzene	0.00000	130	78.11	0.00000	6.906	1211	220.79	0.5064					
Partially Insulated; Eq. 1-29, $TLA = 0.3 \cdot TAA + 0.7 \cdot TB + 0.005 \cdot \sigma R I$	TLA	491.49	°R	Effective Tank diameter	D _e	13.35	ft	2,2,4 TMP	0.00000	130	114.23	0.00000	6.812	1257.8	220.74	0.2495					
Fully Insulated; TLA = TB	TLA	490.9	°R	Effective Tank Height	H _e	7.85	ft	toluene	0.00000	130	92.14	0.00000	7.017	1377.6	222.64	0.1400					
				Vapor Space Outage $H_{vo} = 1/2 H$	H _{vo}	3.93	ft	ethylbenzene	0.26400	130	106.17	0.32326	6.95	1419.3	212.61	0.0361					
Average Vapor Temperature (Tv)								xylene	0.73600	130	106.17	0.90120	7.009	1462.3	215.11	0.0312					
Not Insulated; Eq. 1-33, $T_v = 0.7 \cdot TAA + 0.3 \cdot TB + 0.009 \cdot \sigma I$	Tv	491.89	°R					naphthalene	0.00000	130	128.17	0.00000	7.146	1831.6	211.82	0.0007					
Partially Insulated; Eq. 1-34, $T_v = 0.6 \cdot TAA + 0.4 \cdot TB + 0.01 \cdot \sigma R I$	Tv	492.07	°R					cumene	0.00000	130	120.19	0.00000	6.929	1455.8	207.2	0.0153					
Fully Insulated; Tv = TB	Tv	490.92	°R					Liquid Mole Fraction			Component Vapor Pressure			PVAi = (0.019337)10 ³ (PA-B)/(TLA-C)							
Stock Vapor Density; Eq. 1-22, $W_v = (M_v \cdot P_{VA}) / (R \cdot T_v)$								Eq. 40-4 $x_i = (Z_i M_i) / M_i$	Z _i	M _i	M _v	X _i	A	B	C	P _{vui}					
Not Insulated	Wv	7.993E-04						hexane	0.00000	130	86.18	0.00000	6.878	1171.5	224.37	0.8715					
Partially Insulated	Wv	8.004E-04						benzene	0.00000	130	78.11	0.00000	6.906	1211	220.79	0.5064					
Fully Insulated	Wv	7.838E-04						2,2,4 TMP	0.00000	130	114.23	0.00000	6.812	1257.8	220.74	0.2495					

Monthly Calculations (continued)

Tank No.	10455A			FEBRUARY			ROUTINE EMISSIONS CALCULATIONS			Symbol			Units			HAPS Speciation			lb/month		
	ROUTINE EMISSIONS CALCULATIONS			Symbol	Units	ROUTINE EMISSIONS CALCULATIONS			Symbol	Units	HAPS Speciation			lb/month							
	Standing Losses; Eq. 1-2, $L_s = 365 (V_v \cdot W \cdot K_e \cdot K_s)$			LS	0.31	lb/month	Product			Product			Product			Product					
Total Losses (Eq. 1-1: $L_T = L_s + L_W$)	LT	1.05	lb/month	Vapor Space Volume	Vv	549.8	ft ³	Total HAP Emissions =	1.053			Vapor Weight Concentration			Vapor Mole Fraction						
Daily total solar insolation on a horizontal surface; Table 7.1-7	I	527.04	Btu/ft ² -day	Stock Vapor Density	Wv	0.0009	lb/ft ³	Eq. 40-2 $Z_{vi} = Z_{vi}(L_i)$	Eq. 40-6 $Z_{vi} = y_i M_i / M_v$			Eq. 40-5 $y_i = P_i / P_{VA}$									
Nearest US Location	Bridgeport, CT			Vapor Space Expansion Factor ($0 < K_e \leq 1$); Eq. 1-5	KE	0.023	per day	Individual HAPS	L _{ij} (lb/month)			M _i			M _v						
Absolute Pressure	P _a	14.69	psi	Vented Vapor Saturation Factor	Ks	1.00	NA	hexane	0.0000	86.18	130	0.00000	0.00000	0.035	-	-					
Ideal Gas Constant	R	10.73	psia ft ³ /lb-mole R	Constant; Number of Daily Events in a Year	365	28	days/month	benzene	0.0000	114.23	130	0.00000	0.00000	0.035	-	-					
Product Information	Diesel Additive			Working Losses; Eq. 1-35, $L_w = VQ \cdot KN \cdot K_p \cdot W \cdot KB$	LW	0.74	lb/month	2,2,4 TMP	0.0000	92.14	130	0.00000	0.00000	0.035	-	-					
Product Type	Diesel Additive			Net Working Loss Throughput (Eq. 1-39: $VQ = 5.614 \cdot Q$)	VQ	855	ft ³ /month	ethylbenzene	0.3088	106.17	130	0.29318									

Monthly Calculations (continued)

MARCH

Tank No.	10455A	Symbol	Units	ROUTINE EMISSIONS CALCULATIONS	Symbol	Units
ROUTINE EMISSIONS CALCULATIONS						
Total Losses (Eq. 1-1: $LT = LS + LW$)	LT	1.50	lb/month	Standing Losses; Eq. 1-2, $LS = 365 (Vv \cdot Wv \cdot Ke \cdot Ks)$	LS	0.53 lb/month
Nearest US Location	Bridgeport, CT			Vapor Space Volume	Vv	549.8 ft ³
Daily total solar insolation on a horizontal surface; Table 7.1-7	I	1156.0	Btu/ft ² -day	Stock Vapor Density	Wv	0.0011 lb/ft ³
Absolute Pressure	Pa	14.69	psi	Vapor Space Expansion Factor ($0 < Ke \leq 1$); Eq. 1-5	Ke	0.027 per day
Ideal Gas Constant	R	10.73	psi ft ³ /lb-mole R	Vented Vapor Saturation Factor	Ks	1.00 NA
Product Information						
Product Type	Diesel Additive			Constant; Number of Daily Events in a Year	365	31 days/month
Vapor Molecular weight	Mv	130	lb/lb-mole	Working Losses; Eq. 1-35, $Lw = VQ \cdot KN \cdot Kp \cdot Wv \cdot Kb$	Lw	0.97 lb/month
Average organic liquid density	WL	6.10	lb/gal	Net Working Loss Throughput (Eq. 1-39: $VO = 5.614 \cdot Q$)	VQ	855 ft ³ /month
Average Reid Vapor Pressure	RVP	0.00	psi	Working Loss Turnover Factor Eq. 1-35 $Kp = (180 + N)/N$ for $N \geq 36$, else $Kp = KN$	KN	1.0000
Product factor; 0.4 for crude oils or 1 for other organic liquids	Kc	1.00		Working Loss Product Factor	Kp	1.00
Vapor Pressure Equation Constant A	A	0.00		Stock Vapor Density	Wv	0.0011 lb/ft ³
Vapor Pressure Equation Constant B (Table 7.1-2)	B	0.0	R	Vent Setting Correction Factor	KB	1.00
Tank design data						
Shell height	Hs	7.85	ft	Vented Vapor Saturation Factor; Eq. 1-21, $Ks = 1/(1+0.053 \cdot PVA \cdot Hvo)$	Ks	1.00
Diameter	D	13.35	ft	Vapor Space Expansion Factor (Eq. 1-5: $(\Delta T v / TLA) \cdot ((\Delta P v - \Delta P B) / (P v - P v A))$)	KE	0.0273 per day
Throughput	Q	6,400	gal/month	Average Daily Vapor Temperature Range	$\Delta T v$	15.72 R
Turnovers	N	9.16	per year	Average Daily Vapor Pressure Range	$\Delta P v$	0.0000 psia
Roof Type:	0.00			Breather Vent Pressure Setting Range (Equation 1-10: $\Delta P B = P B P - P B V$)	$\Delta P B$	0.0600 psi
Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft	Vapor Pressure at Avg Daily Liq Surface Temp	PvA	0.0470 psia
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA	ft	Average Daily Liquid Surface Temperature	TLA	500.87 R
Maximum Filling Height - use (Pi/4)D if unknown	HLX	6.85	ft	Atmospheric Pressure	Pa	14.69 psia
Minimum Filling Height (use 0 if unknown)	HLN	1.00	ft	Average Daily Vapor Temperature Range ($\Delta T v$)		
Liquid height (assume 1/2 H)	HL	3.93	ft	Not Insulated - Equation 1-7 ($\Delta T v = 0.7 \Delta T A + 0.02 \sigma I$)	$\Delta T A$	14.2 R
Tank insulation (pick from drop down list)	Not Insulated			Partially Insulated - Equation 1-8 ($\Delta T v = 0.6 \Delta T A + 0.02 \sigma R I$)	$\Delta T v$	15.72 R
Tank Construction (pick from drop down list)	Welded			Fully Insulated, constant temperature	$\Delta T v$	0.00 R
Tank Shell Color (pick from drop down list)	White			Average Daily Vapor Pressure Range ($\Delta P v$)		
Tank Shell Condition (pick from drop down list)	Average			Not Insulated - Equation 1-9: $\Delta P v = P v X - P v N$	$\Delta P v$	0.00000 psia
Tank Interior Condition (pick from drop down list)	Light Rust			Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25 $P v X = \exp(P v N)$)	PvX	1.00000 psia
Tank paint solar absorptance, dimensionless; Table 7.1-6	α	0.25		Vapor pressure at ave daily min liquid surface temp. (Eq. 1-25 $P v N = \exp(P v N)$)	PvN	1.00000 psia
Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	-0.03	psi	Average daily max. liquid surface temp.; Fig. 7.1-17 $TLX = TLA + 0.25 \Delta T v$	TLX	504.80 R
True Vapor Pressure; Eq. 1-25, $P v A = \exp(A \cdot (B/TLA))$						
Not Insulated	PvA	0.047042	psi	Average daily min. liquid surface temp.; Fig. 7.1-17 $TLN = TLA - 0.25 \Delta T v$	TLN	496.94 R
Partially Insulated	PvA	0.0471992	psi	Partially Insulated - Equation 1-9: $\Delta P v = P v X - P v N$		
Fully Insulated	PvA	0.0450895	psi	Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25 $u P v X$)	PvX	1.00000 psia
Average Daily Ambient Temperature (TAA) Eq. 1-30 $TAA = ((TAX + TAN) / 2)$						
Not Insulated	TAA	498.90	R	Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25 $u P v N$)	PvN	1.000000 psia
Partially Insulated	TAX	506.00	R	Average daily maximum liquid surface temperature, deg R ($TLX = TLA + TLX$)	TLX	504.53 R
Fully Insulated	TAN	491.80	R	Average daily minimum liquid surface temperature, deg R ($TLN = TLA - TLN$)	TLN	497.38 R
Liquid Bulk Temperature; Eq. 1-31: $TB = TAA + 0.003 \sigma I$						
Not Insulated	TB	499.77	R	Fully Insulated ($\Delta P v = 0$)	$\Delta P v$	0.00 psia
Average Daily Liquid Surface Temperature (TLA)						
Not Insulated; Eq. 1-28, $TLA = 0.4 \cdot TAA + 0.6 \cdot TB + 0.005 \cdot \sigma I$	TLA	500.87	R	Vapor Space Volume (Eq. 1-3: $Vv = ((P/4) D^2 H)$)	Vv	549.78 ft ³
Partially Insulated; Eq. 1-29, $TLA = 0.3 \cdot TAA + 0.7 \cdot TB + 0.005 \cdot \sigma I$	TLA	500.95	R	Effective Tank diameter	D _e	13.35 ft
Fully Insulated; $TLA = TB$	TLA	499.8	R	Effective Tank Height	H _e	7.85 ft
Average Vapor Temperature (Tv)						
Not Insulated; Eq. 1-33, $Tv = 0.7 \cdot TAA + 0.3 \cdot TB + 0.009 \cdot \sigma I$	Tv	501.76	R	Vapor Space Outage Hvo = 1/2 H	Hvo	3.93 ft
Partially Insulated; Eq. 1-34, $Tv = 0.6 \cdot TAA + 0.4 \cdot TB + 0.01 \cdot \sigma I$	Tv	502.14	R	Average Vapor Pressure (Pv)		
Fully Insulated; $Tv = TB$	Tv	499.77	R	Not Insulated	Pv	0.00000 psia
Stock Vapor Density; Eq. 1-22, $Wv = (Mv \cdot PvA) / (R \cdot Tv)$						
Not Insulated	Wv	1.136E-03		Individual HAPS		
Partially Insulated	Wv	1.139E-03		Product		
Fully Insulated	Wv	1.093E-03		Total HAP Emissions = 2.288		

Product	lb/month	Vapor Weight Concentration	Vapor Mole Fraction
hexane	0.0000	86.18	0.00000
benzene	0.0000	78.11	0.00000
2,2,4 TMP	0.0000	114.23	0.00000
toluene	0.0000	92.14	0.00000
ethylbenzene	0.4391	106.17	0.29278
xylene	1.0607	106.17	0.70722
naphthalene	0.0000	128.17	0.00E+00
cumene	0.0000	120.19	0.00E+00

Monthly Calculations (continued)

APRIL

Tank No.	10455A	Symbol	Units	ROUTINE EMISSIONS CALCULATIONS	Symbol	Units
ROUTINE EMISSIONS CALCULATIONS						
Total Losses (Eq. 1-1: $LT = LS + LW$)	LT	2.29	lb/month	Standing Losses; Eq. 1-2, $LS = 365 (Vv \cdot Wv \cdot Ke \cdot Ks)$	LS	0.96 lb/month
Nearest US Location	Bridgeport, CT			Vapor Space Volume	Vv	549.8 ft ³
Daily total solar insolation on a horizontal surface; Table 7.1-7	I	1490.0	Btu/ft ² -day	Stock Vapor Density	Wv	0.0017 lb/ft ³
Absolute Pressure	Pa	14.69	psi	Vapor Space Expansion Factor ($0 < Ke \leq 1$); Eq. 1-5	Ke	0.031 per day
Ideal Gas Constant	R	10.73	psi ft ³ /lb-mole R	Vented Vapor Saturation Factor	Ks	1.00 NA
Product Information						
Product Type	Diesel Additive			Constant; Number of Daily Events in a Year	365	30 days/month
Vapor Molecular weight	Mv	130	lb/lb-mole	Working Losses; Eq. 1-35, $Lw = VQ \cdot KN \cdot Kp \cdot Wv \cdot Kb$	Lw	1.43 lb/month
Average organic liquid density	WL	6.10	lb/gal	Net Working Loss Throughput (Eq. 1-39: $VO = 5.614 \cdot Q$)	VQ	855 ft ³ /month
Average Reid Vapor Pressure	RVP	0.00	psi	Working Loss Turnover Factor Eq. 1-35 $Kp = (180 + N)/N$ for $N \geq 36$, else $Kp = KN$	KN	1.0000
Product factor; 0.4 for crude oils or 1 for other organic liquids	Kc	1.00		Working Loss Product Factor	Kp	1.00
Vapor Pressure Equation Constant A	A	0.00		Stock Vapor Density	Wv	0.0017 lb/ft ³
Vapor Pressure Equation Constant B (Table 7.1-2)	B	0.0	R	Vent Setting Correction Factor	KB	1.00
Tank design data						
Shell height	Hs	7.85	ft	Vented Vapor Saturation Factor; Eq. 1-21, $Ks = 1/(1+0.053 \cdot PVA \cdot Hvo)$	Ks	1.00
Diameter	D	13.35	ft	Vapor Space Expansion Factor (Eq. 1-5: $(\Delta T v / TLA) \cdot ((\Delta P v - \Delta P B) / (P v - P v A))$)	KE	0.0314 per day
Throughput	Q	6,400	gal/month	Average Daily Vapor Temperature Range	$\Delta T v$	18.16 R
Turnovers	N	9.47	per year	Average Daily Vapor Pressure Range	$\Delta P v$	0.0000 psia
Roof Type:	0.00			Breather Vent Pressure Setting Range (Equation 1-10: $\Delta P B = P B P - P B V$)	$\Delta P B$	0.0600 psi
Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft	Vapor Pressure at Avg Daily Liq Surface Temp	PvA	0.0706 psia
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA	ft	Average Daily Liquid Surface Temperature	TLA	511.68 R
Maximum Filling Height - use (Pi/4)D if unknown	HLX	6.85	ft	Atmospheric Pressure	Pa	14.69 psia
Minimum Filling Height (use 0 if unknown)	HLN	1.00	ft	Average Daily Vapor Temperature Range ($\Delta T v$)		
Liquid height (assume 1/2 H)	HL	3.93	ft	Not Insulated - Equation 1-7 ($\Delta T v = 0.7 \Delta T A + 0.02 \sigma I$)	$\Delta T A$	15.3 R
Tank insulation (pick from drop down list)	Not Insulated			Partially Insulated - Equation 1-8 ($\Delta T v = 0.6 \Delta T A + 0.02 \sigma R I$)	$\Delta T v$	18.16 R
Tank Construction (pick from drop down list)	Welded			Fully Insulated, constant temperature	$\Delta T v$	0.00 R
Tank Shell Color (pick from drop down list)	White			Average Daily Vapor Pressure Range ($\Delta P v$)		
Tank Shell Condition (pick from drop down list)	Average			Not Insulated - Equation 1-9: $\Delta P v = P v X - P v N$	$\Delta P v$	0.00000 psia
Tank Interior Condition (pick from drop down list)	Light Rust			Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25 $P v X = \exp(P v N)$)	PvX	1.00000 psia
Tank paint solar absorptance, dimensionless; Table 7.1-6	α	0.25		Vapor pressure at ave daily min liquid surface temp. (Eq. 1-25 $P v N = \exp(P v N)$)	PvN	1.00000 psia
Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	-0.03	psi	Average daily max. liquid surface temp.; Fig. 7.1-17 $TLX = TLA + 0.25 \Delta T v$	TLX	516.22 R
True Vapor Pressure; Eq. 1-25, $P v A = \exp(A \cdot (B/TLA))$						
Not Insulated	PvA	0.070523	psi	Average daily min. liquid surface temp.; Fig. 7.1-17 $TLN = TLA - 0.25 \Delta T v$	TLN	507.14 R
Partially Insulated	PvA	0.0708403	psi	Partially Insulated - Equation 1-9: $\Delta P v = P v X - P v N$		
Fully Insulated	PvA	0.0669906	psi	Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25 $u P v X$)	PvX	1.00000 psia
Average Daily Ambient Temperature (TAA) Eq. 1-30 $TAA = ((TAX + TAN) / 2)$						
Not Insulated	TAA	509.15	R	Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25 $u P v N$)	PvN	1.000000 psia
Partially Insulated	TAX	516.80	R	Average daily maximum liquid surface temperature, deg R ($TLX = TLA + TLX$)	TLX	515.95 R
Fully Insulated	TAN	501.50	R	Average daily minimum liquid surface temperature, deg R ($TLN = TLA - TLN$)	TLN	507.64 R
Liquid Bulk Temperature; Eq. 1-31: $TB = TAA + 0.003 \sigma I$						
Not Insulated	TB	510.27	R	Fully Insulated ($\Delta P v = 0$)	$\Delta P v$	0.00 psia
Average Daily Liquid Surface Temperature (TLA)						
Not Insulated; Eq. 1-28, $TLA = 0.4 \cdot TAA + 0.6 \cdot TB + 0.005 \cdot \sigma I$	TLA	511.68	R	Vapor Space Volume (Eq. 1-3: $Vv = ((P/4) D^2 H)$)	Vv	549.78 ft ³
Partially Insulated; Eq. 1-29, $TLA = 0.3 \cdot TAA + 0.7 \cdot TB + 0.005 \cdot \sigma I$	TLA	511.79	R	Effective Tank diameter	D _e	13.35 ft
Fully Insulated; $TLA = TB$	TLA	510.3	R	Effective Tank Height	H _e	7.85 ft
Average Vapor Temperature (Tv)						
Not Insulated; Eq. 1-33, $Tv = 0.7 \cdot TAA + 0.3 \cdot TB + 0.009 \cdot \sigma I$	Tv	512.84	R	Vapor Space Outage Hvo = 1/2 H	Hvo	3.93 ft
Partially Insulated; Eq. 1-34, $Tv = 0.6 \cdot TAA + 0.4 \cdot TB + 0.01 \cdot \sigma I$	Tv	513.32	R	Average Vapor Pressure (Pv)		
Fully Insulated; $Tv = TB$	Tv	510.27	R	Not Insulated	Pv	0.00000 psia
Stock Vapor Density; Eq. 1-22, $Wv = (Mv \cdot PvA) / (R \cdot Tv)$						
Not Insulated	Wv	1.667E-03		Individual HAPS		
Partially Insulated	Wv	1.672E-03		Product		
Fully Insulated	Wv	1.590E-03		Total HAP Emissions = 2.288		

Product	lb/month	Vapor Weight Concentration	Vapor Mole Fraction
hexane	0.0000	86.18	0.00000
benzene	0.0000	78.11	0.00000
2,2,4 TMP	0.0000	114.23	0.00000
toluene	0.0000	92.14	0.00000
ethylbenzene	0.6666	106.17	0.29216
xylene	1.6199	106.17	0.061148
naphthalene	0.0000	128.17	0.00E+00
cumene	0.0000	120.19	0.00E+00

Monthly Calculations (continued)

MAY

Tank No.	10455A	Symbol	Units	ROUTINE EMISSIONS CALCULATIONS	Symbol	Units
ROUTINE EMISSIONS CALCULATIONS						
Total Losses (Eq. 1-1: LT = LS+LW)	LT	3.33	lb/month	Standing Losses; Eq. 1-2, $LS = 365 (Vv \cdot Wv \cdot Ke \cdot Ks)$	LS	1.34 lb/month
		1.67E-03	ton/month	Vapor Space Volume	Vv	549.8 ft ³
				Stock Vapor Density	Wv	0.0023 lb/ft ³
				Vapor Space Expansion Factor ($0 < Ke \leq 1$); Eq. 1-5	Ke	0.034 per day
Nearest US Location		Bridgeport, CT		Vented Vapor Saturation Factor	Ks	1.00 NA
Daily total solar insolation on a horizontal surface; Table 7.1-7	I	1750.0	Btu/ft ² -day	Constant; Number of Daily Events in a Year	365	31 days/month
Absolute Pressure	Pa	14.69	psi	Working Losses; Eq. 1-35, $LW = VQ \cdot KN \cdot Kp \cdot Wv \cdot KB$	Lw	1.99 lb/month
Ideal Gas Constant	R	10.73	psi ft ³ /lb-mole R	Net Working Loss Throughput (Eq. 1-39: $VO=5.614 \cdot Q$)	VQ	855 ft ³ /month
Product Information						
Product Type		Diesel Additive		Working Loss Turnover Factor Eq. 1-35 $Kp=(180+N)/N$ for $N \geq 36$, else $Kp=KN$	Kp	1.0000
Vapor Molecular weight	Mv	130	lb/lb-mole	Working Loss Product Factor	Kp	1.00
Average organic liquid density	WL	6.10	lb/gal	Stock Vapor Density	Wv	0.0023 lb/ft ³
Average Reid Vapor Pressure	RVP	0.00	psi	Vent Setting Correction Factor	KB	1.00
Product factor; 0.4 for crude oils or 1 for other organic liquids	Kc	1.00		Vented Vapor Saturation Factor; Eq. 1-21, $Ks = 1/(1+0.053 \cdot PVA \cdot Hvo)$	Ks	1.00
Vapor Pressure Equation Constant A	A	0.00		Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.1005 psia
Vapor Pressure Equation Constant B (Table 7.1-2)	B	0.0		Vapor Space Outage	Hvo	0.00 ft
Tank design data						
Shell height	Hs	7.85	ft	Vapor Space Expansion Factor (Eq. 1-5: $(\Delta T v / TLA) \cdot ((\Delta P v - \Delta P B) / (P v - P v A))$)	KE	0.0337 per day
Diameter	D	13.35	ft	Average Daily Vapor Temperature Range	$\Delta T v$	19.74 °R
Throughput	Q	6.400	gal/month	Average Daily Vapor Pressure Range	$\Delta P v$	0.0000 psia
Turnovers	N	9.16	per year	Breather Vent Pressure Setting Range (Equation 1-10: $\Delta P B = P B P - P B V$)	$\Delta P B$	0.0600 psi
Roof Type:		0.00		Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.1005 psia
Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft	Average Daily Liquid Surface Temperature	TLA	521.63 °R
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA	ft	Atmospheric Pressure	Pa	14.69 psia
Maximum Filling Height -use (Pi/4)D if unknown	HLX	6.85	ft			
Minimum Filling Height (use 0 if unknown)	HLN	1.00	ft	Average Daily Vapor Temperature Range ($\Delta T v$)	$\Delta T v$	15.7 °R
Liquid height (assume 1/2 H)	HL	3.93	ft	Average daily ambient temperature range - Equation 1-11 ($\Delta T A = T A X - T A$)	$\Delta T A$	19.74 °R
Tank insulation (pick from drop down list)		Not Insulated		Partially Insulated - Equation 1-7 ($\Delta T v = 0.7 \Delta T A + 0.02 \sigma I$)	$\Delta T v$	18.17 °R
Tank Construction (pick from drop down list)		Welded		Fully Insulated - Equation 1-8 ($\Delta T v = 0.6 \Delta T A + 0.02 \sigma R I$)	$\Delta T v$	0.00 °R
Tank Shell Color (pick from drop down list)		White				
Tank Shell Condition (pick from drop down list)		Average				
Tank Interior Condition (pick from drop down list)		Light Rust		Average Daily Vapor Pressure Range ($\Delta P v$)	$\Delta P v$	0.00000 psia
Tank paint solar absorptance, dimensionless; Table 7.1-6	α	0.25		Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25 $P V X = \exp(P V N)$)	PvX	1.00000 psia
Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	-0.03	psi	Vapor pressure at ave daily min liquid surface temp. (Eq. 1-25 $P V N = \exp(P V N)$)	PvN	1.00000 psia
True Vapor Pressure; Eq. 1-25, $PvA = \exp(A \cdot (B/TLA))$						
Not Insulated	PvA	0.1005102		Average daily max. liquid surface temp.; Fig. 7.1-17 $TLX = TLA + 0.25 \Delta T v$	TLX	526.56 °R
Partially Insulated	PvA	0.1009694		Average daily min. liquid surface temp.; Fig. 7.1-17 $TLN = TLA - 0.25 \Delta T v$	TLN	516.69 °R
Fully Insulated	PvA	0.0948467		Partially Insulated - Equation 1-9: $\Delta P v = P v X - P v N$	$\Delta P v$	0.00000 psia
Average Daily Ambient Temperature (TAA) Eq. 1-30 $TAA = ((TAX+TAN)/2)$						
Average daily ambient temperature, Table 7.1-7	TAX	526.50	°R	Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25 $P V X$)	PvX	1.000000 psia
Average daily maximum ambient temperature, Table 7.1-7	TAN	510.80	°R	Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25 $P V N$)	PvN	1.000000 psia
Average daily minimum ambient temperature, Table 7.1-7	TAN	510.80	°R	Average daily maximum liquid surface temperature, deg R ($TLX = TLA + TLX$)	TLX	526.30 °R
				Average daily minimum liquid surface temperature, deg R ($TLN = TLA - TLN$)	TLN	517.21 °R
Liquid Bulk Temperature; Eq. 1-31: $TB = TAA + 0.003 \sigma I$						
	TB	519.96	°R	Fully Insulated ($\Delta P v = 0$)	$\Delta P v$	0.00 psia
Average Daily Liquid Surface Temperature (TLA)						
Not Insulated; Eq. 1-28, $TLA = 0.4 \cdot TAA + 0.6 \cdot TB + 0.005 \cdot \sigma I$	TLA	521.63	°R	Vapor Space Volume (Eq. 1-3: $Vv = ((P/4) \cdot D^2 \cdot Hvo)$)	Vv	549.78 ft ³
Partially Insulated; Eq. 1-29, $TLA = 0.3 \cdot TAA + 0.7 \cdot TB + 0.005 \cdot \sigma I$	TLA	521.76	°R	Effective Tank diameter	D _e	13.35 ft
Fully Insulated; $TLA = TB$	TLA	520.0	°R	Effective Tank Height	H _e	7.85 ft
				Vapor Space Outage $Hvo = 1/2 H$	Hvo	3.93 ft
Average Vapor Temperature (Tv)						
Not Insulated; Eq. 1-33, $Tv = 0.7 \cdot TAA + 0.3 \cdot TB + 0.009 \cdot \sigma I$	Tv	522.98	°R			
Partially Insulated; Eq. 1-34, $Tv = 0.6 \cdot TAA + 0.4 \cdot TB + 0.01 \cdot \sigma I$	Tv	523.55	°R			
Fully Insulated; $Tv = TB$	Tv	519.96	°R			
Stock Vapor Density; Eq. 1-22, $Wv = (Mv \cdot PvA) / (R \cdot Tv)$						
Not Insulated	Wv	2.328E-03				
Partially Insulated	Wv	2.336E-03				
Fully Insulated	Wv	2.210E-03				

HAPS Speciation	Product	lb/month	Vapor Weight Concentration	Vapor Mole Fraction
Total HAP Emissions =	3.330		Eq. 40-6 $Zvi = yiMi / MV$	Eq. 40-5 $yi = Pi / PVA$
Eq. 40-2 $L_i = Z_i(L_i)$				
Individual HAPS				
	L_i (lb/month)	M_i	M_v	Z_{vi}
hexane	0.0000	86.18	130	0.00000
benzene	0.0000	78.11	130	0.00000
2,2,4 TMP	0.0000	114.23	130	0.00000
toluene	0.0000	92.14	130	0.00000
ethylbenzene	0.9710	106.17	130	0.29159
xylene	2.3591	106.17	130	0.70841
naphthalene	0.0000	128.17	130	0.00E+00
cumene	0.0000	120.19	130	0.00E+00
Liquid Mole Fraction				
Eq. 40-4 $x_i = (Z_i \cdot M_i) / M_i$	Z_i	M_i	M_v	x_i
hexane	0.00000	130	86.18	0.00000
benzene	0.00000	130	78.11	0.00000
2,2,4 TMP	0.00000	130	114.23	0.00000
toluene	0.00000	130	92.14	0.00000
ethylbenzene	0.26400	130	106.17	0.32326
xylene	0.73600	130	106.17	0.90120
naphthalene	0.00000	130	128.17	0.00000
cumene	0.00000	130	120.19	0.00000
Component Vapor Pressure				
Eq. 40-5 $yi = Pi / PVA$	PVA	A	B	C
hexane	0.00000	130	86.18	0.00000
benzene	0.00000	130	78.11	0.00000
2,2,4 TMP	0.00000	130	114.23	0.00000
toluene	0.00000	130	92.14	0.00000
ethylbenzene	0.26400	130	106.17	0.32326
xylene	0.73600	130	106.17	0.90120
naphthalene	0.00000	130	128.17	0.00000
cumene	0.00000	130	120.19	0.00000

Monthly Calculations (continued)

JUNE

Tank No.	10455A	Symbol	Units	ROUTINE EMISSIONS CALCULATIONS	Symbol	Units
ROUTINE EMISSIONS CALCULATIONS						
Total Losses (Eq. 1-1: LT = LS+LW)	LT	4.52	lb/month	Standing Losses; Eq. 1-2, $LS = 365 (Vv \cdot Wv \cdot Ke \cdot Ks)$	LS	1.76 lb/month
		2.26E-03	ton/month	Vapor Space Volume	Vv	549.8 ft ³
				Stock Vapor Density	Wv	0.0032 lb/ft ³
				Vapor Space Expansion Factor ($0 < Ke \leq 1$); Eq. 1-5	Ke	0.033 per day
Nearest US Location		Bridgeport, CT		Vented Vapor Saturation Factor	Ks	1.00 NA
Daily total solar insolation on a horizontal surface; Table 7.1-7	I	1862.0	Btu/ft ² -day	Constant; Number of Daily Events in a Year	365	30 days/month
Absolute Pressure	Pa	14.69	psi	Working Losses; Eq. 1-35, $LW = VQ \cdot KN \cdot Kp \cdot Wv \cdot KB$	Lw	2.76 lb/month
Ideal Gas Constant	R	10.73	psi ft ³ /lb-mole R	Net Working Loss Throughput (Eq. 1-39: $VO=5.614 \cdot Q$)	VQ	855 ft ³ /month
Product Information						
Product Type		Diesel Additive		Working Loss Turnover Factor Eq. 1-35 $Kp=(180+N)/N$ for $N \geq 36$, else $Kp=KN$	Kp	1.0000
Vapor Molecular weight	Mv	130	lb/lb-mole	Working Loss Product Factor	Kp	1.00
Average organic liquid density	WL	6.10	lb/gal	Stock Vapor Density	Wv	0.0032 lb/ft ³
Average Reid Vapor Pressure	RVP	0.00	psi	Vent Setting Correction Factor	KB	1.00
Product factor; 0.4 for crude oils or 1 for other organic liquids	Kc	1.00		Vented Vapor Saturation Factor; Eq. 1-21, $Ks = 1/(1+0.053 \cdot PVA \cdot Hvo)$	Ks	1.00
Vapor Pressure Equation Constant A	A	0.00		Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.1418 psia
Vapor Pressure Equation Constant B (Table 7.1-2)	B	0.0		Vapor Space Outage	Hvo	0.00 ft
Tank design data						
Shell height	Hs	7.85	ft	Vapor Space Expansion Factor (Eq. 1-5: $(\Delta T v / TLA) \cdot ((\Delta P v - \Delta P B) / (P v - P v A))$)	KE	0.0331 per day
Diameter	D	13.35	ft	Average Daily Vapor Temperature Range	$\Delta T v$	19.81 °R
Throughput	Q	6.400	gal/month	Average Daily Vapor Pressure Range	$\Delta P v$	0.0000 psia
Turnovers	N	9.47	per year	Breather Vent Pressure Setting Range (Equation 1-10: $\Delta P B = P B P - P B V$)	$\Delta P B$	0.0600 psi
Roof Type:		0.00		Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.1418 psia
Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft	Average Daily Liquid Surface Temperature	TLA	531.77 °R
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA	ft	Atmospheric Pressure	Pa	14.69 psia
Maximum Filling Height -use (Pi/4)D if unknown	HLX	6.85	ft			
Minimum Filling Height (use 0 if unknown)	HLN	1.00	ft	Average Daily Vapor Temperature Range ($\Delta T v$)	$\Delta T v$	15.0 °R
Liquid height (assume 1/2 H)	HL	3.93	ft	Average daily ambient temperature range - Equation 1-11 ($\Delta T A = T A X - T A$)	$\Delta T A$	19.81 °R
Tank insulation (pick from drop down list)		Not Insulated		Partially Insulated - Equation 1-7 ($\Delta T v = 0.7 \Delta T A + 0.02 \sigma I$)	$\Delta T v$	18.31 °R
Tank Construction (pick from drop down list)		Welded		Fully Insulated - Equation 1-8 ($\Delta T v = 0.6 \Delta T A + 0.02 \sigma R I$)	$\Delta T v$	0.00 °R
Tank Shell Color (pick from drop down list)		White				
Tank Shell Condition (pick from drop down list)		Average				
Tank Interior Condition (pick from drop down list)		Light Rust		Average Daily Vapor Pressure Range ($\Delta P v$)	$\Delta P v$	0.00000 psia
Tank paint solar absorptance, dimensionless; Table 7.1-6	α	0.25		Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25 $P V X = \exp(P V N)$)	PvX	1.00000 psia
Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	-0.03	psi	Vapor pressure at ave daily min liquid surface temp. (Eq. 1-25 $P V N = \exp(P V N)$)	PvN	1.00000 psia
True Vapor Pressure; Eq. 1-25, $PvA = \exp(A \cdot (B/TLA))$						
Not Insulated	PvA	0.1417706		Average daily max. liquid surface temp.; Fig. 7.1-17 $TLX = TLA + 0.25 \Delta T v$	TLX	536.72 °R
Partially Insulated	PvA	0.1424275		Average daily min. liquid surface temp.; Fig. 7.1-17 $TLN = TLA - 0.25 \Delta T v$	TLN	526.81 °R
Fully Insulated	PvA	0.1336728		Partially Insulated - Equation 1-9: $\Delta P v = P v X - P v N$	$\Delta P v$	0.00000 psia
Average Daily Ambient Temperature (TAA) Eq. 1-30 $TAA = ((TAX+TAN)/2)$						
Average daily ambient temperature, Table 7.1-7	TAX	536.10	°R	Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25 $P V X$)	PvX	1.000000 psia
Average daily maximum ambient temperature, Table 7.1-7	TAN	521.10	°R	Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25 $P V N$)	PvN	1.000000 psia
Average daily minimum ambient temperature, Table 7.1-7	TAN	521.10	°R	Average daily maximum liquid surface temperature, deg R ($TLX = TLA + TLX$)	TLX	536.48 °R
				Average daily minimum liquid surface temperature, deg R ($TLN = TLA - TLN$)	TLN	527.33 °R
Liquid Bulk Temperature; Eq. 1-31: $TB = TAA + 0.003 \sigma I$						
	TB	530.00	°R	Fully Insulated ($\Delta P v = 0$)	$\Delta P v$	0.00 psia
Average Daily Liquid Surface Temperature (TLA)						
Not Insulated; Eq. 1-28, $TLA = 0.4 \cdot TAA + 0.6 \cdot TB + 0.005 \cdot \sigma I$	TLA	531.77	°R	Vapor Space Volume (Eq. 1-3: $Vv = ((P/4) \cdot D^2 \cdot Hvo)$)	Vv	549.78 ft ³
Partially Insulated; Eq. 1-29, $TLA = 0.3 \cdot TAA + 0.7 \cdot TB + 0.005 \cdot \sigma I$	TLA	531.91	°R	Effective Tank diameter	D _e	13.35 ft
Fully Insulated; $TLA = TB$	TLA	530.0	°R	Effective Tank Height	H _e	7.85 ft
				Vapor Space Outage $Hvo = 1/2 H$	Hvo	3.93 ft
Average Vapor Temperature (Tv)						
Not Insulated; Eq. 1-33, $Tv = 0.7 \cdot TAA + 0.3 \cdot TB + 0.009 \cdot \sigma I$	Tv	533.21	°R			
Partially Insulated; Eq. 1-34, $Tv = 0.6 \cdot TAA + 0.4 \cdot TB + 0.01 \cdot \sigma I$	Tv	533.81	°R			
Fully Insulated; $Tv = TB$	Tv	530.00	°R			
Stock Vapor Density; Eq. 1-22, $Wv = (Mv \cdot PvA) / (R \cdot Tv)$						
Not Insulated	Wv	3.221E-03				
Partially Insulated	Wv	3.232E-03				
Fully Insulated	Wv	3.055E-03				

HAPS Speciation	Product	lb/month	Vapor Weight Concentration	Vapor Mole Fraction
Total HAP Emissions =	4.515		Eq. 40-6 $Zvi = yiMi / MV$	Eq. 40-5 $yi = Pi / PVA$
Eq. 40-2 $L_i = Z_i(L_i)$				
Individual HAPS				
	L_i (lb/month			

Monthly Calculations (continued)

NOVEMBER

Tank No.	10455A	Symbol	Units	ROUTINE EMISSIONS CALCULATIONS	Symbol	Units
ROUTINE EMISSIONS CALCULATIONS						
Total Losses (Eq. 1-1: $LT = LS + LW$)	LT	1.66	lb/month	Standing Losses; Eq. 1-2, $LS = 365 (Vv \cdot Wv \cdot Ke \cdot Ks)$	LS	0.47 lb/month
		8.30E-04	ton/month	Vapor Space Volume	Vv	549.8 ft ³
				Stock Vapor Density	Wv	0.0014 lb/ft ³
				Vapor Space Expansion Factor ($0 < Ke \leq 1$); Eq. 1-5	Ke	0.021 per day
Nearest US Location		Bridgeport, CT		Vented Vapor Saturation Factor	Ks	1.00 NA
Daily total solar insolation on a horizontal surface; Table 7.1-7	I	621.0	Btu/ft ² -day	Constant; Number of Daily Events in a Year	365	30 days/month
Absolute Pressure	Pa	14.69	psia	Working Losses; Eq. 1-35, $Lw = VQ \cdot KN \cdot Kp \cdot Wv \cdot Kb$	Lw	1.19 lb/month
Ideal Gas Constant	R	10.73	psia ft ³ /lb-mole R	Net Working Loss Throughput (Eq. 1-39: $VO=5.614 \cdot Q$)	VQ	855 ft ³ /month
Product Information						
Product Type		Diesel Additive		Working Loss Turnover Factor Eq. 1-35 $Kp=(180+N)/N$ for $N \geq 36$, else $Kp=KN$	KN	1.0000
Vapor Molecular weight	Mv	130	lb/lb-mole	Working Loss Product Factor	Kp	1.00
Average organic liquid density	WL	6.10	lb/gal	Stock Vapor Density	Wv	0.0014 lb/ft ³
Average Reid Vapor Pressure	RVP	0.00		Vent Setting Correction Factor	KB	1.00
Product factor; 0.4 for crude oils or 1 for other organic liquids	Kc	1.00		Vented Vapor Saturation Factor; Eq. 1-21, $Ks = 1/(1+0.053 \cdot PVA \cdot Hvo)$		
Vapor Pressure Equation Constant A	A	0.00		Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.0581 psia
Vapor Pressure Equation Constant B (Table 7.1-2)	B	0.0		Vapor Space Outage	Hvo	0.00 ft
Tank design data						
Shell height	Hs	7.85	ft	Vapor Space Expansion Factor (Eq. 1-5: $(\Delta T v / TLA) \cdot ((\Delta P v - \Delta P B) / (P v - P v A))$	KE	0.0207 per day
Diameter	D	13.35	ft	Average Daily Vapor Temperature Range	$\Delta T v$	12.56 °R
Throughput	Q	6.400	gal/month	Average Daily Vapor Pressure Range	$\Delta P v$	0.0000 psia
Turnovers	N	9.47	per year	Breather Vent Pressure Setting Range (Equation 1-10: $\Delta P B = P B P - P B V$)	$\Delta P B$	0.0600 psi
Roof Type:		0.00		Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.0581 psia
Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft	Average Daily Liquid Surface Temperature	TLA	506.41 °R
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA	ft	Atmospheric Pressure	Pa	14.69 psia
Maximum Filling Height - use (Pi/4)D if unknown	HLX	6.85	ft	Average Daily Vapor Temperature Range ($\Delta T v$)		
Minimum Filling Height (use 0 if unknown)	HLN	1.00	ft	Average daily ambient temperature range - Equation 1-11 ($\Delta T A = T A X - T A I$)	$\Delta T A$	13.5 °R
Liquid height (assume 1/2 H)	HL	3.93	ft	Not Insulated - Equation 1-7 ($\Delta T v = 0.7 \Delta T A + 0.92 \sigma I$)	$\Delta T v$	12.56 °R
Tank insulation (pick from drop down list)		Not Insulated		Partially Insulated - Equation 1-8 ($\Delta T v = 0.6 \Delta T A + 0.02 \sigma R I$)	$\Delta T v$	11.21 °R
Tank Construction (pick from drop down list)		Welded		Fully Insulated, constant temperature	$\Delta T v$	0.00 °R
Tank Shell Color (pick from drop down list)		White		Average Daily Vapor Pressure Range ($\Delta P v$)		
Tank Shell Condition (pick from drop down list)		Average		Not Insulated - Equation 1-9: $\Delta P v = P v X - P v N$	$\Delta P v$	0.00000 psia
Tank Interior Condition (pick from drop down list)		Light Rust		Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25 $P v X = e x P v X$)	PvX	1.00000 psia
Tank paint solar absorptance, dimensionless, Table 7.1-6	α	0.25		Vapor pressure at ave daily min liquid surface temp. (Eq. 1-25 $P v N = e x P v N$)	PvN	1.00000 psia
Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	-0.03	psi	Average daily max. liquid surface temp.; Fig. 7.1-17 $T L X = T L A + 0.25 \Delta T$	TLX	509.54 °R
True Vapor Pressure; Eq. 1-25, $P v A = \exp(A \cdot (B/T L A))$						
Not Insulated	PvA	0.0580534		Average daily min. liquid surface temp.; Fig. 7.1-17 $T L N = T L A - 0.25 \Delta T$	TLN	503.27 °R
Partially Insulated	PvA	0.0581547		Partially Insulated - Equation 1-9: $\Delta P v = P v X - P v N$		
Fully Insulated	PvA	0.0567834		Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25 $u P v X$)	PvX	1.00000 psia
Average Daily Ambient Temperature (TAA) Eq. 1-30 $T A A = ((T A X + T A N) / 2)$						
Not Insulated	TAA	505.35	°R	Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25 $u P v N$)	PvN	1.000000 psia
Partially Insulated	TAX	512.10	°R	Average daily maximum liquid surface temperature, deg R ($T L X = T L A + T L X$)	TLX	509.25 °R
Fully Insulated	TAN	498.60	°R	Average daily minimum liquid surface temperature, deg R ($T L N = T L A - T L N$)	TLN	503.65 °R
Liquid Bulk Temperature; Eq. 1-31: $T B = T A A + 0.003 \sigma I$						
Not Insulated	TB	505.82	°R	Fully Insulated ($\Delta P v = 0$)		
Average Daily Liquid Surface Temperature (TLA)						
Not Insulated; Eq. 1-28, $T L A = 0.4 \cdot T A A + 0.6 \cdot T B + 0.005 \cdot \sigma I$	TLA	506.41	°R	Vapor Space Volume (Eq. 1-3: $V v = ((P i / 4) D^2 H)$	Vv	549.78 ft ³
Partially Insulated; Eq. 1-29, $T L A = 0.3 \cdot T A A + 0.7 \cdot T B + 0.005 \cdot \sigma I$	TLA	506.45	°R	Effective Tank diameter	D _e	13.35 ft
Fully Insulated; $T L A = T B$	TLA	505.8	°R	Effective Tank Height	H _e	7.85 ft
Average Vapor Temperature (Tv)						
Not Insulated; Eq. 1-33, $T v = 0.7 \cdot T A A + 0.3 \cdot T B + 0.009 \cdot \sigma I$	Tv	506.89	°R	Vapor Space Outage $H v o = 1/2 H$	Hvo	3.93 ft
Partially Insulated; Eq. 1-34, $T v = 0.6 \cdot T A A + 0.4 \cdot T B + 0.01 \cdot \sigma I$	Tv	507.09	°R	Average Vapor Pressure Range ($\Delta P v$)		
Fully Insulated; $T v = T B$	Tv	505.82	°R	Not Insulated - Equation 1-9: $\Delta P v = P v X - P v N$	$\Delta P v$	0.00000 psia
Stock Vapor Density; Eq. 1-22, $W v = (M v \cdot P v A) / (R \cdot T v)$						
Not Insulated	Wv	1.387E-03		Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25 $P v X = e x P v X$)	PvX	1.00000 psia
Partially Insulated	Wv	1.389E-03		Vapor pressure at ave daily min liquid surface temp. (Eq. 1-25 $P v N = e x P v N$)	PvN	1.00000 psia
Fully Insulated	Wv	1.360E-03		Average daily max. liquid surface temp.; Fig. 7.1-17 $T L X = T L A + 0.25 \Delta T$	TLX	499.18 °R
				Average daily min. liquid surface temp.; Fig. 7.1-17 $T L N = T L A - 0.25 \Delta T$	TLN	493.52 °R

HAPS Speciation	Product	lb/month	Vapor Weight Concentration	Vapor Mole Fraction
Total HAP Emissions =	1.660		Eq. 40-6 $Z v i = y i M i / M v$	Eq. 40-5 $y i = P v / P v A$
Eq. 40-2 $L i = Z i (L i)$				
Individual HAPS				
hexane	0.0000	86.18	130	0.00000
benzene	0.0000	78.11	130	0.00000
2,2,4 TMP	0.0000	114.23	130	0.00000
toluene	0.0000	92.14	130	0.00000
ethylbenzene	0.4856	106.17	130	0.29247
xylene	1.1748	106.17	130	0.70753
naphthalene	0.0000	128.17	130	0.00E+00
cumene	0.0000	120.19	130	0.00E+00
Liquid Mole Fraction				
Eq. 40-4 $x i = (Z i \cdot M i) / M i$				
Component Vapor Pressure				
Eq. 40-3 $P v i = (0.1013277) \cdot 10^{(A - (B / (T L A - C)))}$				
Individual HAPS				
hexane	0.00000	130	86.18	0.00000
benzene	0.00000	130	78.11	0.00000
2,2,4 TMP	0.00000	130	114.23	0.00000
toluene	0.00000	130	92.14	0.00000
ethylbenzene	0.26400	130	106.17	0.32326
xylene	0.73600	130	106.17	0.90120
naphthalene	0.00000	130	128.17	0.00000
cumene	0.00000	130	120.19	0.00000

Monthly Calculations (continued)

DECEMBER

Tank No.	10455A	Symbol	Units	ROUTINE EMISSIONS CALCULATIONS	Symbol	Units
ROUTINE EMISSIONS CALCULATIONS						
Total Losses (Eq. 1-1: $LT = LS + LW$)	LT	1.13	lb/month	Standing Losses; Eq. 1-2, $LS = 365 (Vv \cdot Wv \cdot Ke \cdot Ks)$	LS	0.31 lb/month
		5.65E-04	ton/month	Vapor Space Volume	Vv	549.8 ft ³
				Stock Vapor Density	Wv	0.0010 lb/ft ³
				Vapor Space Expansion Factor ($0 < Ke \leq 1$); Eq. 1-5	Ke	0.019 per day
Nearest US Location		Bridgeport, CT		Vented Vapor Saturation Factor	Ks	1.00 NA
Daily total solar insolation on a horizontal surface; Table 7.1-7	I	501.0	Btu/ft ² -day	Constant; Number of Daily Events in a Year	365	31 days/month
Absolute Pressure	Pa	14.69	psia	Working Losses; Eq. 1-35, $Lw = VQ \cdot KN \cdot Kp \cdot Wv \cdot Kb$	Lw	0.82 lb/month
Ideal Gas Constant	R	10.73	psia ft ³ /lb-mole R	Net Working Loss Throughput (Eq. 1-39: $VO=5.614 \cdot Q$)	VQ	855 ft ³ /month
Product Information						
Product Type		Diesel Additive		Working Loss Turnover Factor Eq. 1-35 $Kp=(180+N)/N$ for $N \geq 36$, else $Kp=KN$	KN	1.0000
Vapor Molecular weight	Mv	130	lb/lb-mole	Working Loss Product Factor	Kp	1.00
Average organic liquid density	WL	6.10	lb/gal	Stock Vapor Density	Wv	0.0010 lb/ft ³
Average Reid Vapor Pressure	RVP	0.00		Vent Setting Correction Factor	KB	1.00
Product factor; 0.4 for crude oils or 1 for other organic liquids	Kc	1.00		Vented Vapor Saturation Factor; Eq. 1-21, $Ks = 1/(1+0.053 \cdot PVA \cdot Hvo)$		
Vapor Pressure Equation Constant A	A	0.00		Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.0395 psia
Vapor Pressure Equation Constant B (Table 7.1-2)	B	0.0		Vapor Space Outage	Hvo	0.00 ft
Tank design data						
Shell height	Hs	7.85	ft	Vapor Space Expansion Factor (Eq. 1-5: $(\Delta T v / TLA) \cdot ((\Delta P v - \Delta P B) / (P v - P v A))$	KE	0.0187 per day
Diameter	D	13.35	ft	Average Daily Vapor Temperature Range	$\Delta T v$	11.33 °R
Throughput	Q	6.400	gal/month	Average Daily Vapor Pressure Range	$\Delta P v$	0.0000 psia
Turnovers	N	9.16	per year	Breather Vent Pressure Setting Range (Equation 1-10: $\Delta P B = P B P - P B V$)	$\Delta P B$	0.0600 psi
Roof Type:		0.00		Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.0395 psia
Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft	Average Daily Liquid Surface Temperature	TLA	496.35 °R
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA	ft	Atmospheric Pressure	Pa	14.69 psia
Maximum Filling Height - use (Pi/4)D if unknown	HLX	6.85	ft	Average Daily Vapor Temperature Range ($\Delta T v$)		
Minimum Filling Height (use 0 if unknown)	HLN	1.00	ft	Average daily ambient temperature range - Equation 1-11 ($\Delta T A = T A X - T A I$)	$\Delta T A$	12.6 °R
Liquid height (assume 1/2 H)	HL	3.93	ft	Not Insulated - Equation 1-7 ($\Delta T v = 0.7 \Delta T A + 0.92 \sigma I$)	$\Delta T v$	11.33 °R
Tank insulation (pick from drop down list)		Not Insulated		Partially Insulated - Equation 1-8 ($\Delta T v = 0.6 \Delta T A + 0.02 \sigma R I$)	$\Delta T v$	10.07 °R
Tank Construction (pick from drop down list)		Welded		Fully Insulated, constant temperature	$\Delta T v$	0.00 °R
Tank Shell Color (pick from drop down list)		White		Average Daily Vapor Pressure Range ($\Delta P v$)		
Tank Shell Condition (pick from drop down list)		Average		Not Insulated - Equation 1-9: $\Delta P v = P v X - P v N$	$\Delta P v$	0.00000 psia
Tank Interior Condition (pick from drop down list)		Light Rust		Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25 $P v X = e x P v X$)	PvX	1.00000 psia
Tank paint solar absorptance, dimensionless, Table 7.1-6	α	0.25		Vapor pressure at ave daily min liquid surface temp. (Eq. 1-25 $P v N = e x P v N$)	PvN	1.00000 psia
Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	-0.03	psi	Average daily max. liquid surface temp.; Fig. 7.1-17 $T L X = T L A + 0.25 \Delta T$	TLX	499.18 °R
True Vapor Pressure; Eq. 1-25, $P v A = \exp(A \cdot (B/T L A))$						
Not Insulated	PvA	0.0394603		Average daily min. liquid surface temp.; Fig. 7.1-17 $T L N = T L A - 0.25 \Delta T$	TLN	493.52 °R
Partially Insulated	PvA	0.0395187		Partially Insulated - Equation 1-9: $\Delta P v = P v X - P v N$		
Fully Insulated	PvA	0.0387265		Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25 $u P v X$)	PvX	1.00000 psia
Average Daily Ambient Temperature (TAA) Eq. 1-30 $T A A = ((T A X + T A N) / 2)$						
Not Insulated	TAA	495.50	°R	Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25 $u P v N$)	PvN	1.000000 psia
Partially Insulated	TAX	501.80	°R	Average daily maximum liquid surface temperature, deg R ($T L X = T L A + T L X$)	TLX	498.91 °R
Fully Insulated	TAN	489.20	°R	Average daily minimum liquid surface temperature, deg R ($T L N = T L A - T L N$)	TLN	493.87 °R
Liquid Bulk Temperature; Eq. 1-31: $T B = T A A + 0.003 \sigma I$						
Not Insulated	TB	495.88	°R	Fully Insulated ($\Delta P v = 0$)		
Average Daily Liquid Surface Temperature (TLA)						
Not Insulated; Eq. 1-28, $T L A = 0.4 \cdot T A A + 0.6 \cdot T B + 0.005 \cdot \sigma I$	TLA	496.35	°R	Vapor Space Volume (Eq. 1-3: $V v = ((P i / 4) D^2 H)$	Vv	549.78 ft ³
Partially Insulated; Eq. 1-29, $T L A = 0.3 \cdot T A A + 0.7 \cdot T B + 0.005 \cdot \sigma I$	TLA	496.39	°R	Effective Tank diameter	D _e	13.35 ft
Fully Insulated; $T L A = T B$	TLA	495.9	°R	Effective Tank Height	H _e	7.85 ft
Average Vapor Temperature (Tv)						
Not Insulated; Eq. 1-33, $T v = 0.7 \cdot T A A + 0.3 \cdot T B + 0.009 \cdot \sigma I$	Tv	496.74	°R	Vapor Space Outage $H v o = 1/2 H$	Hvo	3.93 ft
Partially Insulated; Eq. 1-34, $T v = 0.6 \cdot T A A + 0.4 \cdot T B + 0.01 \cdot \sigma I$	Tv	496.90	°R	Average Vapor Pressure Range ($\Delta P v$)		
Fully Insulated; $T v = T B$	Tv	495.88	°R	Not Insulated - Equation 1-9: $\Delta P v = P v X - P v N$	$\Delta P v$	0.00000 psia
Stock Vapor Density; Eq. 1-22, $W v = (M v \cdot P v A) / (R \cdot T v)$						
Not Insulated	Wv	9.624E-04		Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25 $P v X = e x P v X$)	PvX	1.00000 psia
Partially Insulated	Wv	9.635E-04		Vapor pressure at ave daily min liquid surface temp. (Eq. 1-25 $P v N = e x P v N$)	PvN	1.00000 psia
Fully Insulated	Wv	9.461E-04		Average daily max. liquid surface temp.; Fig. 7.1-17 $T L X = T L A + 0.25 \Delta T$	TLX	499.18 °R
				Average daily min. liquid surface temp.; Fig. 7.1-17 $T L N = T L A - 0.25 \Delta T$	TLN	493.52 °R

HAPS Speciation	Product	lb/month	Vapor Weight Concentration	Vapor Mole Fraction
Total HAP Emissions =	1.130		Eq. 40-6 $Z v i = y i M i / M v$	Eq. 40-5 $y i = P v / P v A$
Eq. 40-2 $L i = Z i (L i)$				
Individual HAPS				
hexane	0.0000	86.18	130	0.00000
benzene	0.0000	78.11	130	0.00000
2,2,4 TMP	0.0000	114.23	130	0.00000
toluene	0.0000	92.		

Monthly Calculations - JANUARY

Tank No.	13061A			ROUTINE EMISSIONS CALCULATIONS			ROUTINE EMISSIONS CALCULATIONS			HAPS Speciation		lb/month						
	Symbol	Units	Value	Symbol	Units	Value	Symbol	Units	Value	Value	Value	Value						
	ROUTINE EMISSIONS CALCULATIONS			ROUTINE EMISSIONS CALCULATIONS			ROUTINE EMISSIONS CALCULATIONS			Product								
	Total Losses (Eq.1-1: LT = LS+LW)	LT	0.95	Standing Losses; Eq.1-2: LS = 365 (Vv * Wv * KE * Ks)	LS	0.27	Vapor Space Volume	Vv	549.8	Total HAP Emissions =	0.954	Vapor Weight Concentration						
	Daily total solar insolation on a horizontal surface; Table 7.1-7	I	590.0	Stock Vapor Density	Wv	0.0008	Stock Vapor Density	Wv	0.0008	Eq. 40-6 $ZV_i = y_i M_i / MV$		Vapor Mole Fraction						
	Absolute Pressure	P _a	14.69	Vapor Space Expansion Factor (0 < KE <= 1); Eq. 1-5	KE	0.020	Vapor Space Expansion Factor (0 < KE <= 1); Eq. 1-5	KE	0.020	Eq. 40-5 $y_i = P_i / PVA$								
	Ideal Gas Constant	R	10.73	Vented Vapor Saturation Factor	Ks	1.00	Vented Vapor Saturation Factor	Ks	1.00	Individual HAPS	L_{ti} (lb/month)	M_i	M_v	Z_{vi}	P_i = P_{v,i}(K_s)	P_{va}	y_i	
	Product Information			Working Losses; Eq.1-35: LW = VQ * KN * Kp * Wv * KB	LW	0.68	Net Working Loss Throughput (Eq. 1-39: VQ=5.614*Q)	VQ	855	hexane	0.0000	86.18	130	0.00000	0.000000	0.032	-	
	Product Type	Diezel Additive		Working Loss Turnover Factor Eq.1-35 $K_p = (180+N)/6N$ for N>36, else $K_p = 1$	KN	1.0000	Working Loss Turnover Factor Eq.1-35 $K_p = (180+N)/6N$ for N>36, else $K_p = 1$	KN	1.0000	benzene	0.0000	78.11	130	0.00000	0.000000	0.032	-	
	Vapor Molecular weight	Mv	130	Vented Vapor Saturation Factor; Eq. 1-21: $K_s = 1/(1+0.053^{PVA/Hvo})$	Ks	1.00	Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.0325	2,2,4 TMP	0.0000	114.23	130	0.00000	0.000000	0.032	-	
	Average organic liquid density	WL	6.10	Vapor Space Volume (Eq.1-3: $Vv = (PI/4) D^2 Hvo$)	Vv	549.8	Vapor Space Volume (Eq.1-3: $Vv = (PI/4) D^2 Hvo$)	Vv	549.8	toluene	0.0000	92.14	130	0.00000	0.000000	0.032	-	
	Average Reid Vapor Pressure	RVP	0.00	Effective Tank diameter	D _e	13.35	Effective Tank diameter	D _e	13.35	ethylbenzene	0.2798	106.17	130	0.29329	0.011655	0.032	0.35912	
	Product factor: 0.4 for crude oils or 1 for other organic liquids	Kc	1.00	Effective Tank Height	H _e	7.85	Effective Tank Height	H _e	7.85	xylene	0.6742	106.17	130	0.70671	0.028084	0.032	0.86533	
	Vapor Pressure Equation Constant A	A	0.00	Vapor Space Outage	Hvo	0.00	Vapor Space Outage	Hvo	0.00	naphthalene	0.0000	128.17	130	0.00E+00	0.00E+00	0.032	0.00E+00	
	Vapor Pressure Equation Constant B (Table 7.1-2)	B	0.0							cumene	0.0000	120.19	130	0.00E+00	0.00E+00	0.032	0.00E+00	
	Tank design data			Vapor Space Expansion Factor (Eq. 1-5: $(\Delta T_v/TLA) \cdot (\Delta P_v - \Delta P_B) / (P_A - PVA)$)	KE	0.0198	Average Daily Vapor Temperature Range (ΔT_v)	ΔT_v	11.76	Individual HAPS	Z_i	M_i	M_v	X_i	A	B	C	P_{VAL}
	Shell height	Hs	7.85	Average Daily Vapor Temperature Range	ΔT_v	11.76	Average daily ambient temperature range - Equation 1-11 ($\Delta T_A = T_{AX} - T_{AT}$)	ΔT_A	12.8	hexane	0.00000	130	86.18	0.00000	6.878	1171.5	224.37	0.8715
	Diameter	D	13.35	Not Insulated - Equation 1-7 ($\Delta T_v = 0.7 \Delta T_A + 0.02 \alpha$)	ΔT_v	11.76	Not Insulated - Equation 1-7 ($\Delta T_v = 0.7 \Delta T_A + 0.02 \alpha$)	ΔT_v	11.76	benzene	0.00000	130	78.11	0.00000	6.906	1211	220.79	0.5064
	Throughput	Q	6.400	Partially Insulated - Equation 1-8 ($\Delta T_v = 0.6 \Delta T_A + 0.02 \alpha$)	ΔT_v	10.48	Partially Insulated - Equation 1-8 ($\Delta T_v = 0.6 \Delta T_A + 0.02 \alpha$)	ΔT_v	10.48	2,2,4 TMP	0.00000	130	114.23	0.00000	6.812	1257.8	220.74	0.2495
	Turnovers	N	9.16	Fully Insulated, constant temperature	ΔT_v	0.00	Fully Insulated, constant temperature	ΔT_v	0.00	toluene	0.00000	130	92.14	0.00000	7.017	1377.6	222.64	0.1296
	Roof Type:		0.00							ethylbenzene	0.26400	130	106.17	0.32326	8.95	1419.3	212.81	0.0361
	Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625							xylene	0.73600	130	106.17	0.90120	7.009	1462.3	215.11	0.0312
	Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA							naphthalene	0.00000	130	128.17	0.00000	7.146	1831.6	211.82	0.0006
	Maximum Filling Height - use (Pi/4)D if unknown	HLX	6.85							cumene	0.00000	130	120.19	0.00000	6.929	1455.8	207.2	0.0153
	Minimum Filling Height (use 0 if unknown)	HLN	1.00															
	Liquid height (assume 1/2 H)	HL	3.93															
	Tank Insulation (pick from drop down list)		Not Insulated															
	Tank Construction (pick from drop down list)		Welded															
	Tank Shell Color (pick from drop down list)		White															
	Tank Shell Condition (pick from drop down list)		Average															
	Tank Interior Condition (pick from drop down list)		Light Rust															
	Tank paint solar absorptance, dimensionless; Table 7.1-6	α	0.25															
	Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	-0.03															
	True Vapor Pressure; Eq. 1-25: $PVA = \exp(A - (B/TLA))$																	
	Not Insulated	PVA	0.032455															
	Partially Insulated	PVA	0.0325101															
	Fully Insulated	PVA	0.031764															
	Average Daily Ambient Temperature (TAA) Eq. 1-30 $TAA = ((TAX + TAN) / 2)$	TAA	490.50															
	Average daily maximum ambient temperature; Table 7.1-7	TAX	496.90															
	Average daily minimum ambient temperature; Table 7.1-7	TAN	484.10															
	Liquid Bulk Temperature; Eq. 1-31: $TB = TAA + 0.003 \alpha$	TB	490.92															
	Average Daily Liquid Surface Temperature (TLA)																	
	Not Insulated; Eq. 1-28: $TLA = 0.4 TAA + 0.6 TB + 0.005 \alpha$	TLA	491.45															
	Partially Insulated; Eq. 1-29: $TLA = 0.3 TAA + 0.7 TB + 0.005 \alpha$	TLA	491.49															
	Fully Insulated; $TLA = TB$	TLA	490.9															
	Average Vapor Temperature (Tv)																	
	Not Insulated; Eq. 1-33: $Tv = 0.7 TAA + 0.3 TB + 0.009 \alpha$	Tv	491.89															
	Partially Insulated; Eq. 1-34: $Tv = 0.6 TAA + 0.4 TB + 0.01 \alpha$	Tv	492.07															
	Fully Insulated; $Tv = TB$	Tv	490.92															
	Stock Vapor Density; Eq. 1-22: $Wv = (Mv PVA) / (R Tv)$																	
	Not Insulated	Wv	7.993E-04															
	Partially Insulated	Wv	8.004E-04															
	Fully Insulated	Wv	7.838E-04															

Monthly Calculations (continued)

Tank No.	13061A			ROUTINE EMISSIONS CALCULATIONS			ROUTINE EMISSIONS CALCULATIONS			HAPS Speciation		lb/month						
	Symbol	Units	Value	Symbol	Units	Value	Symbol	Units	Value	Value	Value	Value						
	ROUTINE EMISSIONS CALCULATIONS			ROUTINE EMISSIONS CALCULATIONS			ROUTINE EMISSIONS CALCULATIONS			Product								
	Total Losses (Eq.1-1: LT = LS+LW)	LT	1.05	Standing Losses; Eq.1-2: LS = 365 (Vv * Wv * KE * Ks)	LS	0.31	Vapor Space Volume	Vv	549.8	Total HAP Emissions =	1.053	Vapor Weight Concentration						
	Daily total solar insolation on a horizontal surface; Table 7.1-7	I	847.0	Stock Vapor Density	Wv	0.0009	Stock Vapor Density	Wv	0.0009	Eq. 40-6 $ZV_i = y_i M_i / MV$		Vapor Mole Fraction						
	Absolute Pressure	P _a	14.69	Vapor Space Expansion Factor (0 < KE <= 1); Eq. 1-5	KE	0.023	Vapor Space Expansion Factor (0 < KE <= 1); Eq. 1-5	KE	0.023	Eq. 40-5 $y_i = P_i / PVA$								
	Ideal Gas Constant	R	10.73	Vented Vapor Saturation Factor	Ks	1.00	Vented Vapor Saturation Factor	Ks	1.00	Individual HAPS	L_{ti} (lb/month)	M_i	M_v	Z_{vi}	P_i = P_{v,i}(K_s)	P_{va}	y_i	
	Product Information			Working Losses; Eq.1-35: LW = VQ * KN * Kp * Wv * KB	LW	0.74	Net Working Loss Throughput (Eq. 1-39: VQ=5.614*Q)	VQ	855	hexane	0.0000	86.18	130	0.00000	0.000000	0.035	-	
	Product Type	Diezel Additive		Working Loss Turnover Factor Eq.1-35 $K_p = (180+N)/6N$ for N>36, else $K_p = 1$	KN	1.0000	Working Loss Turnover Factor Eq.1-35 $K_p = (180+N)/6N$ for N>36, else $K_p = 1$	KN	1.0000	benzene	0.0000	78.11	130	0.00000	0.000000	0.035	-	
	Vapor Molecular weight	Mv	130	Vented Vapor Saturation Factor; Eq. 1-21: $K_s = 1/(1+0.053^{PVA/Hvo})$	Ks	1.00	Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.0354	2,2,4 TMP	0.0000	114.23	130	0.00000	0.000000	0.035	-	
	Average organic liquid density	WL	6.10	Vapor Space Volume (Eq.1-3: $Vv = (PI/4) D^2 Hvo$)	Vv	549.8	Vapor Space Volume (Eq.1-3: $Vv = (PI/4) D^2 Hvo$)	Vv	549.8	toluene	0.0000	92.14	130	0.00000	0.000000	0.035	-	
	Average Reid Vapor Pressure	RVP	0.00	Effective Tank diameter	D _e	13.35	Effective Tank diameter	D _e	13.35	ethylbenzene	0.3088	106.17	130	0.29318	0.012721	0.035	0.35898	
	Product factor: 0.4 for crude oils or 1 for other organic liquids	Kc	1.00	Effective Tank Height	H _e	7.85	Effective Tank Height	H _e	7.85	xylene	0.7444	106.17	130	0.70682	0.030669	0.035	0.86547	
	Vapor Pressure Equation Constant A	A	0.00	Vapor Space Outage	Hvo	0.00	Vapor Space Outage	Hvo	0.00	naphthalene	0.0000	128.17	130	0.00E+00	0.00E+00	0.035	0.00E+00	
	Vapor Pressure Equation Constant B (Table 7.1-2)	B	0.0							cumene	0.0000	120.19	130	0.00E+00	0.00E+00	0.035	0.00E+00	
	Tank design data			Vapor Space Expansion Factor (Eq. 1-5: $(\Delta T_v/TLA) \cdot (\Delta P_v - \Delta P_B) / (P_A - PVA)$)	KE	0.0232	Average Daily Vapor Temperature Range (ΔT_v)	ΔT_v	13.48	Individual HAPS	Z_i	M_i	M_v	X_i	A	B	C	P_{VAL}
	Shell height	Hs	7.85	Average Daily Vapor Temperature Range	ΔT_v	13.48	Average daily ambient temperature range - Equation 1-11 ($\Delta T_A = T_{AX} - T_{AT}$)	ΔT_A	13.2	hexane	0.00000	130	86.18	0.00000	6.878	1171.5	224.37	0.9299
	Diameter	D	13.35	Not Insulated - Equation 1-7 ($\Delta T_v = 0.7 \Delta T_A + 0.02 \alpha$)	ΔT_v	13.48	Not Insulated - Equation 1-7 ($\Delta T_v = 0.7 \Delta T_A + 0.02 \alpha$)	ΔT_v	13.48	benzene	0.00000	130	78.11	0.00000	6.906	1211	220.79	0.5427
	Throughput	Q	6.400	Partially Insulated - Equation 1-8 ($\Delta T_v = 0.6 \Delta T_A + 0.02 \alpha$)	ΔT_v	12.16	Partially Insulated - Equation 1-8 ($\Delta T_v = 0.6 \Delta T_A + $											

Monthly Calculations (continued)

MARCH

Tank No.	13061A			ROUTINE EMISSIONS CALCULATIONS			Symbol	Units	HAPS Speciation	lb/month	Product	Vapor Weight Concentration		Vapor Mole Fraction				
	ROUTINE EMISSIONS CALCULATIONS			ROUTINE EMISSIONS CALCULATIONS								Eq. 40-2 $Z_{vi} = y_i M_i / M_v$		Eq. 40-5 $y_i = P_i / PVA$				
Total Losses (Eq. 1-1: $LT = LS + LW$)													Total HAP Emissions = 1.500		Eq. 40-6 $Z_{vi} = y_i M_i / M_v$		Eq. 40-5 $y_i = P_i / PVA$	
	LT	1.50	lb/month	Standing Losses: Eq. 1-2: $LS = 365 (Vv * Wv * KE * Ks)$	LS	0.53	lb/month	Vapor Space Volume	Vv	549.8	ft ³	Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
		7.50E-04	ton/month	Stock Vapor Density	Wv	0.0011	lb/ft ³		Wv	0.0011	lb/ft ³	Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Vapor Space Expansion Factor ($0 < KE <= 1$): Eq. 1-5	KE	0.027	per day		KE	0.027	per day	Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Vented Vapor Saturation Factor	Ks	1.00	NA		Ks	1.00	NA	Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Constant: Number of Daily Events in a Year	365	31	days/month		365	31	days/month	Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Working Losses: Eq. 1-3: $Lw = VQ * KN * Kp * Wv * KB$	Lw	0.97	lb/month	Net Working Loss Throughput (Eq. 1-3: $VQ=5.614^{\circ}Q$)	VQ	855	ft ³ /month	Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Working Loss Turnover Factor Eq. 1-3: $Kp=(180+N)/6N$ for N=36, else $Kp=1$	KN	1.0000		Working Loss Turnover Factor	KN	1.0000		Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Working Loss Product Factor	Kp	1.00		Working Loss Product Factor	Kp	1.00		Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Stock Vapor Density	Wv	0.0011	lb/ft ³	Stock Vapor Density	Wv	0.0011	lb/ft ³	Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Vent Setting Correction Factor	KB	1.00		Vent Setting Correction Factor	KB	1.00		Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Vented Vapor Saturation Factor: Eq. 1-21: $Ks = 1/(1+0.053^{\circ}PVA^{\circ}Hvo)$	Ks	1.00		Vented Vapor Saturation Factor	Ks	1.00		Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.0470	psia	Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.0470	psia	Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Vapor Space Outage	Hvo	0.00	ft	Vapor Space Outage	Hvo	0.00	ft	Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Vapor Space Expansion Factor (Eq. 1-5: $(\Delta T_v/TLA) \cdot (\Delta P_v - \Delta P_B) / (P_A - PVA)$)	KE	0.0273	per day	Vapor Space Expansion Factor	KE	0.0273	per day	Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Average Daily Vapor Temperature Range	ΔT_v	15.72	°R	Average Daily Vapor Temperature Range	ΔT_v	15.72	°R	Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Average Daily Vapor Pressure Range	ΔP_v	0.0000	psia	Average Daily Vapor Pressure Range	ΔP_v	0.0000	psia	Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Not Insulated - Equation 1-7 ($\Delta T_v = 0.7 \Delta T_A + 0.02 \alpha R$)	ΔT_v	15.72	°R	Not Insulated - Equation 1-7 ($\Delta T_v = 0.7 \Delta T_A + 0.02 \alpha R$)	ΔT_v	15.72	°R	Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Partially Insulated - Equation 1-8 ($\Delta T_v = 0.6 \Delta T_A + 0.02 \alpha R$)	ΔT_v	14.30	°R	Partially Insulated - Equation 1-8 ($\Delta T_v = 0.6 \Delta T_A + 0.02 \alpha R$)	ΔT_v	14.30	°R	Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Fully Insulated, constant temperature	ΔT_v	0.00	°R	Fully Insulated, constant temperature	ΔT_v	0.00	°R	Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Average Daily Vapor Pressure Range (ΔP_v)	ΔP_v	0.00000	psia	Average Daily Vapor Pressure Range (ΔP_v)	ΔP_v	0.00000	psia	Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Not Insulated - Equation 1-9: $\Delta P_v = PVX - PVN$	ΔP_v	0.00000	psia	Not Insulated - Equation 1-9: $\Delta P_v = PVX - PVN$	ΔP_v	0.00000	psia	Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25: $PVX = e^{PVA}$)	PVX	1.00000	psia	Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25: $PVX = e^{PVA}$)	PVX	1.00000	psia	Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Vapor pressure at ave daily min liquid surface temp. (Eq. 1-25: $PVN = e^{PVA}$)	PVN	1.00000	psia	Vapor pressure at ave daily min liquid surface temp. (Eq. 1-25: $PVN = e^{PVA}$)	PVN	1.00000	psia	Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Average daily max. liquid surface temp.: Fig. 7.1-17 $TLX = TLA + 0.25 \Delta T_v$	TLX	504.80	°R	Average daily max. liquid surface temp.: Fig. 7.1-17 $TLX = TLA + 0.25 \Delta T_v$	TLX	504.80	°R	Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Average daily min. liquid surface temp.: Fig. 7.1-17 $TLN = TLA - 0.25 \Delta T_v$	TLN	496.94	°R	Average daily min. liquid surface temp.: Fig. 7.1-17 $TLN = TLA - 0.25 \Delta T_v$	TLN	496.94	°R	Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Partially Insulated - Equation 1-9: $\Delta P_v = PVX - PVN$	ΔP_v	0.00000	psia	Partially Insulated - Equation 1-9: $\Delta P_v = PVX - PVN$	ΔP_v	0.00000	psia	Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25: PVX)	PVX	1.00000	psia	Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25: PVX)	PVX	1.00000	psia	Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25: PVN)	PVN	1.000000	psia	Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25: PVN)	PVN	1.000000	psia	Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Average daily maximum ambient temperature, Table 7.1-7	TAX	506.00	°R	Average daily maximum ambient temperature, Table 7.1-7	TAX	506.00	°R	Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Average daily maximum liquid surface temperature, deg R ($TLX = TLA + TLX$)	TLX	504.80	°R	Average daily maximum liquid surface temperature, deg R ($TLX = TLA + TLX$)	TLX	504.80	°R	Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Average daily minimum ambient temperature, Table 7.1-7	TAN	491.80	°R	Average daily minimum ambient temperature, Table 7.1-7	TAN	491.80	°R	Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Average daily minimum liquid surface temperature, deg R ($TLN = TLA - TLN$)	TLN	496.94	°R	Average daily minimum liquid surface temperature, deg R ($TLN = TLA - TLN$)	TLN	496.94	°R	Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Fully Insulated ($\Delta P_v = 0$)	ΔP_v	0.00	psia	Fully Insulated ($\Delta P_v = 0$)	ΔP_v	0.00	psia	Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Vapor Space Volume (Eq. 1-3: $Vv = (PI/4) D^2 Hvo$)	Vv	549.78	ft ³	Vapor Space Volume (Eq. 1-3: $Vv = (PI/4) D^2 Hvo$)	Vv	549.78	ft ³	Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Effective Tank diameter	D_E	13.35	ft	Effective Tank diameter	D_E	13.35	ft	Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Effective Tank Height	H_E	7.85	ft	Effective Tank Height	H_E	7.85	ft	Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Vapor Space Outage $Hvo = 1/2 H$	Hvo	3.93	ft	Vapor Space Outage $Hvo = 1/2 H$	Hvo	3.93	ft	Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Average Vapor Temperature (T_v)	T_v	501.76	°R	Average Vapor Temperature (T_v)	T_v	501.76	°R	Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Not Insulated; Eq. 1-33: $T_v = 0.7 TAA + 0.3 T_B + 0.009 \alpha R$	T_v	501.76	°R	Not Insulated; Eq. 1-33: $T_v = 0.7 TAA + 0.3 T_B + 0.009 \alpha R$	T_v	501.76	°R	Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Partially Insulated; Eq. 1-34: $T_v = 0.6 TAA + 0.4 T_B + 0.01 \alpha R$	T_v	502.14	°R	Partially Insulated; Eq. 1-34: $T_v = 0.6 TAA + 0.4 T_B + 0.01 \alpha R$	T_v	502.14	°R	Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Fully Insulated; $T_v = T_B$	T_v	499.77	°R	Fully Insulated; $T_v = T_B$	T_v	499.77	°R	Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Stock Vapor Density: Eq. 1-22: $Wv = (Mv/PVA)/(R \cdot T_v)$	Wv	1.136E-03		Stock Vapor Density: Eq. 1-22: $Wv = (Mv/PVA)/(R \cdot T_v)$	Wv	1.136E-03		Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Not Insulated	Wv	1.136E-03		Not Insulated	Wv	1.136E-03		Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Partially Insulated	Wv	1.136E-03		Partially Insulated	Wv	1.136E-03		Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Fully Insulated	Wv	1.093E-03		Fully Insulated	Wv	1.093E-03		Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					

Monthly Calculations (continued)

APRIL

Tank No.	13061A			ROUTINE EMISSIONS CALCULATIONS			Symbol	Units	HAPS Speciation	lb/month	Product	Vapor Weight Concentration		Vapor Mole Fraction				
	ROUTINE EMISSIONS CALCULATIONS			ROUTINE EMISSIONS CALCULATIONS								Eq. 40-2 $Z_{vi} = y_i M_i / M_v$		Eq. 40-5 $y_i = P_i / PVA$				
Total Losses (Eq. 1-1: $LT = LS + LW$)													Total HAP Emissions = 2.288		Eq. 40-6 $Z_{vi} = y_i M_i / M_v$		Eq. 40-5 $y_i = P_i / PVA$	
	LT	2.29	lb/month	Standing Losses: Eq. 1-2: $LS = 365 (Vv * Wv * KE * Ks)$	LS	0.86	lb/month	Vapor Space Volume	Vv	549.8	ft ³	Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
		1.14E-03	ton/month	Stock Vapor Density	Wv	0.0017	lb/ft ³		Wv	0.0017	lb/ft ³	Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Vapor Space Expansion Factor ($0 < KE <= 1$): Eq. 1-5	KE	0.031	per day		KE	0.031	per day	Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Vented Vapor Saturation Factor	Ks	1.00	NA		Ks	1.00	NA	Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Constant: Number of Daily Events in a Year	365	30	days/month		365	30	days/month	Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Working Losses: Eq. 1-3: $Lw = VQ * KN * Kp * Wv * KB$	Lw	1.43	lb/month	Net Working Loss Throughput (Eq. 1-3: $VQ=5.614^{\circ}Q$)	VQ	855	ft ³ /month	Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Working Loss Turnover Factor Eq. 1-3: $Kp=(180+N)/6N$ for N=36, else $Kp=1$	KN	1.0000		Working Loss Turnover Factor	KN	1.0000		Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Working Loss Product Factor	Kp	1.00		Working Loss Product Factor	Kp	1.00		Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Stock Vapor Density	Wv	0.0017	lb/ft ³	Stock Vapor Density	Wv	0.0017	lb/ft ³	Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Vent Setting Correction Factor	KB	1.00		Vent Setting Correction Factor	KB	1.00		Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Vented Vapor Saturation Factor: Eq. 1-21: $Ks = 1/(1+0.053^{\circ}PVA^{\circ}Hvo)$	Ks	1.00		Vented Vapor Saturation Factor	Ks	1.00		Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.0706	psia	Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.0706	psia	Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Vapor Space Outage	Hvo	0.00	ft	Vapor Space Outage	Hvo	0.00	ft	Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Vapor Space Expansion Factor (Eq. 1-5: $(\Delta T_v/TLA) \cdot (\Delta P_v - \Delta P_B) / (P_A - PVA)$)	KE	0.0314	per day	Vapor Space Expansion Factor	KE	0.0314	per day	Eq. 40-2 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$					
				Average Daily Vapor Temperature Range	ΔT_v	18.												

Monthly Calculations (continued)

MAY

Tank No.	13061A	Symbol	Units	ROUTINE EMISSIONS CALCULATIONS	Symbol	Units
ROUTINE EMISSIONS CALCULATIONS						
Total Losses (Eq. 1-1: $LT = LS + LW$)	LT	3.33	lb/month	Standing Losses; Eq. 1-2: $LS = 365 (Vv \cdot Wv \cdot KE \cdot Ks)$	LS	1.34 lb/month
		1.67E-03	ton/month	Vapor Space Volume	Vv	549.8 ft ³
				Stock Vapor Density	Wv	0.0023 lb/ft ³
				Vapor Space Expansion Factor ($0 < KE <= 1$); Eq. 1-5	KE	0.034 per day
Nearest US Location	Bridgeport, CT			Vented Vapor Saturation Factor	Ks	1.00 NA
Daily total solar insolation on a horizontal surface; Table 7.1-7	I	1750.0	Btu/ft ² -day	Constant; Number of Daily Events in a Year	365	31 days/month
Absolute Pressure	P _A	14.69	psia	Working Losses; Eq. 1-35: $Lw = VQ \cdot KN \cdot Kp \cdot Wv \cdot KB$	Lw	1.99 lb/month
Ideal Gas Constant	R	10.73	psia ft ³ /lb-mole R	Net Working Loss Throughput (Eq. 1-39: $VQ=5.614 \cdot Q$)	VQ	855 ft ³ /month
Product Information						
Product Type	Diesel Additive			Working Loss Turnover Factor Eq. 1-35 $Kp=(180+N)/6N$ for N=36, else $Kp=1$	KN	1.0000
Vapor Molecular weight	Mv	130	Lb/lb-mole	Working Loss Product Factor	Kp	1.00
Average organic liquid density	WL	6.10	lb/gal	Stock Vapor Density	Wv	0.0023 lb/ft ³
Average Reid Vapor Pressure	RVP	0.00	psi	Vent Setting Correction Factor	KB	1.00
Product factor; 0.4 for crude oils or 1 for other organic liquids	Kc	1.00		Vented Vapor Saturation Factor; Eq. 1-21: $Ks = 1/(1+0.053 \cdot PVA/Hvo)$	Ks	1.00
Vapor Pressure Equation Constant A	A	0.00		Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.1005 psia
Vapor Pressure Equation Constant B (Table 7.1-2)	B	0.0	R	Vapor Space Outage	Hvo	0.00 ft
Tank design data						
Shell height	Hs	7.85	ft	Vapor Space Expansion Factor (Eq. 1-5: $(\Delta T_v/TLA) \cdot (\Delta P_v - \Delta P_B)/(PA - PVA)$)	KE	0.0337 per day
Diameter	D	13.35	ft	Average Daily Vapor Temperature Range	ΔT_v	19.74 °R
Throughput	Q	6.400	gal/month	Average Daily Vapor Pressure Range	ΔP_v	0.00000 psia
Turnovers	N	9.16	per year	Breather Vent Pressure Setting Range (Equation 1-10: $\Delta P_B = PBP - PVB$)	ΔP_B	0.0000 psi
Roof type:		0.00		Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.1005 psia
Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft	Average Daily Liquid Surface Temperature	TLA	521.63 °R
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA	ft	Atmospheric Pressure	P _A	14.69 psia
Maximum Filling Height - use (Pi/4)D if unknown	HLX	6.85	ft			
Minimum Filling Height (use 0 if unknown)	HLN	1.00	ft	Average Daily Vapor Temperature Range (ΔT_v)		
Liquid height (assume 1/2 H)	HL	3.93	ft	Average daily ambient temperature range - Equation 1-11 ($\Delta T_A = TAX - TA$)	ΔT_A	15.7 °R
Tank insulation (pick from drop down list)		Not Insulated		Not Insulated - Equation 1-7 ($\Delta T_v = 0.7 \Delta T_A + 0.02 \alpha R$)	ΔT_v	19.74 °R
Tank Construction (pick from drop down list)		Welded		Partially Insulated - Equation 1-8 ($\Delta T_v = 0.6 \Delta T_A + 0.02 \alpha R$)	ΔT_v	18.17 °R
Tank Shell Color (pick from drop down list)		White		Fully Insulated, constant temperature	ΔT_v	0.00 °R
Tank Shell Condition (pick from drop down list)		Average				
Tank Interior Condition (pick from drop down list)		Light Rust		Average Daily Vapor Pressure Range (ΔP_v)		
Tank paint solar absorptance, dimensionless; Table 7.1-6	α	0.25		Not Insulated - Equation 1-9: $\Delta P_v = PVX - PVN$	ΔP_v	0.00000 psia
Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	0.03	psi	Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25: $PVX = e^{PVA}$)	PVX	1.00000 psia
		-0.03		Vapor pressure at ave daily min liquid surface temp. (Eq. 1-25: $PVN = e^{PVA}$)	PVN	1.00000 psia
				Average daily max. liquid surface temp.; Fig. 7.1-17 $TLX = TLA + 0.25 \Delta T$	TLX	526.56 °R
				Average daily min. liquid surface temp.; Fig. 7.1-17 $TLN = TLA - 0.25 \Delta T$	TLN	516.69 °R
True Vapor Pressure; Eq. 1-25: $PVA = \exp(A - (B/TLA))$						
Not Insulated	P _{VA}	0.1005102		Partially Insulated - Equation 1-9: $\Delta P_v = PVX - PVN$	ΔP_v	0.00000 psia
Partially Insulated	P _{VA}	0.1009694		Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25: PVX)	PVX	1.00000 psia
Fully Insulated	P _{VA}	0.0948467		Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25: PVN)	PVN	1.000000 psia
Average Daily Ambient Temperature (TAA) Eq. 1-30 $TAA = ((TAX+1)/2)$						
Not Insulated	TAA	518.65	°R	Average daily maximum liquid surface temperature, deg R ($TLX = TLA + \Delta T$)	TLX	526.30 °R
Average daily maximum ambient temperature; Table 7.1-7	TAX	526.50	°R	Average daily minimum liquid surface temperature, deg R ($TLN = TLA - \Delta T$)	TLN	517.21 °R
Average daily minimum ambient temperature; Table 7.1-7	TAN	510.80	°R			
Liquid Bulk Temperature; Eq. 1-31: $TB = TAA + 0.003 \alpha s$						
Not Insulated	TB	519.96	°R	Fully Insulated ($\Delta P_v = 0$)	ΔP_v	0.00 psia
Average Daily Liquid Surface Temperature (TLA)						
Not Insulated; Eq. 1-28: $TLA = 0.4 \cdot TAA + 0.6 \cdot TB + 0.005 \cdot \alpha R$	TLA	521.63	°R	Vapor Space Volume (Eq. 1-3: $Vv = ((\pi/4) D^2 Hvo)$)	Vv	549.78 ft ³
Partially Insulated; Eq. 1-29: $TLA = 0.3 \cdot TAA + 0.7 \cdot TB + 0.005 \cdot \alpha R$	TLA	521.76	°R	Effective Tank diameter	D _E	13.35 ft
Fully Insulated; $TLA = TB$	TLA	520.0	°R	Effective Tank Height	H _E	7.85 ft
				Vapor Space Outage Hvo = 1/2 H	Hvo	3.93 ft
Average Vapor Temperature (Tv)						
Not Insulated; Eq. 1-33: $Tv = 0.7 \cdot TAA + 0.3 \cdot TB + 0.009 \cdot \alpha R$	Tv	522.98	°R			
Partially Insulated; Eq. 1-34: $Tv = 0.6 \cdot TAA + 0.4 \cdot TB + 0.01 \cdot \alpha R$	Tv	523.55	°R			
Fully Insulated; $Tv = TB$	Tv	519.96	°R			
Stock Vapor Density; Eq. 1-22: $Wv = (Mv \cdot PVA)/(R \cdot Tv)$						
Not Insulated	Wv	2.328E-03				
Partially Insulated	Wv	2.336E-03				
Fully Insulated	Wv	2.210E-03				

HAPS Speciation	lb/month	Vapor Weight Concentration	Vapor Mole Fraction
Total HAP Emissions = 3.330			
Eq. 40-2: $L_{ij} = Z_{ij}(L_i)$		Eq. 40-6: $Z_{vi} = y_i M_i / M_v$	Eq. 40-5: $y_i = P_i / PVA$
Individual HAPS	L_{ij} (lb/month)	M_i M_v Z_{vi}	P_i = P_{v,i}(X_i) P_{VA} y_i
hexane	0.0000	86.18 130 0.00000	0.000000 0.101 -
benzene	0.0000	78.11 130 0.00000	0.000000 0.101 -
2,2,4 TMP	0.0000	114.23 130 0.00000	0.000000 0.101 -
toluene	0.0000	92.14 130 0.00000	0.000000 0.101 -
ethylbenzene	0.9710	106.17 130 0.29159	0.035886 0.101 0.35740
xylene	2.3591	106.17 130 0.70841	0.087184 0.101 0.86742
naphthalene	0.0000	128.17 130 0.00E+00	0.00E+00 0.101 0.00E+00
cumene	0.0000	120.19 130 0.00E+00	0.00E+00 0.101 0.00E+00
Liquid Mole Fraction			
Eq. 40-4: $x_i = (Z_{ij} M_i) / M_v$	Z_i M_i M_v X_i	A B C P_{vi}	
Individual HAPS			
hexane	0.00000 130 86.18 0.00000	6.878 1171.5 224.37 2.0120	
benzene	0.00000 130 78.11 0.00000	6.906 1211 220.79 1.2359	
2,2,4 TMP	0.00000 130 114.23 0.00000	6.812 1257.8 220.74 0.8367	
toluene	0.00000 130 92.14 0.00000	7.017 1377.6 222.64 0.3517	
ethylbenzene	0.26400 130 106.17 0.32326	6.95 1419.3 212.61 0.1110	
xylene	0.73600 130 106.17 0.90120	7.009 1462.3 215.11 0.0967	
naphthalene	0.00000 130 128.17 0.00000	7.146 1831.6 211.82 0.0028	
cumene	0.00000 130 120.19 0.00000	6.929 1455.8 207.2 0.0515	

Monthly Calculations (continued)

JUNE

Tank No.	13061A	Symbol	Units	ROUTINE EMISSIONS CALCULATIONS	Symbol	Units
ROUTINE EMISSIONS CALCULATIONS						
Total Losses (Eq. 1-1: $LT = LS + LW$)	LT	4.52	lb/month	Standing Losses; Eq. 1-2: $LS = 365 (Vv \cdot Wv \cdot KE \cdot Ks)$	LS	1.76 lb/month
		2.26E-03	ton/month	Vapor Space Volume	Vv	549.8 ft ³
				Stock Vapor Density	Wv	0.0032 lb/ft ³
				Vapor Space Expansion Factor ($0 < KE <= 1$); Eq. 1-5	KE	0.033 per day
Nearest US Location	Bridgeport, CT			Vented Vapor Saturation Factor	Ks	1.00 NA
Daily total solar insolation on a horizontal surface; Table 7.1-7	I	1862.0	Btu/ft ² -day	Constant; Number of Daily Events in a Year	365	30 days/month
Absolute Pressure	P _A	14.69	psia	Working Losses; Eq. 1-35: $Lw = VQ \cdot KN \cdot Kp \cdot Wv \cdot KB$	Lw	2.76 lb/month
Ideal Gas Constant	R	10.73	psia ft ³ /lb-mole R	Net Working Loss Throughput (Eq. 1-39: $VQ=5.614 \cdot Q$)	VQ	855 ft ³ /month
Product Information						
Product Type	Diesel Additive			Working Loss Turnover Factor Eq. 1-35 $Kp=(180+N)/6N$ for N=36, else $Kp=1$	KN	1.0000
Vapor Molecular weight	Mv	130	Lb/lb-mole	Working Loss Product Factor	Kp	1.00
Average organic liquid density	WL	6.10	lb/gal	Stock Vapor Density	Wv	0.0032 lb/ft ³
Average Reid Vapor Pressure	RVP	0.00	psi	Vent Setting Correction Factor	KB	1.00
Product factor; 0.4 for crude oils or 1 for other organic liquids	Kc	1.00		Vented Vapor Saturation Factor; Eq. 1-21: $Ks = 1/(1+0.053 \cdot PVA/Hvo)$	Ks	1.00
Vapor Pressure Equation Constant A	A	0.00		Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.1418 psia
Vapor Pressure Equation Constant B (Table 7.1-2)	B	0.0	R	Vapor Space Outage	Hvo	0.00 ft
Tank design data						
Shell height	Hs	7.85	ft	Vapor Space Expansion Factor (Eq. 1-5: $(\Delta T_v/TLA) \cdot (\Delta P_v - \Delta P_B)/(PA - PVA)$)	KE	0.0331 per day
Diameter	D	13.35	ft	Average Daily Vapor Temperature Range	ΔT_v	19.81 °R
Throughput	Q	6.400	gal/month	Average Daily Vapor Pressure Range	ΔP_v	0.00000 psia
Turnovers	N	9.47	per year	Breather Vent Pressure Setting Range (Equation 1-10: $\Delta P_B = PBP - PVB$)	ΔP_B	0.0000 psi
Roof type:		0.00		Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.1418 psia
Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft	Average Daily Liquid Surface Temperature	TLA	531.77 °R
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA	ft	Atmospheric Pressure	P _A	14.69 psia
Maximum Filling Height - use (Pi/4)D if unknown	HLX	6.85	ft			
Minimum Filling Height (use 0 if unknown)	HLN	1.00	ft	Average Daily Vapor Temperature Range (ΔT_v)		
Liquid height (assume 1/2 H)	HL	3.93	ft	Average daily ambient temperature range - Equation 1-11 ($\Delta T_A = TAX - TA$)	ΔT_A	15.0 °R
Tank insulation (pick from drop down list)		Not Insulated		Not Insulated - Equation 1-7 ($\Delta T_v = 0.7 \Delta T_A + 0.02 \alpha R$)	ΔT_v	19.81 °R
Tank Construction (pick from drop down list)		Welded		Partially Insulated - Equation 1-8 ($\Delta T_v = 0.6 \Delta T_A + 0.02 \alpha R$)	ΔT_v	18.31 °R
Tank Shell Color (pick from drop down list)		White		Fully Insulated, constant temperature	ΔT_v	0.00 °R
Tank Shell Condition (pick from drop down list)		Average				
Tank Interior Condition (pick from drop down list)		Light Rust		Average Daily Vapor Pressure Range (ΔP_v)		
Tank paint solar absorptance, dimensionless; Table 7.1-6	α	0.25		Not Insulated - Equation 1-9: $\Delta P_v = PVX - PVN$	ΔP_v	0.00000 psia
Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	0.03	psi	Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25: $PVX = e^{PVA}$)	PVX	1.00000 psia
		-0.03		Vapor pressure at ave daily min liquid surface temp. (Eq. 1-25: $PVN = e^{PVA}$)	PVN	1.00000 psia
				Average daily max. liquid surface temp.; Fig. 7.1-17 $TLX = TLA + 0.25 \Delta T$	TLX	536.72 °R
				Average daily min. liquid surface temp.; Fig. 7.1-17 $TLN = TLA - 0.25 \Delta T$	TLN	526.81 °R
True Vapor Pressure; Eq. 1-25: $PVA = \exp(A - (B/TLA))$						
Not Insulated	P _{VA}	0.1417706		Partially Insulated - Equation 1-9: $\Delta P_v = PVX - PVN$	ΔP_v	0.00000 psia
Partially Insulated	P _{VA}	0.1424275		Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25: PVX)	PVX	1.00000 psia
Fully Insulated	P _{VA}	0.1336728		Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25: PVN)	PVN	1.000000 psia
Average Daily Ambient Temperature (TAA) Eq. 1-30 $TAA = ((TAX+1)/2)$						
Not Insulated	TAA	528.60	°R	Average daily maximum liquid surface temperature, deg R ($TLX = TLA + \Delta T$)	TLX	536.48 °R
Average daily maximum ambient temperature; Table 7.1-7	TAX	536.10	°R	Average daily minimum liquid surface temperature, deg R ($TLN = TLA - \Delta T$)	TLN	527.33 °R
Average daily minimum ambient temperature; Table 7.1-7	TAN	521.10	°R			
Liquid Bulk Temperature; Eq. 1-31: $TB = TAA + 0.003 \alpha s$						
Not Insulated	TB	530.00	°R	Fully Insulated ($\Delta P_v = 0$)	ΔP_v	0.00 psia
Average Daily Liquid Surface Temperature (TLA)						
Not Insulated; Eq. 1-28: $TLA = 0.4 \cdot TAA + 0.6 \cdot TB + 0.005 \cdot \alpha R$	TLA	531.77	°R	Vapor Space Volume (Eq. 1-3: $Vv = ((\pi/4) D^2 Hvo)$)	Vv	549.78 ft ³
Partially Insulated; Eq. 1-29: $TLA = 0.3 \cdot TAA + 0.7 \cdot TB + 0.005 \cdot \alpha R$	TLA	531.91	°R	Effective Tank diameter	D _E	13.35 ft
Fully Insulated; $TLA = TB$	TLA	530.0	°R	Effective Tank Height	H _E	7.85 ft
				Vapor Space Outage Hvo = 1/2 H	Hvo	3.93 ft
Average Vapor Temperature (Tv)						
Not Insulated; Eq. 1-33: $Tv = 0.7 \cdot TAA + 0.3 \cdot TB + 0.009 \cdot \alpha R$	Tv	533.21	°R			
Partially Insulated; Eq. 1-34: $Tv = 0.6 \cdot TAA + 0.4 \cdot TB + 0.01 \cdot \alpha R$	Tv	533.81	°R			
Fully Insulated; $Tv = TB$	Tv	530.00	°R			
Stock Vapor Density; Eq. 1-22: $Wv = (Mv \cdot PVA)/(R \cdot Tv)$						
Not Insulated	Wv	3.221E-03				
Partially Insulated	Wv	3.232E-03				
Fully Insulated	Wv	3.055E-03				

HAPS Speciation	lb/month	Vapor Weight Concentration	Vapor Mole Fraction
Total HAP Emissions = 4.515			
Eq. 40-2: $L_{ij} = Z_{ij}(L_i)$		Eq. 40-6: $Z_{vi} = y_i M_i / M_v$	Eq. 40-5: $y_i = P_i / PVA$
Individual HAPS	L_{ij} (lb/month)	M_i M_v Z_{vi}	P_i = P_{v,i}

Monthly Calculations (continued)

SEPTEMBER

Tank No.	13061A	Symbol	Units	Symbol	Units	HAPS Speciation	lb/month	Product	lb/month	Vapor Weight Concentration	Vapor Mole Fraction					
ROUTINE EMISSIONS CALCULATIONS																
Total Losses (Eq. 1-1: LT = LS+LW)	LT	3.80	lb/month	Standing Losses: Eq. 1-2: LS = 365 (Vv * Wv * KE * Ks)	LS	1.32	lb/month	Total HAP Emissions =	3.798	Vapor Weight Concentration	Vapor Mole Fraction					
		1.90E-03	ton/month	Vapor Space Volume	Vv	549.8	ft ³	Eq. 40-2 Zvi = yiMi / MV		Eq. 40-5 yi = Pi / PVA						
				Stock Vapor Density	Wv	0.0029	lb/ft ³									
				Vapor Space Expansion Factor (0 < KE <= 1); Eq. 1-5	KE	0.028	per day	Individual HAPS	L_{vi} (lb/month)	M_i	M_v	Z_{vi}	P_i = P_{va}(X_i)	P_{va}	y_i	
Nearest US Location	Bridgeport, CT			Vented Vapor Saturation Factor	Ks	1.00	NA	hexane	0.0000	86.18	130	0.00000	0.000000	0.127	-	
Daily total solar insolation on a horizontal surface; Table 7.1-7	I	1320.0	Btu/ft ² -day	Constant: Number of Daily Events in a Year	365	30	days/month	benzene	0.0000	78.11	130	0.00000	0.000000	0.127	-	
Absolute Pressure	P _a	14.69	psia	Working Losses: Eq. 1-35: LW = VQ * KN * Kp * Wv * KB	LW	2.48	lb/month	2,2,4 TMP	0.0000	114.23	130	0.00000	0.000000	0.127	-	
Ideal Gas Constant	R	10.73	psia ft ³ /lb-mole R	Net Working Loss Throughput (Eq. 1-39: VQ=5.614*Q)	VQ	855	ft ³ /month	toluene	0.0000	92.14	130	0.00000	0.000000	0.127	-	
Product Information				Working Loss Turnover Factor Eq. 1-35 K _w =(180+N)/6N for N>36, else K _w =N	KN	1.0000		ethylbenzene	1.061	106.17	130	0.29119	0.045169	0.127	0.35655	
Product Type	Diesel Additive			Working Loss Product Factor	Kp	1.00		xylene	2.624	106.17	130	0.70881	0.109948	0.127	0.86790	
Vapor Molecular weight	Mv	130	lb/lb-mole	Stock Vapor Density	Wv	0.0029	lb/ft ³	naphthalene	0.0000	128.17	130	0.00E+00	0.00E+00	0.127	0.00E+00	
Average organic liquid density	WL	6.10	lb/gal	Vent Setting Correction Factor	KB	1.00		cumene	0.0000	120.19	130	0.00E+00	0.00E+00	0.127	0.00E+00	
Average Reid Vapor Pressure	RVP	0.00	psi	Vented Vapor Saturation Factor: Eq. 1-21: Ks = 1/(1+0.053*PvA/Hvo)	Ks	1.00		Liquid Mole Fraction			Component Vapor Pressure					
Product factor: 0.4 for crude oils or 1 for other organic liquids	Kc	1.00		Vapor Pressure at Avg Daily Liq Surface Temp	PvA	0.1267	psia	Eq. 40-4 xi = (Z _{vi} M _i)/M _v	Z _{vi}	M _i	M _v	X _i	A	B	C	P _{vi}
Vapor Pressure Equation Constant A	A	0.00		Vapor Space Outage	Hvo	0.00	ft	hexane	0.00000	130	86.18	0.00000	6.878	1171.5	224.37	2.3895
Vapor Pressure Equation Constant B (Table 7.1-2)	B	0.0	R	Vapor Space Expansion Factor (Eq. 1-5: (ΔTv/TLA) * (ΔPv-ΔPb)/(PA-PVA) KE	KE	0.0276	per day	benzene	0.00000	130	78.11	0.00000	6.906	1211	220.79	1.4842
Tank design data				Average Daily Vapor Temperature Range	ΔTv	16.75	°R	2,2,4 TMP	0.00000	130	114.23	0.00000	6.812	1257.8	220.74	0.7627
Shell height	Hs	7.85	ft	Average Daily Vapor Pressure Range	ΔPv	0.00000	psia	toluene	0.00000	130	92.14	0.00000	7.017	1377.6	222.64	0.4318
Diameter	D	13.35	ft	Not Insulated - Equation 1-7 (ΔTv = 0.7 ΔTA + 0.02 α I)	ΔTv	16.75	°R	ethylbenzene	0.26400	130	106.17	0.32326	6.95	1419.3	212.61	0.1397
Throughput	Q	6.400	gal/month	Partially Insulated - Equation 1-8 (ΔTv = 0.6 ΔTA + 0.02 α R I)	ΔTv	15.30	°R	xylene	0.73600	130	106.17	0.90120	7.009	1462.3	215.11	0.1220
Turnovers	N	9.47	per year	Fully Insulated, constant temperature	ΔTv	0.00	°R	naphthalene	0.00000	130	128.17	0.00000	7.146	1831.6	211.82	0.0035
Roof type:		0.00		Average Daily Vapor Pressure Range (ΔPv)	ΔPv	0.00000	psia	cumene	0.00000	130	120.19	0.00000	6.929	1455.8	207.2	0.0659
Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft	Not Insulated - Equation 1-9: ΔPv = PVX - PVN	ΔPv	0.00000	psia	Component Vapor Pressure			PVA = (0.019377)¹⁰ PVA - (B)(TLA - C)					
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA	ft	Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25 PVX = e ^{ΔPv} PVA)	PVX	1.00000	psia	A	B	C	P _{vi}					
Maximum Filling Height - use (Pi/4)D if unknown	HLX	6.85	ft	Vapor pressure at ave. daily min liquid surface temp. (Eq. 1-25 PVN = e ^{-ΔPv} PVA)	PVN	1.00000	psia									
Minimum Filling Height (use 0 if unknown)	HLN	1.00	ft	Average daily max. liquid surface temp.; Fig. 7.1-17 TLX = TLA + 0.25ΔT TLX	TLX	532.58	°R									
Liquid height (assume 1/2 H)	HL	3.93	ft	Average daily min. liquid surface temp.; Fig. 7.1-17 TLN = TLA - 0.25ΔT TLN	TLN	524.21	°R									
Tank insulation (pick from drop down list)	Not Insulated			Partially Insulated - Equation 1-9: ΔPv = PVX - PVN	ΔPv	0.00000	psia									
Tank Construction (pick from drop down list)	Welded			Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25 PVX)	PVX	1.00000	psia									
Tank Shell Color (pick from drop down list)	White			Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25 PVN)	PVN	1.000000	psia									
Tank Shell Condition (pick from drop down list)	Average			Average daily maximum liquid surface temperature, deg R (TLX = TLA + TLX)	TLX	532.32	°R									
Tank Interior Condition (pick from drop down list)	Light Rust			Average daily minimum liquid surface temperature, deg R (TLN = TLA - TLN)	TLN	524.67	°R									
Tank paint solar absorptance, dimensionless; Table 7.1-6	α	0.25		Fully Insulated (ΔPv = 0)	ΔPv	0.00	psia									
Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	-0.03	psi	Vapor Space Volume (Eq. 1-3: Vv = ((Pi / 4) D²) Hvo	Vv	549.78	ft ³									
True Vapor Pressure: Eq. 1-25, PVA = exp(A-(B/TLA))				Effective Tank diameter	D _e	13.35	ft									
Not Insulated	P _{va}	0.1266829	psia	Effective Tank Height	H _e	7.85	ft									
Partially Insulated	P _{va}	0.1271055	psia	Vapor Space Outage Hvo = 1/2 H	Hvo	3.93	ft									
Fully Insulated	P _{va}	0.1214345	psia	Average Vapor Temperature (Tv)												
Average Daily Ambient Temperature (TAA) Eq. 1-30 TAA = ((TAX+1)	TAA	526.15	°R	Not Insulated; Eq. 1-33, Tv = 0.7*TAA + 0.3*TB + 0.009*o ¹	Tv	529.42	°R									
Average daily maximum ambient temperature; Table 7.1-7	TAX	533.40	°R	Partially Insulated; Eq. 1-34, Tv = 0.6*TAA + 0.4*TB + 0.01*o ¹ R ¹	Tv	529.85	°R									
Average daily minimum ambient temperature; Table 7.1-7	TAN	518.90	°R	Fully Insulated; Tv = TB	Tv	527.14	°R									
Liquid Bulk Temperature; Eq. 1-31: TB = TAA + 0.003 α I	TB	527.14	°R	Stock Vapor Density: Eq. 1-22, Wv = (Mv/PVA)/(R*TV)												
Average Daily Liquid Surface Temperature (TLA)				Not Insulated	Wv	2.899E-03										
Not Insulated; Eq. 1-28, TLA = 0.4*TAA + 0.6*TB + 0.005*o ¹	TLA	528.39	°R	Partially Insulated	Wv	2.906E-03										
Partially Insulated; Eq. 1-29, TLA = 0.3*TAA + 0.7*TB + 0.005*o ¹ R	TLA	528.49	°R	Fully Insulated	Wv	2.791E-03										
Fully Insulated; TLA = TB	TLA	527.1	°R													

Monthly Calculations (continued)

OCTOBER

Tank No.	13061A	Symbol	Units	Symbol	Units	HAPS Speciation	lb/month	Product	lb/month	Vapor Weight Concentration	Vapor Mole Fraction					
ROUTINE EMISSIONS CALCULATIONS																
Total Losses (Eq. 1-1: LT = LS+LW)	LT	2.53	lb/month	Standing Losses: Eq. 1-2: LS = 365 (Vv * Wv * KE * Ks)	LS	0.86	lb/month	Total HAP Emissions =	2.535	Vapor Weight Concentration	Vapor Mole Fraction					
		1.27E-03	ton/month	Vapor Space Volume	Vv	549.8	ft ³	Eq. 40-2 Zvi = yiMi / MV		Eq. 40-5 yi = Pi / PVA						
				Stock Vapor Density	Wv	0.0020	lb/ft ³									
				Vapor Space Expansion Factor (0 < KE <= 1); Eq. 1-5	KE	0.026	per day	Individual HAPS	L_{vi} (lb/month)	M_i	M_v	Z_{vi}	P_i = P_{va}(X_i)	P_{va}	y_i	
Nearest US Location	Bridgeport, CT			Vented Vapor Saturation Factor	Ks	1.00	NA	hexane	0.0000	86.18	130	0.00000	0.000000	0.084	-	
Daily total solar insolation on a horizontal surface; Table 7.1-7	I	948.0	Btu/ft ² -day	Constant: Number of Daily Events in a Year	365	31	days/month	benzene	0.0000	78.11	130	0.00000	0.000000	0.084	-	
Absolute Pressure	P _a	14.69	psia	Working Losses: Eq. 1-35: LW = VQ * KN * Kp * Wv * KB	LW	1.67	lb/month	2,2,4 TMP	0.0000	114.23	130	0.00000	0.000000	0.084	-	
Ideal Gas Constant	R	10.73	psia ft ³ /lb-mole R	Net Working Loss Throughput (Eq. 1-39: VQ=5.614*Q)	VQ	855	ft ³ /month	toluene	0.0000	92.14	130	0.00000	0.000000	0.084	-	
Product Information				Working Loss Turnover Factor Eq. 1-35 K _w =(180+N)/6N for N>36, else K _w =N	KN	1.0000		ethylbenzene	0.7398	106.17	130	0.29189	0.029849	0.084	0.35741	
Product Type	Diesel Additive			Working Loss Product Factor	Kp	1.00		xylene	1.7947	106.17	130	0.70811	0.072411	0.084	0.86704	
Vapor Molecular weight	Mv	130	lb/lb-mole	Stock Vapor Density	Wv	0.0020	lb/ft ³	naphthalene	0.0000	128.17	130	0.00E+00	0.00E+00	0.084	0.00E+00	
Average organic liquid density	WL	6.10	lb/gal	Vent Setting Correction Factor	KB	1.00		cumene	0.0000	120.19	130	0.00E+00	0.00E+00	0.084	0.00E+00	
Average Reid Vapor Pressure	RVP	0.00	psi	Vented Vapor Saturation Factor: Eq. 1-21: Ks = 1/(1+0.053*PvA/Hvo)	Ks	1.00		Liquid Mole Fraction			Component Vapor Pressure					
Product factor: 0.4 for crude oils or 1 for other organic liquids	Kc	1.00		Vapor Pressure at Avg Daily Liq Surface Temp	PvA	0.0835	psia	Eq. 40-4 xi = (Z _{vi} M _i)/M _v	Z _{vi}	M _i	M _v	X _i	A	B	C	P _{vi}
Vapor Pressure Equation Constant A	A	0.00		Vapor Space Outage	Hvo	0.00	ft	hexane	0.00000	130	86.18	0.00000	6.878	1171.5	224.37	1.7536
Vapor Pressure Equation Constant B (Table 7.1-2)	B	0.0	R	Vapor Space Expansion Factor (Eq. 1-5: (ΔTv/TLA) * (ΔPv-ΔPb)/(PA-PVA) KE	KE	0.0258	per day	benzene	0.00000	130	78.11	0.00000	6.906	1211	220.79	1.0675
Tank design data				Average Daily Vapor Temperature Range	ΔTv	15.45	°R	2,2,4 TMP	0.00000	130	114.23	0.00000	6.812	1257.8	220.74	0.5416
Shell height	Hs	7.85	ft	Average Daily Vapor Pressure Range	ΔPv	0.00000	psia	toluene	0.00000	130	92.14	0.00000	7.017	1377.6	222.64	0.2985
Diameter	D	13.35	ft	Not Insulated - Equation 1-7 (ΔTv = 0.7 ΔTA + 0.02 α I)	ΔTv	15.45	°R	ethylbenzene	0.26400	130	106.17	0.32326	6.95	1419.3	212.61	0.0923
Throughput	Q	6.400	gal/month	Partially Insulated - Equation 1-8 (ΔTv = 0.6 ΔTA + 0.02 α R I)	ΔTv	13.92	°R	xylene	0.73600	130	106.17	0.90120	7.009	1462.3	215.11	0.0804
Turnovers	N	9.16	per year	Fully Insulated, constant temperature	ΔTv	0.00	°R	naphthalene	0.00000	130	128.17	0.00000	7.146	1831.6	211.82	0.0020
Roof type:		0.00		Average Daily Vapor Pressure Range (ΔPv)	ΔPv	0.00000	psia	cumene	0.00000	130	120.19	0.00000	6.929	1455.8	207.2	0.0422
Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft	Not Insulated - Equation 1-9: ΔPv = PVX - PVN	ΔPv	0.00000	psia	Component Vapor Pressure			PVA = (0.019377)¹⁰ PVA - (B)(TLA - C)					
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA	ft	Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25 PVX = e ^{ΔPv} PVA)	PVX	1.00000	psia	A	B	C	P _{vi}					
Maximum Filling Height - use (Pi/4)D if unknown	HLX	6.85	ft	Vapor pressure at ave. daily min liquid surface temp. (Eq. 1-25 PVN = e ^{-ΔPv} PVA)	PVN	1.00000	psia									
Minimum Filling Height (use 0 if unknown)	HLN	1.00	ft	Average daily max. liquid surface temp.; Fig. 7.1-17 TLX = TLA + 0.25ΔT TLX	TLX	520.22	°R									
Liquid height (assume 1/2 H)	HL	3.93	ft	Average daily min. liquid surface temp.; Fig. 7.1-17 TLN = TLA - 0.25ΔT TLN	TLN	512.50	°R									
Tank insulation (pick from drop down list)	Not Insulated			Partially Insulated - Equation 1-9: ΔPv = PVX - PVN	ΔPv	0.00000	psia									
Tank Construction (pick from drop down list)	Welded			Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25 PVX)	PVX	1.00000	psia									

Monthly Calculations (continued)

NOVEMBER

Tank No.	13061A	Symbol	Units	ROUTINE EMISSIONS CALCULATIONS	Symbol	Units
ROUTINE EMISSIONS CALCULATIONS						
Total Losses (Eq. 1-1: $LT = LS+LW$)	LT	1.66	lb/month	Standing Losses; Eq. 1-2: $LS = 365 (Vv \cdot Wv \cdot KE \cdot Ks)$	LS	0.47 lb/month
		8.30E-04	ton/month	Vapor Space Volume	Vv	549.8 ft ³
				Stock Vapor Density	Wv	0.0014 lb/ft ³
				Vapor Space Expansion Factor ($0 < KE <= 1$); Eq. 1-5	KE	0.021 per day
Nearest US Location	Bridgeport, CT			Vented Vapor Saturation Factor	KS	1.00 NA
Daily total solar insolation on a horizontal surface; Table 7.1-7	I	621.0	Btu/ft ² -day	Constant; Number of Daily Events in a Year	365	30 days/month
Absolute Pressure	PA	14.69	psia	Working Losses; Eq. 1-35: $Lw = VQ \cdot KN \cdot Kp \cdot Wv \cdot KB$	Lw	1.19 lb/month
Ideal Gas Constant	R	10.73	psia ft ³ /lb-mole R	Net Working Loss Throughput (Eq. 1-39: $VQ=5.614 \cdot Q$)	VQ	855 ft ³ /month
Product Information				Working Loss Turnover Factor Eq. 1-35 $Kp=(180+N)/6N$ for N=36, else $Kp=1$	KN	1.0000
Product Type	Diesel Additive			Working Loss Product Factor	Kp	1.00
Vapor Molecular weight	Mv	130	Lb/lb-mole	Stock Vapor Density	Wv	0.0014 lb/ft ³
Average organic liquid density	WL	6.10	lb/gal	Vent Setting Correction Factor	KB	1.00
Average Reid Vapor Pressure	RVP	0.00	psi	Vented Vapor Saturation Factor; Eq. 1-21: $Ks = 1/(1+0.053 \cdot PVA/Hvo)$	Ks	1.00
Product factor; 0.4 for crude oils or 1 for other organic liquids	Kc	1.00		Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.0581 psia
Vapor Pressure Equation Constant A	A	0.00		Vapor Space Outage	Hvo	0.00 ft
Vapor Pressure Equation Constant B (Table 7.1-2)	B	0.0	R	Vapor Space Expansion Factor (Eq. 1-5: $(\Delta T/TLA) \cdot (\Delta Pv - \Delta PBI) / (PA - PVA)$)	KE	0.0207 per day
Tank design data				Average Daily Vapor Temperature Range	ΔT_v	12.56 °R
Shell height	Hs	7.85	ft	Average Daily Vapor Pressure Range	ΔP_v	0.00000 psia
Diameter	D	13.35	ft	Breather Vent Pressure Setting Range (Equation 1-10: $\Delta PBI = PBP - PBI$)	ΔPBI	0.0600 psi
Throughput	Q	6.400	gal/month	Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.0395 psia
Turnovers	N	9.47	per year	Average Daily Liquid Surface Temperature	TLA	496.35 °R
Roof type:		0.00		Atmospheric Pressure	PA	14.69 psia
Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft	Average Daily Vapor Temperature Range (ΔT_v)		
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA	ft	Average daily ambient temperature range - Equation 1-11 ($\Delta T_A = TAX - TAA$)	ΔT_A	13.5 °R
Maximum Filling Height - use (Pi/4)D if unknown	HLX	6.85	ft	Not Insulated - Equation 1-7 ($\Delta T_v = 0.7 \Delta T_A + 0.02 \alpha R$)	ΔT_v	12.56 °R
Minimum Filling Height (use 0 if unknown)	HLN	1.00	ft	Partially Insulated - Equation 1-8 ($\Delta T_v = 0.6 \Delta T_A + 0.02 \alpha R$)	ΔT_v	11.21 °R
Liquid height (assume 1/2 H)	HL	3.93	ft	Fully Insulated, constant temperature	ΔT_v	0.00 °R
Tank insulation (pick from drop down list)		Not Insulated		Average Daily Vapor Pressure Range (ΔP_v)		
Tank Construction (pick from drop down list)		Welded		Not Insulated - Equation 1-9: $\Delta P_v = PVX - PVN$	ΔP_v	0.00000 psia
Tank Shell Color (pick from drop down list)		White		Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25: $PVX = e^{PVA}$)	PVX	1.00000 psia
Tank Shell Condition (pick from drop down list)		Average		Vapor pressure at ave daily min liquid surface temp. (Eq. 1-25: $PVN = e^{PVA}$)	PVN	1.00000 psia
Tank Interior Condition (pick from drop down list)		Light Rust		Average daily max. liquid surface temp.; Fig. 7.1-17 $TLX = TLA + 0.25 \Delta T$	TLX	509.54 °R
Tank paint solar absorptance, dimensionless; Table 7.1-6	α	0.25		Average daily min. liquid surface temp.; Fig. 7.1-17 $TLN = TLA - 0.25 \Delta T$	TLN	503.27 °R
Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	-0.03	psi	Partially Insulated - Equation 1-9: $\Delta P_v = PVX - PVN$	ΔP_v	0.00000 psia
True Vapor Pressure; Eq. 1-25: $PVA = \exp(A - (B/TLA))$				Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25: PVX)	PVX	1.00000 psia
Not Insulated	PVA	0.0580534	psi	Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25: PVN)	PVN	1.000000 psia
Partially Insulated	PVA	0.0581547	psi	Average daily maximum liquid surface temperature, deg R ($TLX = TLA +$)	TLX	509.25 °R
Fully Insulated	PVA	0.0567834	psi	Average daily minimum liquid surface temperature, deg R ($TLN = TLA -$)	TLN	503.65 °R
Average Daily Ambient Temperature (TAA) Eq. 1-30 $TAA = ((TAX+TAN)/2)$	TAA	505.35	°R	Fully Insulated ($\Delta P_v = 0$)	ΔP_v	0.00 psia
Average daily maximum ambient temperature; Table 7.1-7	TAX	512.10	°R	Vapor Space Volume (Eq. 1-3: $Vv = ((PI/4) D^2 Hvo)$)	Vv	549.78 ft ³
Average daily minimum ambient temperature; Table 7.1-7	TAN	498.60	°R	Effective Tank diameter	De	13.35 ft
Liquid Bulk Temperature; Eq. 1-31: $TB = TAA + 0.003 \alpha s$	TB	505.62	°R	Effective Tank Height	He	7.85 ft
Average Daily Liquid Surface Temperature (TLA)				Vapor Space Outage Hvo = 1/2 H	Hvo	3.93 ft
Not Insulated; Eq. 1-28: $TLA = 0.4 \cdot TAA + 0.6 \cdot TB + 0.005 \cdot \alpha R$	TLA	506.41	°R			
Partially Insulated; Eq. 1-29: $TLA = 0.3 \cdot TAA + 0.7 \cdot TB + 0.005 \cdot \alpha R$	TLA	506.45	°R			
Fully Insulated; $TLA = TB$	TLA	505.8	°R			
Average Vapor Temperature (Tv)						
Not Insulated; Eq. 1-33: $Tv = 0.7 \cdot TAA + 0.3 \cdot TB + 0.009 \cdot \alpha R$	Tv	506.89	°R			
Partially Insulated; Eq. 1-34: $Tv = 0.6 \cdot TAA + 0.4 \cdot TB + 0.01 \cdot \alpha R$	Tv	507.09	°R			
Fully Insulated; $Tv = TB$	Tv	505.82	°R			
Stock Vapor Density; Eq. 1-22: $Wv = (Mv/PVA) \cdot (R \cdot Tv)$						
Not Insulated	Wv	1.387E-03				
Partially Insulated	Wv	1.389E-03				
Fully Insulated	Wv	1.360E-03				

HAPS Speciation	lb/month	Vapor Weight Concentration	Vapor Mole Fraction
Total HAP Emissions =	1.660	Eq. 40-6 $ZVi = yiMi / MV$	Eq. 40-5 $yi = Pi / PVA$
Eq. 40-2 $L_{vi} = Z_i(L_i)$			
Individual HAPS	L_{vi} (lb/month)	M_i M_v Z_{vi}	P_i = P_{v,i}(X_i) P_{v,i} y_i
hexane	0.0000	86.18 130 0.00000	0.000000 0.039
benzene	0.0000	78.11 130 0.00000	0.000000 0.039
2,2,4 TMP	0.0000	114.23 130 0.00000	0.000000 0.039
toluene	0.0000	92.14 130 0.00000	0.000000 0.039
ethylbenzene	0.4856	106.17 130 0.29247	0.014158 0.039
xylene	1.1748	106.17 130 0.70753	0.034159 0.039
naphthalene	0.0000	128.17 130 0.00E+00	0.00E+00 0.039
cumene	0.0000	120.19 130 0.00E+00	0.00E+00 0.039

Individual HAPS	Z _i	M _i	M _v	X _i	A	B	C	P _{v,i}
hexane	0.00000	130	86.18	0.00000	6.878	1171.5	224.37	1.3394
benzene	0.00000	130	78.11	0.00000	6.906	1211	220.79	0.8010
2,2,4 TMP	0.00000	130	114.23	0.00000	6.812	1257.8	220.74	0.4018
toluene	0.00000	130	92.14	0.00000	7.017	1377.6	222.64	0.2164
ethylbenzene	0.26400	130	106.17	0.32326	6.95	1419.3	212.61	0.0643
xylene	0.73600	130	106.17	0.90120	7.009	1462.3	215.11	0.0558
naphthalene	0.00000	130	128.17	0.00000	7.146	1831.6	211.82	0.0013
cumene	0.00000	130	120.19	0.00000	6.929	1455.8	207.2	0.0286

Monthly Calculations (continued)

DECEMBER

Tank No.	13061A	Symbol	Units	ROUTINE EMISSIONS CALCULATIONS	Symbol	Units
ROUTINE EMISSIONS CALCULATIONS						
Total Losses (Eq. 1-1: $LT = LS+LW$)	LT	1.13	lb/month	Standing Losses; Eq. 1-2: $LS = 365 (Vv \cdot Wv \cdot KE \cdot Ks)$	LS	0.31 lb/month
		5.65E-04	ton/month	Vapor Space Volume	Vv	549.8 ft ³
				Stock Vapor Density	Wv	0.0010 lb/ft ³
				Vapor Space Expansion Factor ($0 < KE <= 1$); Eq. 1-5	KE	0.019 per day
Nearest US Location	Bridgeport, CT			Vented Vapor Saturation Factor	KS	1.00 NA
Daily total solar insolation on a horizontal surface; Table 7.1-7	I	501.0	Btu/ft ² -day	Constant; Number of Daily Events in a Year	365	31 days/month
Absolute Pressure	PA	14.69	psia	Working Losses; Eq. 1-35: $Lw = VQ \cdot KN \cdot Kp \cdot Wv \cdot KB$	Lw	0.82 lb/month
Ideal Gas Constant	R	10.73	psia ft ³ /lb-mole R	Net Working Loss Throughput (Eq. 1-39: $VQ=5.614 \cdot Q$)	VQ	855 ft ³ /month
Product Information				Working Loss Turnover Factor Eq. 1-35 $Kp=(180+N)/6N$ for N=36, else $Kp=1$	KN	1.0000
Product Type	Diesel Additive			Working Loss Product Factor	Kp	1.00
Vapor Molecular weight	Mv	130	Lb/lb-mole	Stock Vapor Density	Wv	0.0010 lb/ft ³
Average organic liquid density	WL	6.10	lb/gal	Vent Setting Correction Factor	KB	1.00
Average Reid Vapor Pressure	RVP	0.00	psi	Vented Vapor Saturation Factor; Eq. 1-21: $Ks = 1/(1+0.053 \cdot PVA/Hvo)$	Ks	1.00
Product factor; 0.4 for crude oils or 1 for other organic liquids	Kc	1.00		Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.0395 psia
Vapor Pressure Equation Constant A	A	0.00		Vapor Space Outage	Hvo	0.00 ft
Vapor Pressure Equation Constant B (Table 7.1-2)	B	0.0	R	Vapor Space Expansion Factor (Eq. 1-5: $(\Delta T/TLA) \cdot (\Delta Pv - \Delta PBI) / (PA - PVA)$)	KE	0.0187 per day
Tank design data				Average Daily Vapor Temperature Range	ΔT_v	11.33 °R
Shell height	Hs	7.85	ft	Average Daily Vapor Pressure Range	ΔP_v	0.00000 psia
Diameter	D	13.35	ft	Breather Vent Pressure Setting Range (Equation 1-10: $\Delta PBI = PBP - PBI$)	ΔPBI	0.0600 psi
Throughput	Q	6.400	gal/month	Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.0395 psia
Turnovers	N	9.16	per year	Average Daily Liquid Surface Temperature	TLA	496.35 °R
Roof type:		0.00		Atmospheric Pressure	PA	14.69 psia
Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft	Average Daily Vapor Temperature Range (ΔT_v)		
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA	ft	Average daily ambient temperature range - Equation 1-11 ($\Delta T_A = TAX - TAA$)	ΔT_A	12.6 °R
Maximum Filling Height - use (Pi/4)D if unknown	HLX	6.85	ft	Not Insulated - Equation 1-7 ($\Delta T_v = 0.7 \Delta T_A + 0.02 \alpha R$)	ΔT_v	11.33 °R
Minimum Filling Height (use 0 if unknown)	HLN	1.00	ft	Partially Insulated - Equation 1-8 ($\Delta T_v = 0.6 \Delta T_A + 0.02 \alpha R$)	ΔT_v	10.07 °R
Liquid height (assume 1/2 H)	HL	3.93	ft	Fully Insulated, constant temperature	ΔT_v	0.00 °R
Tank insulation (pick from drop down list)		Not Insulated		Average Daily Vapor Pressure Range (ΔP_v)		
Tank Construction (pick from drop down list)		Welded		Not Insulated - Equation 1-9: $\Delta P_v = PVX - PVN$	ΔP_v	0.00000 psia
Tank Shell Color (pick from drop down list)		White		Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25: $PVX = e^{PVA}$)	PVX	1.00000 psia
Tank Shell Condition (pick from drop down list)		Average		Vapor pressure at ave daily min liquid surface temp. (Eq. 1-25: $PVN = e^{PVA}$)	PVN	1.00000 psia
Tank Interior Condition (pick from drop down list)		Light Rust		Average daily max. liquid surface temp.; Fig. 7.1-17 $TLX = TLA + 0.25 \Delta T$	TLX	499.18 °R
Tank paint solar absorptance, dimensionless; Table 7.1-6	α	0.25		Average daily min. liquid surface temp.; Fig. 7.1-17 $TLN = TLA - 0.25 \Delta T$	TLN	493.52 °R
Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	-0.03	psi	Partially Insulated - Equation 1-9: $\Delta P_v = PVX - PVN$	ΔP_v	0.00000 psia
True Vapor Pressure; Eq. 1-25: $PVA = \exp(A - (B/TLA))$				Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25: PVX)	PVX	1.00000 psia
Not Insulated	PVA	0.0394603	psi	Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25: PVN)	PVN	1.000000 psia
Partially Insulated	PVA	0.0395187	psi	Average daily maximum liquid surface temperature, deg R ($TLX = TLA +$)	TLX	498.91 °R
Fully Insulated	PVA	0.0387265	psi	Average daily minimum liquid surface temperature, deg R ($TLN = TLA -$)	TLN	493.87 °R
Average Daily Ambient Temperature (TAA) Eq. 1-30 $TAA = ((TAX+TAN)/2)$	TAA	495.50	°R	Fully Insulated ($\Delta P_v = 0$)	ΔP_v	0.00 psia
Average daily maximum ambient temperature; Table 7.1-7	TAX	501.80	°R	Vapor Space Volume (Eq. 1-3: $Vv = ((PI/4) D^2 Hvo)$)	Vv	549.78 ft ³
Average daily minimum ambient temperature; Table 7.1-7	TAN	489.20	°R	Effective Tank diameter	De	13.35 ft
Liquid Bulk Temperature; Eq. 1-31: $TB = TAA + 0.003 \alpha s$	TB	495.88	°R	Effective Tank Height	He	7.85 ft
Average Daily Liquid Surface Temperature (TLA)				Vapor Space Outage Hvo = 1/2 H	Hvo	3.93 ft
Not Insulated; Eq. 1-28: $TLA = 0.4 \cdot TAA + 0.6 \cdot TB + 0.005 \cdot \alpha R$	TLA	496.35	°R			
Partially Insulated; Eq. 1-29: $TLA = 0.3 \cdot TAA + 0.7 \cdot TB + 0.005 \cdot \alpha R$	TLA	496.39	°R			
Fully Insulated; $TLA = TB$	TLA	495.9	°R			
Average Vapor Temperature (Tv)						
Not Insulated; Eq. 1-33: $Tv = 0.7 \cdot TAA + 0.3 \cdot TB + 0.009 \cdot \alpha R$	Tv	496.74	°R			
Partially Insulated; Eq. 1-34: $Tv = 0.6 \cdot TAA + 0.4 \cdot TB + 0.01 \cdot \alpha R$	Tv	496.90	°R			
Fully Insulated; $Tv = TB$	Tv	495.88	°R			
Stock Vapor Density; Eq. 1-22: $Wv = (Mv/PVA) \cdot (R \cdot Tv)$						
Not Insulated	Wv	9.624E-04				
Partially Insulated	Wv	9.635E-04				
Fully Insulated	Wv	9.461E-04				

HAPS Speciation	lb/month	Vapor Weight Concentration	Vapor Mole Fraction
Total HAP Emissions =	1.130	Eq. 40-6 $ZVi = yiMi / MV$	Eq. 40-5 $yi = Pi / PVA$
Eq. 40-2 $L_{vi} = Z_i(L_i)$			
Individual HAPS	L_{vi} (lb/month)	M_i M_v Z_{vi}</	

Monthly Calculations - JANUARY

Tank No.	13316A			ROUTINE EMISSIONS CALCULATIONS			Symbol			Units			ROUTINE EMISSIONS CALCULATIONS			Symbol			Units			HAPS Speciation			ib/month		
	ROUTINE EMISSIONS CALCULATIONS			Symbol	Units	ROUTINE EMISSIONS CALCULATIONS			Symbol	Units	HAPS Speciation			ib/month													
	Total Losses (Eq.1-1: LT = LS+LW)	LT	0.95	lb/month	Standing Losses; Eq.1-2: LS = 365 (Vv * Wv * KE * Ks)	LS	0.27	lb/month	Product																		
	Daily total solar insolation on a horizontal surface; Table 7.1-7	I	560.35	btu/ft ² -day	Vapor Space Volume	Vv	549.8	ft ³	Total HAP Emissions =	0.954	Vapor Weight Concentration	Eq. 40-6 Zvi = yMi / MV															
	Absolute Pressure	P	14.69	psi	Stock Vapor Density	Wv	0.0008	lb/ft ³	Eq. 40-2 Li = Zi(Li)		Vapor Mole Fraction	Eq. 40-5 yi = Pi / PVA															
	Ideal Gas Constant	R	10.73	psia ft ³ /lb-mole R	Vapor Space Expansion Factor (0 < KE <= 1); Eq. 1-5	KE	0.020	per day	Individual HAPS	Li (lb/month)	Mi	Mv	Zvi	Fi = Pvi(Xi)	Pvi	yi											
	Product Information				Working Losses; Eq.1-3: LW = VQ * KN * Kp * Wv * KB	LW	0.68	lb/month	hexane	0.0000	86.18	130	0.00000	0.000000	0.032	-											
	Product Type	Diesel Additive			Net Working Loss Throughput (Eq. 1-39: VQ=5.614*Q)	VQ	855	ft ³ /month	benzene	0.0000	78.11	130	0.00000	0.000000	0.032	-											
	Vapor Molecular weight	Mv	130	lb/lb-mole	Working Loss Turnover Factor Eq.1-35 Kp=(180+N)/6N for N>=36, else Kp=	KN	1.0000		2,2,4 TMP	0.0000	114.23	130	0.00000	0.000000	0.032	-											
	Average organic liquid density	WL	6.10	lb/gal	Stock Vapor Density	Wv	1.000	lb/ft ³	toluene	0.0000	92.14	130	0.00000	0.000000	0.032	-											
	Average Reid Vapor Pressure	RVP	0.00	psi	Vent Settling Correction Factor	KB	1.00		ethylbenzene	0.2798	106.17	130	0.29329	0.011655	0.032	0.35912											
	Product factor: 0.4 for crude oils or 1 for other organic liquids	Kc	1.00		Vented Vapor Saturation Factor; Eq. 1-21: Ks = 1/(1+(0.053*Pv^{0.7}/Hvo))	Ks	1.00		xylenes	0.6742	106.17	130	0.70671	0.028084	0.032	0.86533											
	Vapor Pressure Equation Constant A	A	0.00		Vapor Pressure at Avg Daily Liq Surface Temp	PvA	0.0325	psia	naphthalene	0.0000	128.17	130	0.00E+00	0.00E+00	0.032	0.00E+00											
	Vapor Pressure Equation Constant B (Table 7.1-2)	B	0.0	R	Vapor Space Outage	Hvo	0.00	ft	cumene	0.0000	120.19	130	0.00E+00	0.00E+00	0.032	0.00E+00											
	Tank design data				Vapor Space Expansion Factor (Eq. 1-5: (ΔTV/TLA)+(ΔPv-ΔPB)/(PA-PvA))	KE	0.0198	per day	Liquid Mole Fraction	Eq. 40-4 xi = (ZiMLi)/M	Zi	Mi	Mv	Xi	Component Vapor Pressure			PVAi=(0.019373)PVA-B(TLA+C)									
	Shell height	Hs	7.85	ft	Average Daily Vapor Temperature Range	ΔTv	11.76	R	hexane	0.00000	130	86.18	0.00000	6.878	1171.5	224.37	0.8715										
	Diameter	D	13.35	ft	Stock Vapor Density	Wv	0.0009	lb/ft ³	benzene	0.00000	130	78.11	0.00000	6.906	1211	220.79	0.5064										
	Throughput	Q	6.400	gal/month	Average Daily Vapor Pressure Range	ΔPv	0.0000	psi	2,2,4 TMP	0.00000	130	114.23	0.00000	6.812	1257.8	220.74	0.2495										
	Turnovers	N	9.16	per year	Breather Vent Pressure Setting Range (Equation 1-10: ΔPB = PBP - PBV)	ΔPB	0.0600	psi	toluene	0.00000	130	92.14	0.00000	7.017	1377.6	222.64	0.1296										
	Roof Type:		0.00		Vapor Pressure at Avg Daily Liq Surface Temp	PvA	0.0325	psia	ethylbenzene	0.26400	130	106.17	0.32326	6.95	1419.3	212.61	0.0361										
	Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft	Average Daily Liquid Surface Temperature	TLA	491.45	R	xylenes	0.73600	130	106.17	0.90120	7.009	1462.3	215.11	0.0312										
	Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA	ft	Atmospheric Pressure	PA	14.69	psia	naphthalene	0.00000	130	128.17	0.00000	7.146	1831.6	211.82	0.0006										
	Maximum Filling Height -use (Pi/4)D if unknown	HLX	6.85	ft	Average Daily Vapor Temperature Range (ΔTv)				cumene	0.00000	130	120.19	0.00000	6.929	1455.8	207.2	0.0153										
	Minimum Filling Height (use 0 if unknown)	HLN	1.00	ft	Average daily ambient temperature range - Equation 1-11 (ΔTA=TAX-TA)	ΔTA	12.8	R																			
	Liquid height (assume 1/2 H)	HL	3.93	ft	Not Insulated - Equation 1-7 (ΔTV = 0.7 ΔTA + 0.02 α I)	ΔTV	11.76	R																			
	Tank Insulation (pick from drop down list)		Not Insulated		Partially Insulated - Equation 1-8 (ΔTV = 0.6 ΔTA + 0.02 α R I)	ΔTV	10.48	R																			
	Tank Construction (pick from drop down list)		Welded		Fully Insulated, constant temperature	ΔTV	0.00	R																			
	Tank Shell Color (pick from drop down list)		White		Average Daily Vapor Pressure Range (ΔPv)																						
	Tank Shell Condition (pick from drop down list)		Average		Not Insulated - Equation 1-9: ΔPv = PvX - Pvn	ΔPv	0.00000	psia																			
	Tank Interior Condition (pick from drop down list)		Light Rust		Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25 PvX = e ^{ΔPv})	PvX	1.00000	psia																			
	Tank paint solar absorptance, dimensionless; Table 7.1-6	α	0.25		Vapor pressure at ave daily min liquid surface temp. (Eq. 1-25 Pvn = e ^{ΔPv})	Pvn	1.00000	psia																			
	Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	-0.03	psi	Average daily max. liquid surface temp.; Fig. 7.1-17 TLX = TLA + 0.25ΔT	TLX	494.39	R																			
	True Vapor Pressure; Eq. 1-25, PvA = exp(A-(B/TLA))				Average daily min. liquid surface temp.; Fig. 7.1-17 TLN = TLA - 0.25ΔT	TLN	488.51	R																			
	Not Insulated	PvA	0.032455		Partially Insulated - Equation 1-9: ΔPv = PvX - Pvn	ΔPv	0.00000	psia																			
	Partially Insulated	PvA	0.0325101		Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25 u ^{PvX})	PvX	1.00000	psia																			
	Fully Insulated	PvA	0.031764		Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25 u ^{Pvn})	Pvn	1.000000	psia																			
	Average Daily Ambient Temperature (TAA) Eq. 1-30 TAA = ((TAX+TAN)/2)	TAA	490.50	R	Fully Insulated (ΔPv = 0)	ΔPv	0.00	psia																			
	Average daily maximum ambient temperature; Table 7.1-7	TAX	496.90	R	Vapor Space Volume (Eq.1-3: Vv = (Pi/4) D²Hvo)	Vv	549.78	ft ³																			
	Average daily minimum ambient temperature; Table 7.1-7	TAN	484.10	R	Effective Tank diameter	D _e	13.35	ft																			
	Liquid Bulk Temperature; Eq.1-31: TB = TAA + 0.003 α I	TB	490.92	R	Effective Tank Height	H _e	7.85	ft																			
	Average Daily Liquid Surface Temperature (TLA)				Vapor Space Outage Hvo = 1/2 H	Hvo	3.93	ft																			
	Not Insulated; Eq. 1-28, TLA = 0.4*TAA + 0.6*TB + 0.005*α*I	TLA	491.45	R																							
	Partially Insulated; Eq. 1-29, TLA = 0.3*TAA + 0.7*TB + 0.005*α*R	TLA	491.49	R																							
	Fully Insulated; TLA = TB	TLA	490.9	R																							
	Average Vapor Temperature (Tv)																										
	Not Insulated; Eq. 1-33, Tv = 0.7*TAA + 0.3*TB + 0.009*α*I	Tv	491.89	R																							
	Partially Insulated; Eq. 1-34, Tv = 0.6*TAA + 0.4*TB + 0.01*α*R	Tv	492.07	R																							
	Fully Insulated; Tv = TB	Tv	490.92	R																							
	Stock Vapor Density; Eq. 1-22, Wv = (Mv*PVA)/(R*TV)																										
	Not Insulated	Wv	7.993E-04																								
	Partially Insulated	Wv	8.004E-04																								
	Fully Insulated	Wv	7.838E-04																								

Monthly Calculations (continued)

Tank No.	13316A			ROUTINE EMISSIONS CALCULATIONS			Symbol			Units			ROUTINE EMISSIONS CALCULATIONS			Symbol			Units			HAPS Speciation			ib/month		
	ROUTINE EMISSIONS CALCULATIONS			Symbol	Units	ROUTINE EMISSIONS CALCULATIONS			Symbol	Units	HAPS Speciation			ib/month													
	Total Losses (Eq.1-1: LT = LS+LW)	LT	1.05	lb/month	Standing Losses; Eq.1-2: LS = 365 (Vv * Wv * KE * Ks)	LS	0.31	lb/month	Product																		
	Daily total solar insolation on a horizontal surface; Table 7.1-7	I	847.0	btu/ft ² -day	Vapor Space Volume	Vv	549.8	ft ³	Total HAP Emissions =	1.053	Vapor Weight Concentration	Eq. 40-6 Zvi = yMi / MV															
	Absolute Pressure	P	14.69	psi	Stock Vapor Density	Wv	0.0009	lb/ft ³	Eq. 40-2 Li = Zi(Li)		Vapor Mole Fraction	Eq. 40-5 yi = Pi / PVA															
	Ideal Gas Constant	R	10.73	psia ft ³ /lb-mole R	Vapor Space Expansion Factor (0 < KE <= 1); Eq. 1-5	KE	0.023	per day	Individual HAPS	Li (lb/month)	Mi	Mv	Zvi	Fi = Pvi(Xi)	Pvi	yi											
	Product Information				Working Losses; Eq.1-3: LW = VQ * KN * Kp * Wv * KB	LW	0.74	lb/month	hexane	0.0000	86.18	130	0.00000	0.000000	0.035	-											
	Product Type	Diesel Additive			Net Working Loss Throughput (Eq. 1-39: VQ=5.614*Q)	VQ	855	ft ³ /month	benzene	0.0000	78.11	130	0.00000	0.000000	0.035	-											
	Vapor Molecular weight	Mv	130	lb/lb-mole	Working Loss Turnover Factor Eq.1-3																						

Monthly Calculations (continued)

MARCH

Tank No.	13316A	Symbol	Units	ROUTINE EMISSIONS CALCULATIONS	Symbol	Units
ROUTINE EMISSIONS CALCULATIONS						
Total Losses (Eq. 1-1: $LT = LS + LW$)	LT	1.50	lb/month	Standing Losses; Eq. 1-2: $LS = 365 (Vv \cdot Wv \cdot KE \cdot Ks)$	LS	0.53 lb/month
Nearest US Location	Bridgeport, CT			Vapor Space Volume	Vv	549.8 ft ³
Daily total solar insolation on a horizontal surface; Table 7.1-7	I	1156.0	Btu/ft ² ·day	Stock Vapor Density	Wv	0.0011 lb/ft ³
Absolute Pressure	Pa	14.69	psia	Vapor Space Expansion Factor ($0 < KE \leq 1$); Eq. 1-5	KE	0.027 per day
Ideal Gas Constant	R	10.73	psia ft ³ /lb-mole R	Vented Vapor Saturation Factor	Ks	1.00 NA
Product Information				Constant, Number of Daily Events in a Year	365	31 days/month
Product Type	Diesel Additive			Working Losses; Eq. 1-35: $Lw = VQ \cdot KN \cdot Kp \cdot Wv \cdot KB$	Lw	0.97 lb/month
Vapor Molecular weight	Mv	130	lb/lb-mole	Net Working Loss Throughput (Eq. 1-39: $VQ = 5.614 \cdot Q$)	VQ	855 ft ³ /month
Average organic liquid density	WL	6.10	lb/gal	Working Loss Turnover Factor Eq. 1-35 $Ks = (180 + N)/6N$ for $N > 36$, else $Ks = 1$	KN	1.0000
Average Reid Vapor Pressure	RVP	0.00	psia	Working Loss Product Factor	Kp	1.00
Product factor, 0.4 for crude oils or 1 for other organic liquids	Kc	1.00		Stock Vapor Density	Wv	0.0011 lb/ft ³
Vapor Pressure Equation Constant A	A	0.00		Vent Setting Correction Factor	KB	1.00
Vapor Pressure Equation Constant B (Table 7.1-2)	B	0.0	R	Vented Vapor Saturation Factor; Eq. 1-21: $Ks = 1/(1 + 0.053 \cdot PVA \cdot Hvo)$	Ks	1.00
Tank design data				Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.0470 psia
Shell height	Hs	7.85	ft	Vapor Space Outage	Hvo	0.00 ft
Diameter	D	13.35	ft	Vapor Space Expansion Factor (Eq. 1-5: $(\Delta Tv/TLA) + (\Delta Pv - \Delta PB)/(PA - PVA)$)	KE	0.0273 per day
Throughput	Q	6.400	gal/month	Average Daily Vapor Temperature Range	ΔTv	15.72 °R
Turnovers	N	9.16	per year	Average Daily Vapor Pressure Range	ΔPv	0.0000 psia
Roof Type:				Breather Vent Pressure Setting Range (Equation 1-10: $\Delta PB = PBP - PBV$)	ΔPB	0.0600 psi
Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft	Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.0470 psia
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA	ft	Average Daily Liquid Surface Temperature	TLA	500.87 °R
Maximum Filling Height - use (Pi/4)D if unknown	HLX	6.85	ft	Atmospheric Pressure	PA	14.69 psia
Minimum Filling Height (use 0 if unknown)	HLN	1.00	ft	Average Daily Vapor Temperature Range (ΔTv)	ΔTv	14.2 °R
Liquid height (assume 1/2 H)	HL	3.93	ft	Average daily ambient temperature range - Equation 1-11 ($\Delta TA = TAX - TA$)	ΔTA	14.2 °R
Tank insulation (pick from drop down list)	Not Insulated			Not Insulated - Equation 1-7 ($\Delta Tv = 0.7 \Delta TA + 0.02 \text{ or } 1$)	ΔTv	15.72 °R
Tank Construction (pick from drop down list)	Welded			Partially Insulated - Equation 1-8 ($\Delta Tv = 0.6 \Delta TA + 0.02 \text{ or } 1$)	ΔTv	14.30 °R
Tank Shell Color (pick from drop down list)	White			Fully Insulated, constant temperature	ΔTv	0.00 °R
Tank Shell Condition (pick from drop down list)	Average			Average Daily Vapor Pressure Range (ΔPv)	ΔPv	0.0000 psia
Tank Interior Condition (pick from drop down list)	Light Rust			Not Insulated - Equation 1-9: $\Delta Pv = PVX - PVN$	ΔPv	0.0000 psia
Tank paint solar absorptance, dimensionless; Table 7.1-6	α	0.25		Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25: $PvX = \text{exp}(A - (B/TLX))$)	PvX	1.00000 psia
Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	0.03	psi	Vapor pressure at ave. daily min liquid surface temp. (Eq. 1-25: $PvN = \text{exp}(A - (B/TLN))$)	PvN	1.00000 psia
True Vapor Pressure; Eq. 1-25: $PvA = \text{exp}(A - (B/TLA))$				Average daily max. liquid surface temp.; Fig. 7.1-17 $TLX = TLA + 0.25 \Delta Tv$	TLX	504.80 °R
Not Insulated	PvA	0.047042	psia	Average daily min. liquid surface temp.; Fig. 7.1-17 $TLN = TLA - 0.25 \Delta Tv$	TLN	496.94 °R
Partially Insulated	PvA	0.0471992	psia	Partially Insulated - Equation 1-9: $\Delta Pv = PVX - PVN$	ΔPv	0.00000 psia
Fully Insulated	PvA	0.0450895	psia	Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25: PvX)	PvX	1.00000 psia
Average Daily Ambient Temperature (TAA) Eq. 1-30 $TAA = ((TAX + TA)/2)$	TAA	498.90	°R	Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25: PvN)	PvN	1.0000000 psia
Average daily maximum ambient temperature; Table 7.1-7	TAX	506.00	°R	Average daily maximum liquid surface temperature, deg R ($TLX = TLA + \Delta Tv$)	TLX	504.53 °R
Average daily minimum ambient temperature; Table 7.1-7	TAN	491.80	°R	Average daily minimum liquid surface temperature, deg R ($TLN = TLA - \Delta Tv$)	TLN	497.36 °R
Liquid Bulk Temperature; Eq. 1-31: $TB = TAA + 0.003 \text{ or } 1$	TB	499.77	°R	Fully Insulated ($\Delta Pv = 0$)	ΔPv	0.00 psia
Average Daily Liquid Surface Temperature (TLA)				Vapor Space Volume (Eq. 1-3: $Vv = (PI/4) D^2 Hvo$)	Vv	549.78 ft ³
Not Insulated; Eq. 1-28: $TLA = 0.4 \cdot TAA + 0.6 \cdot TB + 0.005 \cdot \alpha \cdot I$	TLA	500.87	°R	Effective Tank diameter	D _e	13.35 ft
Partially Insulated; Eq. 1-29: $TLA = 0.3 \cdot TAA + 0.7 \cdot TB + 0.005 \cdot \alpha \cdot R$	TLA	500.95	°R	Effective Tank Height	H _e	7.85 ft
Fully Insulated: $TLA = TB$	TLA	499.8	°R	Vapor Space Outage $Hvo = 1/2 H$	Hvo	3.93 ft
Average Vapor Temperature (Tv)						
Not Insulated; Eq. 1-33: $Tv = 0.7 \cdot TAA + 0.3 \cdot TB + 0.009 \cdot \alpha \cdot I$	Tv	501.76	°R			
Partially Insulated; Eq. 1-34: $Tv = 0.6 \cdot TAA + 0.4 \cdot TB + 0.01 \cdot \alpha \cdot R$	Tv	502.14	°R			
Fully Insulated; $Tv = TB$	Tv	499.77	°R			
Stock Vapor Density; Eq. 1-22: $Wv = (Mv \cdot PvA)/(R \cdot Tv)$						
Not Insulated	Wv	1.136E-03				
Partially Insulated	Wv	1.139E-03				
Fully Insulated	Wv	1.093E-03				

HAPS Speciation	lb/month	Vapor Weight Concentration	Vapor Mole Fraction
Product	additive		
Total HAP Emissions = Eq. 40-2: $L_{ij} = Z_{ij}(L_{ij})$	1.500	Eq. 40-6 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$
Individual HAPS	L_{ij} (lb/month)	M_i	M_v
hexane	0.0000	86.18	130
benzene	0.0000	78.11	130
2,2,4 TMP	0.0000	114.23	130
toluene	0.0000	92.14	130
ethylbenzene	0.4391	106.17	130
xylene	1.0607	106.17	130
naphthalene	0.0000	128.17	130
cumene	0.0000	120.19	130

Monthly Calculations (continued)

APRIL

Tank No.	13316A	Symbol	Units	ROUTINE EMISSIONS CALCULATIONS	Symbol	Units
ROUTINE EMISSIONS CALCULATIONS						
Total Losses (Eq. 1-1: $LT = LS + LW$)	LT	2.29	lb/month	Standing Losses; Eq. 1-2: $LS = 365 (Vv \cdot Wv \cdot KE \cdot Ks)$	LS	0.86 lb/month
Nearest US Location	Bridgeport, CT			Vapor Space Volume	Vv	549.8 ft ³
Daily total solar insolation on a horizontal surface; Table 7.1-7	I	1490.0	Btu/ft ² ·day	Stock Vapor Density	Wv	0.0017 lb/ft ³
Absolute Pressure	Pa	14.69	psia	Vapor Space Expansion Factor ($0 < KE \leq 1$); Eq. 1-5	KE	0.031 per day
Ideal Gas Constant	R	10.73	psia ft ³ /lb-mole R	Vented Vapor Saturation Factor	Ks	1.00 NA
Product Information				Constant, Number of Daily Events in a Year	365	30 days/month
Product Type	Diesel Additive			Working Losses; Eq. 1-35: $Lw = VQ \cdot KN \cdot Kp \cdot Wv \cdot KB$	Lw	1.43 lb/month
Vapor Molecular weight	Mv	130	lb/lb-mole	Net Working Loss Throughput (Eq. 1-39: $VQ = 5.614 \cdot Q$)	VQ	855 ft ³ /month
Average organic liquid density	WL	6.10	lb/gal	Working Loss Turnover Factor Eq. 1-35 $Ks = (180 + N)/6N$ for $N > 36$, else $Ks = 1$	KN	1.0000
Average Reid Vapor Pressure	RVP	0.00	psia	Working Loss Product Factor	Kp	1.00
Product factor, 0.4 for crude oils or 1 for other organic liquids	Kc	1.00		Stock Vapor Density	Wv	0.0017 lb/ft ³
Vapor Pressure Equation Constant A	A	0.00		Vent Setting Correction Factor	KB	1.00
Vapor Pressure Equation Constant B (Table 7.1-2)	B	0.0	R	Vented Vapor Saturation Factor; Eq. 1-21: $Ks = 1/(1 + 0.053 \cdot PVA \cdot Hvo)$	Ks	1.00
Tank design data				Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.0706 psia
Shell height	Hs	7.85	ft	Vapor Space Outage	Hvo	0.00 ft
Diameter	D	13.35	ft	Vapor Space Expansion Factor (Eq. 1-5: $(\Delta Tv/TLA) + (\Delta Pv - \Delta PB)/(PA - PVA)$)	KE	0.0314 per day
Throughput	Q	6.400	gal/month	Average Daily Vapor Temperature Range	ΔTv	18.16 °R
Turnovers	N	9.47	per year	Average Daily Vapor Pressure Range	ΔPv	0.0000 psia
Roof Type:				Breather Vent Pressure Setting Range (Equation 1-10: $\Delta PB = PBP - PBV$)	ΔPB	0.0600 psi
Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft	Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.0706 psia
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA	ft	Average Daily Liquid Surface Temperature	TLA	511.68 °R
Maximum Filling Height - use (Pi/4)D if unknown	HLX	6.85	ft	Atmospheric Pressure	PA	14.69 psia
Minimum Filling Height (use 0 if unknown)	HLN	1.00	ft	Average Daily Vapor Temperature Range (ΔTv)	ΔTv	15.3 °R
Liquid height (assume 1/2 H)	HL	3.93	ft	Average daily ambient temperature range - Equation 1-11 ($\Delta TA = TAX - TA$)	ΔTA	15.3 °R
Tank insulation (pick from drop down list)	Not Insulated			Not Insulated - Equation 1-7 ($\Delta Tv = 0.7 \Delta TA + 0.02 \text{ or } 1$)	ΔTv	18.16 °R
Tank Construction (pick from drop down list)	Welded			Partially Insulated - Equation 1-8 ($\Delta Tv = 0.6 \Delta TA + 0.02 \text{ or } 1$)	ΔTv	16.63 °R
Tank Shell Color (pick from drop down list)	White			Fully Insulated, constant temperature	ΔTv	0.00 °R
Tank Shell Condition (pick from drop down list)	Average			Average Daily Vapor Pressure Range (ΔPv)	ΔPv	0.00000 psia
Tank Interior Condition (pick from drop down list)	Light Rust			Not Insulated - Equation 1-9: $\Delta Pv = PVX - PVN$	ΔPv	0.00000 psia
Tank paint solar absorptance, dimensionless; Table 7.1-6	α	0.25		Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25: $PvX = \text{exp}(A - (B/TLX))$)	PvX	1.00000 psia
Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	0.03	psi	Vapor pressure at ave. daily min liquid surface temp. (Eq. 1-25: $PvN = \text{exp}(A - (B/TLN))$)	PvN	1.00000 psia
True Vapor Pressure; Eq. 1-25: $PvA = \text{exp}(A - (B/TLA))$				Average daily max. liquid surface temp.; Fig. 7.1-17 $TLX = TLA + 0.25 \Delta Tv$	TLX	516.22 °R
Not Insulated	PvA	0.0705523	psia	Average daily min. liquid surface temp.; Fig. 7.1-17 $TLN = TLA - 0.25 \Delta Tv$	TLN	507.14 °R
Partially Insulated	PvA	0.0708403	psia	Partially Insulated - Equation 1-9: $\Delta Pv = PVX - PVN$	ΔPv	0.00000 psia
Fully Insulated	PvA	0.0669906	psia	Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25: PvX)	PvX	1.00000 psia
Average Daily Ambient Temperature (TAA) Eq. 1-30 $TAA = ((TAX + TA)/2)$	TAA	509.15	°R	Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25: PvN)	PvN	1.0000000 psia
Average daily maximum ambient temperature; Table 7.1-7	TAX	516.80	°R	Average daily maximum liquid surface temperature, deg R ($TLX = TLA + \Delta Tv$)	TLX	515.95 °R
Average daily minimum ambient temperature; Table 7.1-7	TAN	501.50	°R	Average daily minimum liquid surface temperature, deg R ($TLN = TLA - \Delta Tv$)	TLN	507.64 °R
Liquid Bulk Temperature; Eq. 1-31: $TB = TAA + 0.003 \text{ or } 1$	TB	510.27	°R	Fully Insulated ($\Delta Pv = 0$)	ΔPv	0.00 psia
Average Daily Liquid Surface Temperature (TLA)				Vapor Space Volume (Eq. 1-3: $Vv = (PI/4) D^2 Hvo$)	Vv	549.78 ft ³
Not Insulated; Eq. 1-28: $TLA = 0.4 \cdot TAA + 0.6 \cdot TB + 0.005 \cdot \alpha \cdot I$	TLA	511.68	°R	Effective Tank diameter	D _e	13.35 ft
Partially Insulated; Eq. 1-29: $TLA = 0.3 \cdot TAA + 0.7 \cdot TB + 0.005 \cdot \alpha \cdot R$	TLA	511.79	°R	Effective Tank Height	H _e	7.85 ft
Fully Insulated: $TLA = TB$	TLA	510.3	°R	Vapor Space Outage $Hvo = 1/2 H$	Hvo	3.93 ft
Average Vapor Temperature (Tv)						
Not Insulated; Eq. 1-33: $Tv = 0.7 \cdot TAA + 0.3 \cdot TB + 0.009 \cdot \alpha \cdot I$	Tv	512.84	°R			
Partially Insulated; Eq. 1-34: $Tv = 0.6 \cdot TAA + 0.4 \cdot TB + 0.01 \cdot \alpha \cdot R$	Tv	513.32	°R			
Fully Insulated; $Tv = TB$	Tv	510.27	°R			
Stock Vapor Density; Eq. 1-22: $Wv = (Mv \cdot PvA)/(R \cdot Tv)$						
Not Insulated	Wv	1.667E-03				
Partially Insulated	Wv	1.672E-03				
Fully Insulated	Wv	1.590E-03				

HAPS Speciation	lb/month	Vapor Weight Concentration	Vapor Mole Fraction
Product	additive		
Total HAP Emissions = Eq. 40-2: $L_{ij} = Z_{ij}(L_{ij})$	2.288	Eq. 40-6 $Z_{vi} = y_i M_i / M_v$	Eq. 40-5 $y_i = P_i / PVA$
Individual HAPS	L_{ij} (lb/month)	M_i	M_v
hexane	0.0000	86.18	130
benzene	0.0000	78.11	130
2,2,4 TMP	0.0000	114.23	130
toluene	0.0000	92.14	130
ethylbenzene	0.6686	106.17	130
xylene	1.6199	106.17	130
naphthalene	0.0000	128.17	130
cumene	0.0000	120.19	130

Monthly Calculations (continued)

MAY

Tank No.	13316A	Symbol	Units	ROUTINE EMISSIONS CALCULATIONS	Symbol	Units
ROUTINE EMISSIONS CALCULATIONS						
Total Losses (Eq. 1-1: LT = LS+LW)	LT	3.33	lb/month	Standing Losses; Eq. 1-2: LS = 365 (Vv * Wv * KE * Ks)	LS	1.34 lb/month
		1.67E-03	ton/month	Vapor Space Volume	Vv	549.8 ft ³
				Stock Vapor Density	Wv	0.0023 lb/ft ³
				Vapor Space Expansion Factor (0 < KE <= 1); Eq. 1-5	KE	0.034 per day
				Vented Vapor Saturation Factor	Ks	1.00 NA
				Constant, Number of Daily Events in a Year	365	31 days/month
Nearest US Location	Bridgeport, CT			Working Losses; Eq. 1-35: LW = VQ * KN * Kp * Wv * KB	Lw	1.99 lb/month
Daily total solar insolation on a horizontal surface; Table 7.1-7	I	1750.0	Btu/ft ² -day	Net Working Loss Throughput (Eq. 1-39: VQ=5.614*Q)	VQ	855 lb/month
Absolute Pressure	Pa	14.69	psia	Working Loss Turnover Factor Eq. 1-35: KN=(180+N)/6N for N>=36, else KN=1	KN	1.0000
Ideal Gas Constant	R	10.73	psia ft ³ /lb-mole R	Working Loss Product Factor	Kp	1.00
Product Information						
Product Type	Diesel Additive			Stock Vapor Density	Wv	0.0023 lb/ft ³
Vapor Molecular weight	Mv	130	lb/lb-mole	Vent Setting Correction Factor	Kb	1.00
Average organic liquid density	WL	6.10	lb/gal	Vented Vapor Saturation Factor; Eq. 1-21: Ks = 1/(1+0.053*PvA*Hvo)	Ks	1.00
Average Reid Vapor Pressure	RVP	0.00		Vapor Pressure at Avg Daily Liq Surface Temp	PvA	0.1005 psia
Product factor: 0.4 for crude oils or 1 for other organic liquids	Kc	1.00		Vapor Space Outage	Hvo	0.00 ft
Vapor Pressure Equation Constant A	A	0.00		Vapor Space Expansion Factor (Eq. 1-5: (ΔTv/TLA)+(ΔPv-ΔPB)/(PA-PvA))	KE	0.0337 per day
Vapor Pressure Equation Constant B (Table 7.1-2)	B	0.0	R	Average Daily Vapor Temperature Range	ΔTv	19.74 °R
Tank design data						
Shell height	Hs	7.85	ft	Average Daily Vapor Pressure Range	ΔPv	0.0000 psi
Diameter	D	13.35	ft	Partially Insulated - Equation 1-8 (ΔTv = 0.6 ΔTA + 0.02 or I)	ΔTv	18.17 °R
Throughput	Q	6.400	gal/month	Fully Insulated, constant temperature	ΔTv	0.00 °R
Turnovers	N	9.16	per year	Average Daily Vapor Pressure Range (ΔPv)	ΔPv	0.00000 psia
Roof Type:		0.00		Not Insulated - Equation 1-9: ΔPv = PvX - Pvn	ΔPv	0.00000 psia
Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft	Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25: PvX = exPvN)	PvX	1.00000 psia
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA	ft	Vapor pressure at ave daily min liquid surface temp. (Eq. 1-25: Pvn = exPvn)	Pvn	1.00000 psia
Maximum Filling Height -use (Pi/4)D if unknown	HLX	6.85	ft	Average daily max. liquid surface temp.; Fig. 7.1-17 TLX = TLA + 0.25ΔTv	TLX	526.56 °R
Minimum Filling Height (use 0 if unknown)	HLN	1.00	ft	Average daily min. liquid surface temp.; Fig. 7.1-17 TLN = TLA - 0.25ΔTv	TLN	516.69 °R
Liquid height (assume 1/2 H)	HL	3.93	ft	Average Daily Ambient Temperature (TAA) Eq. 1-30 TAA = ((TAX+TAN)/2)		
Tank insulation (pick from drop down list)	Q	Not Insulated		Average daily maximum ambient temperature, Table 7.1-7		
Tank Construction (pick from drop down list)		Welded		Average daily minimum ambient temperature, Table 7.1-7		
Tank Shell Color (pick from drop down list)		White		Liquid Bulk Temperature; Eq. 1-31: TB = TAA + 0.003 or I		
Tank Shell Condition (pick from drop down list)		Average		Average Daily Liquid Surface Temperature (TLA)		
Tank Interior Condition (pick from drop down list)		Light Rust		Not Insulated; Eq. 1-28: TLA = 0.4*TAA + 0.6*TB + 0.005*oI		
Tank paint solar absorptance, dimensionless, Table 7.1-6	α	0.25		Partially Insulated; Eq. 1-29: TLA = 0.3*TAA + 0.7*TB + 0.005*oR		
Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	0.03	psia	Fully Insulated; TLA = TB		
True Vapor Pressure; Eq. 1-25: PvA = exp(A/(B-TLA))						
Not Insulated	PvA	0.1005102		Average Vapor Temperature (Tv)		
Partially Insulated	PvA	0.1009694		Not Insulated; Eq. 1-33: Tv = 0.7*TAA + 0.3*TB + 0.009*oI		
Fully Insulated	PvA	0.0948467		Partially Insulated; Eq. 1-34: Tv = 0.6*TAA + 0.4*TB + 0.01*oR		
Average Daily Ambient Temperature (TAA) Eq. 1-30 TAA = ((TAX+TAN)/2)						
Average daily maximum ambient temperature, Table 7.1-7	TAX	526.50	°R	Fully Insulated; Tv = TB		
Average daily minimum ambient temperature, Table 7.1-7	TAN	510.80	°R	Stock Vapor Density; Eq. 1-22: Wv = (Mv/PvA)/(R*Tv)		
Liquid Bulk Temperature; Eq. 1-31: TB = TAA + 0.003 or I						
Fully Insulated (ΔPv = 0) ΔPv = 0.00 psia						
Average Daily Liquid Surface Temperature (TLA)						
Not Insulated; Eq. 1-28: TLA = 0.4*TAA + 0.6*TB + 0.005*oI						
Partially Insulated; Eq. 1-29: TLA = 0.3*TAA + 0.7*TB + 0.005*oR						
Fully Insulated; TLA = TB						
Average Vapor Temperature (Tv)						
Not Insulated; Eq. 1-33: Tv = 0.7*TAA + 0.3*TB + 0.009*oI						
Partially Insulated; Eq. 1-34: Tv = 0.6*TAA + 0.4*TB + 0.01*oR						
Fully Insulated; Tv = TB						
Stock Vapor Density; Eq. 1-22: Wv = (Mv/PvA)/(R*Tv)						
Not Insulated Wv = 2.328E-03						
Partially Insulated Wv = 2.336E-03						
Fully Insulated Wv = 2.210E-03						

HAPS Speciation	lb/month	Vapor Weight Concentration	Vapor Mole Fraction
Total HAP Emissions	3.330	Eq. 40-6 Zvi = yMi / MV	Eq. 40-5 yi = Pi / PvA
Individual HAPS			
hexane	0.0000	86.18	0.00000
benzene	0.0000	78.11	0.00000
2,2,4 TMP	0.0000	114.23	0.00000
toluene	0.0000	92.14	0.00000
ethylbenzene	0.9710	106.17	0.29159
xylene	2.3591	106.17	0.70841
naphthalene	0.0000	128.17	0.00E+00
cumene	0.0000	120.19	0.00E+00

Component Vapor Pressure	PvA=(0.0193737)10 ^{(A-B/(TLA-C))}	A	B	C	PvA
hexane	0.00000	130	86.18	0.00000	6.878
benzene	0.00000	130	78.11	0.00000	6.906
2,2,4 TMP	0.00000	130	114.23	0.00000	6.812
toluene	0.00000	130	92.14	0.00000	7.017
ethylbenzene	0.26400	130	106.17	0.32326	6.95
xylene	0.73600	130	106.17	0.9120	7.009
naphthalene	0.00000	130	128.17	0.00000	7.146
cumene	0.00000	130	120.19	0.00000	6.929

Monthly Calculations (continued)

JUNE

Tank No.	13316A	Symbol	Units	ROUTINE EMISSIONS CALCULATIONS	Symbol	Units
ROUTINE EMISSIONS CALCULATIONS						
Total Losses (Eq. 1-1: LT = LS+LW)	LT	4.52	lb/month	Standing Losses; Eq. 1-2: LS = 365 (Vv * Wv * KE * Ks)	LS	1.76 lb/month
		2.26E-03	ton/month	Vapor Space Volume	Vv	549.8 ft ³
				Stock Vapor Density	Wv	0.0032 lb/ft ³
				Vapor Space Expansion Factor (0 < KE <= 1); Eq. 1-5	KE	0.033 per day
				Vented Vapor Saturation Factor	Ks	1.00 NA
				Constant, Number of Daily Events in a Year	365	30 days/month
Nearest US Location	Bridgeport, CT			Working Losses; Eq. 1-35: LW = VQ * KN * Kp * Wv * KB	Lw	2.76 lb/month
Daily total solar insolation on a horizontal surface; Table 7.1-7	I	1862.0	Btu/ft ² -day	Net Working Loss Throughput (Eq. 1-39: VQ=5.614*Q)	VQ	855 lb/month
Absolute Pressure	Pa	14.69	psia	Working Loss Turnover Factor Eq. 1-35: KN=(180+N)/6N for N>=36, else KN=1	KN	1.0000
Ideal Gas Constant	R	10.73	psia ft ³ /lb-mole R	Working Loss Product Factor	Kp	1.00
Product Information						
Product Type	Diesel Additive			Stock Vapor Density	Wv	0.0032 lb/ft ³
Vapor Molecular weight	Mv	130	lb/lb-mole	Vent Setting Correction Factor	Kb	1.00
Average organic liquid density	WL	6.10	lb/gal	Vented Vapor Saturation Factor; Eq. 1-21: Ks = 1/(1+0.053*PvA*Hvo)	Ks	1.00
Average Reid Vapor Pressure	RVP	0.00		Vapor Pressure at Avg Daily Liq Surface Temp	PvA	0.1418 psia
Product factor: 0.4 for crude oils or 1 for other organic liquids	Kc	1.00		Vapor Space Outage	Hvo	0.00 ft
Vapor Pressure Equation Constant A	A	0.00		Vapor Space Expansion Factor (Eq. 1-5: (ΔTv/TLA)+(ΔPv-ΔPB)/(PA-PvA))	KE	0.0331 per day
Vapor Pressure Equation Constant B (Table 7.1-2)	B	0.0	R	Average Daily Vapor Temperature Range	ΔTv	19.81 °R
Tank design data						
Shell height	Hs	7.85	ft	Average Daily Vapor Pressure Range	ΔPv	0.00000 psia
Diameter	D	13.35	ft	Partially Insulated - Equation 1-8 (ΔTv = 0.6 ΔTA + 0.02 or I)	ΔTv	18.31 °R
Throughput	Q	6.400	gal/month	Fully Insulated, constant temperature	ΔTv	0.00 °R
Turnovers	N	9.47	per year	Average Daily Vapor Pressure Range (ΔPv)	ΔPv	0.00000 psia
Roof Type:		0.00		Not Insulated - Equation 1-9: ΔPv = PvX - Pvn	ΔPv	0.00000 psia
Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft	Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25: PvX = exPvN)	PvX	1.00000 psia
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA	ft	Vapor pressure at ave daily min liquid surface temp. (Eq. 1-25: Pvn = exPvn)	Pvn	1.00000 psia
Maximum Filling Height -use (Pi/4)D if unknown	HLX	6.85	ft	Average daily max. liquid surface temp.; Fig. 7.1-17 TLX = TLA + 0.25ΔTv	TLX	536.72 °R
Minimum Filling Height (use 0 if unknown)	HLN	1.00	ft	Average daily min. liquid surface temp.; Fig. 7.1-17 TLN = TLA - 0.25ΔTv	TLN	526.81 °R
Liquid height (assume 1/2 H)	HL	3.93	ft	Average Daily Ambient Temperature (TAA) Eq. 1-30 TAA = ((TAX+TAN)/2)		
Tank insulation (pick from drop down list)	Q	Not Insulated		Average daily maximum ambient temperature, Table 7.1-7		
Tank Construction (pick from drop down list)		Welded		Average daily minimum ambient temperature, Table 7.1-7		
Tank Shell Color (pick from drop down list)		White		Liquid Bulk Temperature; Eq. 1-31: TB = TAA + 0.003 or I		
Tank Shell Condition (pick from drop down list)		Average		Average Daily Liquid Surface Temperature (TLA)		
Tank Interior Condition (pick from drop down list)		Light Rust		Not Insulated; Eq. 1-28: TLA = 0.4*TAA + 0.6*TB + 0.005*oI		
Tank paint solar absorptance, dimensionless, Table 7.1-6	α	0.25		Partially Insulated; Eq. 1-29: TLA = 0.3*TAA + 0.7*TB + 0.005*oR		
Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	0.03	psia	Fully Insulated; TLA = TB		
True Vapor Pressure; Eq. 1-25: PvA = exp(A/(B-TLA))						
Not Insulated	PvA	0.1417706		Average Vapor Temperature (Tv)		
Partially Insulated	PvA	0.1424275		Not Insulated; Eq. 1-33: Tv = 0.7*TAA + 0.3*TB + 0.009*oI		
Fully Insulated	PvA	0.1336728		Partially Insulated; Eq. 1-34: Tv = 0.6*TAA + 0.4*TB + 0.01*oR		
Average Daily Ambient Temperature (TAA) Eq. 1-30 TAA = ((TAX+TAN)/2)						
Average daily maximum ambient temperature, Table 7.1-7	TAX	536.10	°R	Fully Insulated; Tv = TB		
Average daily minimum ambient temperature, Table 7.1-7	TAN	521.10	°R	Stock Vapor Density; Eq. 1-22: Wv = (Mv/PvA)/(R*Tv)		
Liquid Bulk Temperature; Eq. 1-31: TB = TAA + 0.003 or I						
Fully Insulated (ΔPv = 0) ΔPv = 0.00 psia						
Average Daily Liquid Surface Temperature (TLA)						
Not Insulated; Eq. 1-28: TLA = 0.4*TAA + 0.6*TB + 0.005*oI						
Partially Insulated; Eq. 1-29: TLA = 0.3*TAA + 0.7*TB + 0.005*oR						
Fully Insulated; TLA = TB						
Average Vapor Temperature (Tv)						
Not Insulated; Eq. 1-33: Tv = 0.7*TAA + 0.3*TB + 0.009*oI						
Partially Insulated; Eq. 1-34: Tv = 0.6*TAA + 0.4*TB + 0.01*oR						
Fully Insulated; Tv = TB						
Stock Vapor Density; Eq. 1-22: Wv = (Mv/PvA)/(R*Tv)						
Not Insulated Wv = 3.221E-03						
Partially Insulated Wv = 3.232E-03						
Fully Insulated Wv = 3.055E-03						

HAPS Speciation	lb/month	Vapor Weight Concentration	Vapor Mole Fraction
Total HAP Emissions	4.515	Eq. 40-6 Zvi = yMi / MV	Eq. 40-5 yi = Pi / PvA
Individual HAPS			
hexane	0.0000	86.18	0.00000
benzene	0.0000	78.11	0.00000
2,2,4 TMP	0.0000	114.23	0.00000
toluene	0.0000	92.14	0.00000
ethylbenzene	1.3140	106.17	0.29099
xylene	3.2015	106.17	0.70901
naphthalene	0.0000	128.17	0.00E+00
cumene	0.0000	120.19	0.00E+00

Component Vapor Pressure	PvA=(0.0193737)10 ^{(A-B/(TLA-C))}	A	B	C	PvA
hexane	0.00000	130	86.18	0.00000	6.878
benzene	0.00000	130	78.11	0.00000	6.906
2,2,4 TMP	0.00000	130	114.23	0.00000	6.812
toluene	0.00000	130	92.14	0.00000	7.017
ethylbenzene	0.26400	130	106.17	0.32326	6.95
xylene	0.73600	130	106.17	0.9120	7.009
naphthalene	0.00000	130	128.17	0.00000	7.146
cumene	0.00000	130	120.19	0.00000	6.929

Monthly Calculations (continued)

JULY

Tank No.	13316A	Symbol	Units	ROUTINE EMISSIONS CALCULATIONS	Symbol	Units	HAPS Speciation	lb/month
ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS	Symbol	Units	additive	
Total Losses (Eq. 1-1: LT = LS+LW)	LT	5.35	lb/month	Standing Losses; Eq. 1-2: LS = 365 (Vv * Wv * KE * Ks)	LS	2.10	Total HAP Emissions =	5.348
Vapor Space Volume	Vv	549.8	ft ³	Vapor Space Density	Wv	0.0038	Eq. 40-2 Zvi = yMi / MV	
Stock Vapor Density	Wv	0.0038	lb/ft ³	Vapor Space Expansion Factor (0 < KE <= 1); Eq. 1-5	KE	0.032	Eq. 40-5 yi = Pi / PVA	
Vented Vapor Saturation Factor	Ks	1.00	NA	Constant; Number of Daily Events in a Year	365	31	Individual HAPS	
Daily total solar insolation on a horizontal surface; Table 7.1-7	I	1904.0	Btu/ft ² -day	Vented Vapor Saturation Factor	KE	1.00	Li (lb/month)	
Absolute Pressure	Pa	14.69	psia	Working Losses; Eq. 1-35: LW = VQ * KN * Kp * Wv * KB	Lw	3.25	Mi	
Ideal Gas Constant	R	10.73	psia ft ³ /lb-mole R	Net Working Loss Throughput (Eq. 1-39: VQ=5.614*Q)	VQ	3.25	Mv	
Product Information				Working Loss Turnover Factor Eq. 1-35 Ks=(180+N)/6N for N>=36, else Ks=	KN	1.0000	Zvi	
Product Type	Diethyl Additive			Working Loss Product Factor	Kp	1.00	Pi = PVA(Xi)	
Vapor Molecular weight	Mv	130	lb/lb-mole	Stock Vapor Density	Wv	0.0038	PVA	
Average organic liquid density	WL	6.10	lb/gal	Vent Saturation Correction Factor	KB	1.00	yi	
Average Reid Vapor Pressure	RVP	0.00	psia	Vented Vapor Saturation Factor; Eq. 1-21: Ks = 1/(1+0.053*PvA*Hvo)	KS	1.00	Component Vapor Pressure	
Product factor: 0.4 for crude oils or 1 for other organic liquids	Kc	1.00		Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.1690	PVA=(0.019373) ¹⁰ *PVA-B/(TLA-C)	
Vapor Pressure Equation Constant A	A	0.00		Vapor Space Outage	Hvo	0.00	A	
Vapor Pressure Equation Constant B (Table 7.1-2)	B	0.0	R	Vapor Space Expansion Factor (Eq. 1-5: (ΔTv/TLA)+(ΔPv-ΔPB)/(PA-PvA))	KE	0.0324	B	
Tank design data				Average Daily Vapor Temperature Range	ΔTv	19.60	C	
Shell height	Hs	7.85	ft	Average Daily Vapor Pressure Range	ΔPv	0.0000	PvB	
Diameter	D	13.35	ft	Partially Insulated - Equation 1-8 (ΔTv = 0.6 ΔTA + 0.02 or I)	ΔTv	18.16		
Throughput	Q	6.400	gal/month	Fully Insulated, constant temperature	ΔTv	0.00		
Turnovers	N	9.16	per year	Average Daily Vapor Pressure Range (ΔPv)				
Roof Type:				Not Insulated - Equation 1-9: ΔPv = PVX - PVN	ΔPv	0.00000		
Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft	Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25 PVX = ex)	PVX	1.00000		
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA	ft	Vapor pressure at ave daily min liquid surface temp. (Eq. 1-25 PVN = ex)	PVN	1.00000		
Maximum Filling Height -use (Pi/4)D if unknown	HLX	6.85	ft	Average daily max. liquid surface temp.; Fig. 7.1-17 TLX = TLA + 0.25ΔT	TLX	542.04		
Minimum Filling Height (use 0 if unknown)	HLN	1.00	ft	Average daily min. liquid surface temp.; Fig. 7.1-17 TLN = TLA - 0.25ΔT	TLN	532.24		
Liquid height (assume 1/2 H)	HL	3.93	ft	Partially Insulated - Equation 1-9: ΔPv = PVX - PVN	ΔPv	0.00000		
Tank insulation (pick from drop down list)	Q	Not Insulated		Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25 u)PVX	PVX	1.00000		
Tank Construction (pick from drop down list)		Welded		Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25 u)PVN	PVN	1.000000		
Tank Shell Color (pick from drop down list)		White		Average daily maximum liquid surface temperature, deg R (TLX = TLA + TLX)	TLX	541.82		
Tank Shell Condition (pick from drop down list)		Average		Average daily minimum liquid surface temperature, deg R (TLN = TLA - TLN)	TLN	532.74		
Tank Interior Condition (pick from drop down list)		Light Rust		Fully Insulated (ΔPv = 0)	ΔPv	0.00		
Tank paint solar absorptance, dimensionless, Table 7.1-6	α	0.25		Vapor Space Volume (Eq.1-3: Vv = (Pi/4) D ² Hvo)	Vv	549.78		
Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	0.03	psia	Effective Tank diameter	Dv	13.35		
True Vapor Pressure; Eq. 1-25, PvA = exp(A-(B/TLA))		-0.03		Effective Tank Height	Hv	7.85		
Not Insulated	PvA	0.168992	psia	Vapor Space Outage Hvo = 1/2 H	Hvo	3.93		
Partially Insulated	PvA	0.1697728	psia					
Fully Insulated	PvA	0.1593647	psia					
Average Daily Ambient Temperature (TAA) Eq. 1-30 TAA = ((TAX+TAN)/2)	TAA	533.90	°R					
Average daily maximum ambient temperature, Table 7.1-7	TAX	541.10	°R					
Average daily minimum ambient temperature, Table 7.1-7	TAN	526.70	°R					
Liquid Bulk Temperature; Eq 1-31: TB = TAA + 0.003 or 1	TB	535.33	°R					
Average Daily Liquid Surface Temperature (TLA)								
Not Insulated; Eq. 1-28, TLA = 0.4*TAA + 0.6*TB + 0.005*Q	TLA	537.14	°R					
Partially Insulated; Eq. 1-29, TLA = 0.3*TAA + 0.7*TB + 0.005*Q	TLA	537.28	°R					
Fully Insulated; TLA = TB	TLA	535.3	°R					
Average Vapor Temperature (Tv)								
Not Insulated; Eq. 1-33, Tv = 0.7*TAA + 0.3*TB + 0.009*Q	Tv	538.61	°R					
Partially Insulated; Eq. 1-34, Tv = 0.6*TAA + 0.4*TB + 0.01*Q	Tv	539.23	°R					
Fully Insulated; Tv = TB	Tv	535.33	°R					
Stock Vapor Density; Eq. 1-22, Wv = (Mv/PVA)/(R*TV)								
Not Insulated	Wv	3.801E-03						
Partially Insulated	Wv	3.814E-03						
Fully Insulated	Wv	3.806E-03						

Monthly Calculations (continued)

AUGUST

Tank No.	13316A	Symbol	Units	ROUTINE EMISSIONS CALCULATIONS	Symbol	Units	HAPS Speciation	lb/month
ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS	Symbol	Units	additive	
Total Losses (Eq. 1-1: LT = LS+LW)	LT	5.00	lb/month	Standing Losses; Eq. 1-2: LS = 365 (Vv * Wv * KE * Ks)	LS	1.86	Total HAP Emissions =	5.005
Vapor Space Volume	Vv	549.8	ft ³	Vapor Space Density	Wv	0.0037	Eq. 40-2 Zvi = yMi / MV	
Stock Vapor Density	Wv	0.0037	lb/ft ³	Vapor Space Expansion Factor (0 < KE <= 1); Eq. 1-5	KE	0.030	Eq. 40-5 yi = Pi / PVA	
Vented Vapor Saturation Factor	Ks	1.00	NA	Constant; Number of Daily Events in a Year	365	31	Individual HAPS	
Daily total solar insolation on a horizontal surface; Table 7.1-7	I	1685.0	Btu/ft ² -day	Vented Vapor Saturation Factor	KE	1.00	Li (lb/month)	
Absolute Pressure	Pa	14.69	psia	Working Losses; Eq. 1-35: LW = VQ * KN * Kp * Wv * KB	Lw	3.15	Mi	
Ideal Gas Constant	R	10.73	psia ft ³ /lb-mole R	Net Working Loss Throughput (Eq. 1-39: VQ=5.614*Q)	VQ	3.15	Mv	
Product Information				Working Loss Turnover Factor Eq. 1-35 Ks=(180+N)/6N for N>=36, else Ks=	KN	1.0000	Zvi	
Product Type	Diethyl Additive			Working Loss Product Factor	Kp	1.00	Pi = PVA(Xi)	
Vapor Molecular weight	Mv	130	lb/lb-mole	Stock Vapor Density	Wv	0.0037	PVA	
Average organic liquid density	WL	6.10	lb/gal	Vent Saturation Correction Factor	KB	1.00	yi	
Average Reid Vapor Pressure	RVP	0.00	psia	Vented Vapor Saturation Factor; Eq. 1-21: Ks = 1/(1+0.053*PvA*Hvo)	KS	1.00	Component Vapor Pressure	
Product factor: 0.4 for crude oils or 1 for other organic liquids	Kc	1.00		Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.1632	PVA=(0.019373) ¹⁰ *PVA-B/(TLA-C)	
Vapor Pressure Equation Constant A	A	0.00		Vapor Space Outage	Hvo	0.00	A	
Vapor Pressure Equation Constant B (Table 7.1-2)	B	0.0	R	Vapor Space Expansion Factor (Eq. 1-5: (ΔTv/TLA)+(ΔPv-ΔPB)/(PA-PvA))	KE	0.0296	B	
Tank design data				Average Daily Vapor Temperature Range	ΔTv	18.09	C	
Shell height	Hs	7.85	ft	Average Daily Vapor Pressure Range	ΔPv	0.00000	PvB	
Diameter	D	13.35	ft	Partially Insulated - Equation 1-8 (ΔTv = 0.6 ΔTA + 0.02 or I)	ΔTv	16.71		
Throughput	Q	6.400	gal/month	Fully Insulated, constant temperature	ΔTv	0.00		
Turnovers	N	9.16	per year	Average Daily Vapor Pressure Range (ΔPv)				
Roof Type:				Not Insulated - Equation 1-9: ΔPv = PVX - PVN	ΔPv	0.00000		
Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft	Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25 PVX = ex)	PVX	1.00000		
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA	ft	Vapor pressure at ave daily min liquid surface temp. (Eq. 1-25 PVN = ex)	PVN	1.00000		
Maximum Filling Height -use (Pi/4)D if unknown	HLX	6.85	ft	Average daily max. liquid surface temp.; Fig. 7.1-17 TLX = TLA + 0.25ΔT	TLX	540.59		
Minimum Filling Height (use 0 if unknown)	HLN	1.00	ft	Average daily min. liquid surface temp.; Fig. 7.1-17 TLN = TLA - 0.25ΔT	TLN	531.54		
Liquid height (assume 1/2 H)	HL	3.93	ft	Partially Insulated - Equation 1-9: ΔPv = PVX - PVN	ΔPv	0.00000		
Tank insulation (pick from drop down list)	Q	Not Insulated		Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25 u)PVX	PVX	1.00000		
Tank Construction (pick from drop down list)		Welded		Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25 u)PVN	PVN	1.000000		
Tank Shell Color (pick from drop down list)		White		Average daily maximum liquid surface temperature, deg R (TLX = TLA + TLX)	TLX	540.37		
Tank Shell Condition (pick from drop down list)		Average		Average daily minimum liquid surface temperature, deg R (TLN = TLA - TLN)	TLN	532.01		
Tank Interior Condition (pick from drop down list)		Light Rust		Fully Insulated (ΔPv = 0)	ΔPv	0.00		
Tank paint solar absorptance, dimensionless, Table 7.1-6	α	0.25		Vapor Space Volume (Eq.1-3: Vv = (Pi/4) D ² Hvo)	Vv	549.78		
Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	0.03	psia	Effective Tank diameter	Dv	13.35		
True Vapor Pressure; Eq. 1-25, PvA = exp(A-(B/TLA))		-0.03		Effective Tank Height	Hv	7.85		
Not Insulated	PvA	0.1632264	psia	Vapor Space Outage Hvo = 1/2 H	Hvo	3.93		
Partially Insulated	PvA	0.163897	psia					
Fully Insulated	PvA	0.1549333	psia					
Average Daily Ambient Temperature (TAA) Eq. 1-30 TAA = ((TAX+TAN)/2)	TAA	533.20	°R					
Average daily maximum ambient temperature, Table 7.1-7	TAX	540.10	°R					
Average daily minimum ambient temperature, Table 7.1-7	TAN	526.30	°R					
Liquid Bulk Temperature; Eq 1-31: TB = TAA + 0.003 or 1	TB	534.46	°R					
Average Daily Liquid Surface Temperature (TLA)								
Not Insulated; Eq. 1-28, TLA = 0.4*TAA + 0.6*TB + 0.005*Q	TLA	536.06	°R					
Partially Insulated; Eq. 1-29, TLA = 0.3*TAA + 0.7*TB + 0.005*Q	TLA	536.19	°R					
Fully Insulated; TLA = TB	TLA	534.5	°R					
Average Vapor Temperature (Tv)								
Not Insulated; Eq. 1-33, Tv = 0.7*TAA + 0.3*TB + 0.009*Q	Tv	537.37	°R					
Partially Insulated; Eq. 1-34, Tv = 0.6*TAA + 0.4*TB + 0.01*Q	Tv	537.92	°R					
Fully Insulated; Tv = TB	Tv	534.46	°R					
Stock Vapor Density; Eq. 1-22, Wv = (Mv/PVA)/(R*TV)								
Not Insulated	Wv	3.680E-03						
Partially Insulated	Wv	3.691E-03						
Fully Insulated	Wv	3.512E-03						

Monthly Calculations (continued)

SEPTEMBER

Tank No.	13316A	Symbol	Units	ROUTINE EMISSIONS CALCULATIONS	Symbol	Units	HAPS Speciation	lb/month
ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS	Symbol	Units	Product	
Total Losses (Eq. 1-1: LT = LS+LW)	LT	3.80	lb/month	Standing Losses; Eq. 1-2: LS = 365 (Vv * Wv * KE * Ks)	LS	1.32	lb/month	additive
Throughput	Q	1.90E-03	ton/month	Vapor Space Volume	Vv	549.8	ft ³	Total HAP Emissions = 3.798
Nearest US Location	Time Period	September	Bridgeport, CT	Stock Vapor Density	Wv	0.0029	lb/ft ³	Eq. 40-6 ZVI = yM / MV
Daily total solar insolation on a horizontal surface; Table 7.1-7	I	1320.0	Btu/ft ² -day	Vapor Space Expansion Factor (0 < KE <= 1); Eq. 1-5	KE	0.028	per day	Eq. 40-5 yi = Pi / PVA
Absolute Pressure	Pa	14.69	psia	Vented Vapor Saturation Factor	Ks	1.00	NA	Individual HAPS
Ideal Gas Constant	R	10.73	psia ft ³ /lb-mole R	Constant; Number of Daily Events in a Year	365	30	days/month	Eq. 40-2 Li = Zi(Li)
Product Information	Product Type	Diesel Additive	Working Losses; Eq. 1-35: Lw = VQ * KN * Kp * Wv * KB	Net Working Loss Throughput (Eq. 1-39: VQ=5.614*Q)	VQ	855	ft ³ /month	Eq. 40-6 ZVI = yM / MV
Vapor Molecular weight	Mv	130	lb/lb-mole	Working Loss Turnover Factor Eq. 1-35 Ks=(180+N)/6N for N>=36, else Ks=	KN	1.0000		Eq. 40-5 yi = Pi / PVA
Average organic liquid density	WL	6.10	lb/gal	Working Loss Product Factor	Kp	1.00		Individual HAPS
Average Reid Vapor Pressure	RVP	0.00		Stock Vapor Density	Wv	0.0029	lb/ft ³	Eq. 40-2 Li = Zi(Li)
Product factor: 0.4 for crude oils or 1 for other organic liquids	Kc	1.00		Vent Setting Correction Factor	KB	1.00		Liquid Mole Fraction
Vapor Pressure Equation Constant A	A	0.00		Vented Vapor Saturation Factor; Eq. 1-21: Ks = 1/(1+0.053*PvA*Hvo)	Ks	1.00		Eq. 40-4 xi = (ZiMLi)Mi
Vapor Pressure Equation Constant B (Table 7.1-2)	B	0.0	R	Vapor Pressure at Avg Daily Liq Surface Temp	PvA	0.1267	psia	Component Vapor Pressure
Tank design data	Shell height	Hs	7.85	Vapor Space Volume (Eq.1-3: Vv = (Pi/4) D^2Hvo)	Vv	549.78	ft ³	Eq. 40-6 ZVI = yM / MV
Diameter	D	13.35	ft	Effective Tank diameter	Dt	13.35	ft	Eq. 40-5 yi = Pi / PVA
Throughput	Q	6.400	gal/month	Vapor Space Height	Hv	7.85	ft	Individual HAPS
Turnovers	N	9.47	per year	Vapor Space Outage Hvo = 1/2 H	Hvo	3.93	ft	Eq. 40-2 Li = Zi(Li)
Roof Type:	0.00							Liquid Mole Fraction
Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft					Eq. 40-4 xi = (ZiMLi)Mi
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA	ft					Component Vapor Pressure
Maximum Filling Height -use (Pi/4)D if unknown	HLX	6.85	ft					Eq. 40-6 ZVI = yM / MV
Minimum Filling Height (use 0 if unknown)	HLN	1.00	ft					Eq. 40-5 yi = Pi / PVA
Liquid height (assume 1/2 H)	HL	3.93	ft					Individual HAPS
Tank insulation (pick from drop down list)	Not Insulated							Eq. 40-2 Li = Zi(Li)
Tank Construction (pick from drop down list)	Welded							Liquid Mole Fraction
Tank Shell Color (pick from drop down list)	White							Eq. 40-4 xi = (ZiMLi)Mi
Tank Shell Condition (pick from drop down list)	Average							Component Vapor Pressure
Tank Interior Condition (pick from drop down list)	Light Rust							Eq. 40-6 ZVI = yM / MV
Tank paint solar absorptance, dimensionless; Table 7.1-6	alpha	0.25						Eq. 40-5 yi = Pi / PVA
Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	0.03	psia					Individual HAPS
True Vapor Pressure; Eq. 1-25: PvA = exp(A-(B/TLA))	PvA	0.1266829	psia					Eq. 40-2 Li = Zi(Li)
Not Insulated	PvA	0.1266829	psia					Liquid Mole Fraction
Partially Insulated	PvA	0.1271055	psia					Eq. 40-4 xi = (ZiMLi)Mi
Fully Insulated	PvA	0.1214345	psia					Component Vapor Pressure
Average Daily Ambient Temperature (TAA) Eq. 1-30 TAA = ((TAX+1	TAA	526.15	R					Eq. 40-6 ZVI = yM / MV
Average daily maximum ambient temperature; Table 7.1-7	TAX	533.40	R					Eq. 40-5 yi = Pi / PVA
Average daily minimum ambient temperature; Table 7.1-7	TAN	518.90	R					Individual HAPS
Liquid Bulk Temperature; Eq. 1-31: TB = TAA + 0.003 os l	TB	527.14	R					Eq. 40-2 Li = Zi(Li)
Average Daily Liquid Surface Temperature (TLA)	TLA	528.39	R					Liquid Mole Fraction
Not Insulated; Eq. 1-28: TLA = 0.4*TAA + 0.6*TB + 0.005*alpha	TLA	528.49	R					Eq. 40-4 xi = (ZiMLi)Mi
Partially Insulated; Eq. 1-29: TLA = 0.3*TAA + 0.7*TB + 0.005*alpha	TLA	527.1	R					Component Vapor Pressure
Fully Insulated; TLA = TB	TLA	527.1	R					Eq. 40-6 ZVI = yM / MV
Average Vapor Temperature (Tv)	Tv	529.42	R					Eq. 40-5 yi = Pi / PVA
Not Insulated; Eq. 1-33: Tv = 0.7*TAA + 0.3*TB + 0.009*alpha	Tv	529.85	R					Individual HAPS
Partially Insulated; Eq. 1-34: Tv = 0.6*TAA + 0.4*TB + 0.01*alpha	Tv	527.14	R					Eq. 40-2 Li = Zi(Li)
Fully Insulated; Tv = TB	Tv	527.14	R					Liquid Mole Fraction
Stock Vapor Density; Eq. 1-22: Wv = (Mv/PVA)/(R*Tv)	Wv	2.899E-03						Eq. 40-4 xi = (ZiMLi)Mi
Not Insulated	Wv	2.899E-03						Component Vapor Pressure
Partially Insulated	Wv	2.906E-03						Eq. 40-6 ZVI = yM / MV
Fully Insulated	Wv	2.791E-03						Eq. 40-5 yi = Pi / PVA

Monthly Calculations (continued)

OCTOBER

Tank No.	13316A	Symbol	Units	ROUTINE EMISSIONS CALCULATIONS	Symbol	Units	HAPS Speciation	lb/month
ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS	Symbol	Units	Product	
Total Losses (Eq. 1-1: LT = LS+LW)	LT	2.53	lb/month	Standing Losses; Eq. 1-2: LS = 365 (Vv * Wv * KE * Ks)	LS	0.86	lb/month	additive
Throughput	Q	1.27E-03	ton/month	Vapor Space Volume	Vv	549.8	ft ³	Total HAP Emissions = 2.535
Nearest US Location	Time Period	October	Bridgeport, CT	Stock Vapor Density	Wv	0.0020	lb/ft ³	Eq. 40-6 ZVI = yM / MV
Daily total solar insolation on a horizontal surface; Table 7.1-7	I	948.0	Btu/ft ² -day	Vapor Space Expansion Factor (0 < KE <= 1); Eq. 1-5	KE	0.026	per day	Eq. 40-5 yi = Pi / PVA
Absolute Pressure	Pa	14.69	psia	Vented Vapor Saturation Factor	Ks	1.00	NA	Individual HAPS
Ideal Gas Constant	R	10.73	psia ft ³ /lb-mole R	Constant; Number of Daily Events in a Year	365	31	days/month	Eq. 40-2 Li = Zi(Li)
Product Information	Product Type	Diesel Additive	Working Losses; Eq. 1-35: Lw = VQ * KN * Kp * Wv * KB	Net Working Loss Throughput (Eq. 1-39: VQ=5.614*Q)	VQ	855	ft ³ /month	Eq. 40-6 ZVI = yM / MV
Vapor Molecular weight	Mv	130	lb/lb-mole	Working Loss Turnover Factor Eq. 1-35 Ks=(180+N)/6N for N>=36, else Ks=	KN	1.0000		Eq. 40-5 yi = Pi / PVA
Average organic liquid density	WL	6.10	lb/gal	Working Loss Product Factor	Kp	1.00		Individual HAPS
Average Reid Vapor Pressure	RVP	0.00		Stock Vapor Density	Wv	0.0020	lb/ft ³	Eq. 40-2 Li = Zi(Li)
Product factor: 0.4 for crude oils or 1 for other organic liquids	Kc	1.00		Vent Setting Correction Factor	KB	1.00		Liquid Mole Fraction
Vapor Pressure Equation Constant A	A	0.00		Vented Vapor Saturation Factor; Eq. 1-21: Ks = 1/(1+0.053*PvA*Hvo)	Ks	1.00		Eq. 40-4 xi = (ZiMLi)Mi
Vapor Pressure Equation Constant B (Table 7.1-2)	B	0.0	R	Vapor Pressure at Avg Daily Liq Surface Temp	PvA	0.0835	psia	Component Vapor Pressure
Tank design data	Shell height	Hs	7.85	Vapor Space Volume (Eq.1-3: Vv = (Pi/4) D^2Hvo)	Vv	549.78	ft ³	Eq. 40-6 ZVI = yM / MV
Diameter	D	13.35	ft	Effective Tank diameter	Dt	13.35	ft	Eq. 40-5 yi = Pi / PVA
Throughput	Q	6.400	gal/month	Vapor Space Height	Hv	7.85	ft	Individual HAPS
Turnovers	N	9.16	per year	Vapor Space Outage Hvo = 1/2 H	Hvo	3.93	ft	Eq. 40-2 Li = Zi(Li)
Roof Type:	0.00							Liquid Mole Fraction
Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft					Eq. 40-4 xi = (ZiMLi)Mi
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA	ft					Component Vapor Pressure
Maximum Filling Height -use (Pi/4)D if unknown	HLX	6.85	ft					Eq. 40-6 ZVI = yM / MV
Minimum Filling Height (use 0 if unknown)	HLN	1.00	ft					Eq. 40-5 yi = Pi / PVA
Liquid height (assume 1/2 H)	HL	3.93	ft					Individual HAPS
Tank insulation (pick from drop down list)	Not Insulated							Eq. 40-2 Li = Zi(Li)
Tank Construction (pick from drop down list)	Welded							Liquid Mole Fraction
Tank Shell Color (pick from drop down list)	White							Eq. 40-4 xi = (ZiMLi)Mi
Tank Shell Condition (pick from drop down list)	Average							Component Vapor Pressure
Tank Interior Condition (pick from drop down list)	Light Rust							Eq. 40-6 ZVI = yM / MV
Tank paint solar absorptance, dimensionless; Table 7.1-6	alpha	0.25						Eq. 40-5 yi = Pi / PVA
Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	0.03	psia					Individual HAPS
True Vapor Pressure; Eq. 1-25: PvA = exp(A-(B/TLA))	PvA	0.0835155	psia					Eq. 40-2 Li = Zi(Li)
Not Insulated	PvA	0.0835155	psia					Liquid Mole Fraction
Partially Insulated	PvA	0.0837274	psia					Eq. 40-4 xi = (ZiMLi)Mi
Fully Insulated	PvA	0.0808716	psia					Component Vapor Pressure
Average Daily Ambient Temperature (TAA) Eq. 1-30 TAA = ((TAX+1	TAA	514.75	R					Eq. 40-6 ZVI = yM / MV
Average daily maximum ambient temperature; Table 7.1-7	TAX	522.40	R					Eq. 40-5 yi = Pi / PVA
Average daily minimum ambient temperature; Table 7.1-7	TAN	507.10	R					Individual HAPS
Liquid Bulk Temperature; Eq. 1-31: TB = TAA + 0.003 os l	TB	515.46	R					Eq. 40-2 Li = Zi(Li)
Average Daily Liquid Surface Temperature (TLA)	TLA	516.36	R					Liquid Mole Fraction
Not Insulated; Eq. 1-28: TLA = 0.4*TAA + 0.6*TB + 0.005*alpha	TLA	516.43	R					Eq. 40-4 xi = (ZiMLi)Mi
Partially Insulated; Eq. 1-29: TLA = 0.3*TAA + 0.7*TB + 0.005*alpha	TLA	515.5	R					Component Vapor Pressure
Fully Insulated; TLA = TB	TLA	515.5	R					Eq. 40-6 ZVI = yM / MV
Average Vapor Temperature (Tv)	Tv	517.10	R					Eq. 40-5 yi = Pi / PVA
Not Insulated; Eq. 1-33: Tv = 0.7*TAA + 0.3*TB + 0.009*alpha	Tv	517.40	R					Individual HAPS
Partially Insulated; Eq. 1-34: Tv = 0.6*TAA + 0.4*TB + 0.01*alpha	Tv	515.46	R					Eq. 40-2 Li = Zi(Li)
Fully Insulated; Tv = TB	Tv	515.46	R					Liquid Mole Fraction
Stock Vapor Density; Eq. 1-22: Wv = (Mv/PVA)/(R*Tv)	Wv	1.957E-03						Eq. 40-4 xi = (ZiMLi)Mi
Not Insulated	Wv	1.957E-03						Component Vapor Pressure
Partially Insulated	Wv	1.960E-03						Eq. 40-6 ZVI = yM / MV
Fully Insulated	Wv	1.901E-03						Eq. 40-5 yi = Pi / PVA

Monthly Calculations (continued)

NOVEMBER

Tank No.	13316A	Symbol	Units	ROUTINE EMISSIONS CALCULATIONS	Symbol	Units	HAPS Speciation	ib/month
ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS	Symbol	Units	additive	
Total Losses (Eq. 1-1: $LT = LS + LW$)	LT	1.66	lb/month	Standing Losses; Eq. 1-2: $LS = 365 (Vv \cdot Wv \cdot KE \cdot Ks)$	LS	0.47	Total HAP Emissions =	1.660
		8.30E-04	ton/month	Vapor Space Volume	Vv	549.8	Eq. 40-6 ZVI = yM / MV	
				Stock Vapor Density	Wv	0.0014	Eq. 40-5 $y_i = P_i / PVA$	
				Vapor Space Expansion Factor ($0 < KE \leq 1$); Eq. 1-5	KE	0.021	Individual HAPS	L_{ij} (lb/month)
Nearest US Location	Bridgeport, CT			Vented Vapor Saturation Factor	Ks	1.00	hexane	0.0000
Daily total solar insolation on a horizontal surface; Table 7.1-7	I	621.0	Btu/ft ² -day	Constant; Number of Daily Events in a Year	365	31	benzene	0.0000
Absolute Pressure	Pa	14.69	psia	Working Losses; Eq. 1-35: $Lw = VQ \cdot KN \cdot Kp \cdot Wv \cdot KB$	Lw	1.19	2,2,4 TMP	0.0000
Ideal Gas Constant	R	10.73	psia ft ³ /lb-mole R	Net Working Loss Throughput (Eq. 1-39: $VQ = 5.614 \cdot Q$)	VQ	855	toluene	0.0000
Product Information				Working Loss Turnover Factor Eq. 1-35 $Ks = (180 + N)/6N$ for $N \geq 36$, else $Ks = N$	KN	1.0000	ethylbenzene	0.4856
Product Type	Diesel Additive			Working Loss Product Factor	Kp	1.00	xylene	1.1748
Vapor Molecular weight	Mv	130	lb/lb-mole	Stock Vapor Density	Wv	0.0014	naphthalene	0.0000
Average organic liquid density	WL	6.10	lb/gal	Vent Setting Correction Factor	KB	1.00	cumene	0.0000
Average Reid Vapor Pressure	RVP	0.00	psia	Vented Vapor Saturation Factor; Eq. 1-21: $Ks = 1 / (1 + 0.053 \cdot PVA \cdot Hvo)$	Ks	1.00	Liquid Mole Fraction	
Product factor; 0.4 for crude oils or 1 for other organic liquids	Kc	1.00		Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.0581	Eq. 40-4 $x_i = (Z_i \cdot M_i) / M_i$	
Vapor Pressure Equation Constant A	A	0.00		Vapor Space Outage	Hvo	0.00	Individual HAPS	Z_i
Vapor Pressure Equation Constant B (Table 7.1-2)	B	0.0	R	Vapor Space Volume (Eq. 1-3: $Vv = ((\pi / 4) \cdot D^2 \cdot Hvo)$	Vv	549.78	hexane	0.00000
Tank design data				Effective Tank diameter	Dt	13.35	benzene	0.00000
Shell height	Hs	7.85	ft	Effective Tank Height	Ht	7.85	2,2,4 TMP	0.00000
Diameter	D	13.35	ft	Vapor Space Outage Hvo = 1/2 H	Hvo	3.93	toluene	0.00000
Throughput	Q	6.400	gal/month				ethylbenzene	0.26400
Turnovers	N	9.47	per year				xylene	0.73600
Roof Type:							naphthalene	0.00000
Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft				cumene	0.00000
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA	ft				Component Vapor Pressure	
Maximum Filling Height - use (Pi/4)D if unknown	HLX	6.85	ft				Eq. 40-3 $PVA = (0.019337) \cdot 10^{(A - B / (TLA - C))}$	
Minimum Filling Height (use 0 if unknown)	HLN	1.00	ft				A	B
Liquid height (assume 1/2 H)	HL	3.93	ft				C	P _{sat}
Tank insulation (pick from drop down list)	Q	6.400	gal/month				hexane	0.00000
Tank Construction (pick from drop down list)							benzene	0.00000
Tank Shell Color (pick from drop down list)							2,2,4 TMP	0.00000
Tank Shell Condition (pick from drop down list)							toluene	0.00000
Tank Interior Condition (pick from drop down list)							ethylbenzene	0.00000
Tank paint solar absorptance, dimensionless; Table 7.1-6	α	0.25					xylene	0.00000
Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	0.03	psi				naphthalene	0.00000
True Vapor Pressure; Eq. 1-25: $PVA = \exp(A - (B/TLA))$							cumene	0.00000
Not Insulated	P _{Va}	0.0580534	psia				Average Daily Vapor Pressure Range (ΔPv)	
Partially Insulated	P _{Va}	0.0581547	psia				Eq. 1-25 $\Delta Pv = PVX - PVN$	
Fully Insulated	P _{Va}	0.0567834	psia				Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25 $PVX = \exp(A - (B/TLA))$)	
Average Daily Ambient Temperature (TAA) Eq. 1-30 $TAA = ((TAX + TAN) / 2)$	TAA	505.35	°R				Average daily max. liquid surface temp.; Fig. 7.1-17 $TLX = TLA + 0.25 \Delta T$	
Average daily maximum ambient temperature; Table 7.1-7	TAX	512.10	°R				Average daily min. liquid surface temp.; Fig. 7.1-17 $TLN = TLA - 0.25 \Delta T$	
Average daily minimum ambient temperature; Table 7.1-7	TAN	498.60	°R				Average daily ambient temperature range - Equation 1-11 ($\Delta TA = TAX - TAN$)	
Liquid Bulk Temperature; Eq. 1-31: $TB = TAA + 0.003 \text{ as l}$	TB	505.82	°R				Average Daily Vapor Temperature Range (ΔTv)	
Average Daily Liquid Surface Temperature (TLA)							Eq. 1-11 $\Delta TA = TAX - TAN$	
Not Insulated; Eq. 1-28: $TLA = 0.4 \cdot TAA + 0.6 \cdot TB + 0.005 \cdot \alpha$	TLA	506.41	°R				Not Insulated - Equation 1-7 ($\Delta Tv = 0.7 \Delta TA + 0.02 \text{ or l}$)	
Partially Insulated; Eq. 1-29: $TLA = 0.3 \cdot TAA + 0.7 \cdot TB + 0.005 \cdot \alpha$	TLA	506.45	°R				Partially Insulated - Equation 1-8 ($\Delta Tv = 0.6 \Delta TA + 0.02 \text{ or l}$)	
Fully Insulated; $TLA = TB$	TLA	505.8	°R				Fully Insulated, constant temperature	
Average Vapor Temperature (Tv)							Average Daily Vapor Pressure Range (ΔPv)	
Not Insulated; Eq. 1-33: $Tv = 0.7 \cdot TAA + 0.3 \cdot TB + 0.009 \cdot \alpha$	Tv	506.89	°R				Eq. 1-25 $\Delta Pv = PVX - PVN$	
Partially Insulated; Eq. 1-34: $Tv = 0.6 \cdot TAA + 0.4 \cdot TB + 0.01 \cdot \alpha$	Tv	507.09	°R				Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25 $PVX = \exp(A - (B/TLA))$)	
Fully Insulated; $Tv = TB$	Tv	505.82	°R				Vapor pressure at ave. daily min liquid surface temp. (Eq. 1-25 $PVN = \exp(A - (B/TLN))$)	
Stock Vapor Density; Eq. 1-22: $Wv = (Mv \cdot PVA) / (R \cdot Tv)$							Average daily max. liquid surface temp.; Fig. 7.1-17 $TLX = TLA + 0.25 \Delta T$	
Not Insulated	Wv	1.387E-03					Average daily min. liquid surface temp.; Fig. 7.1-17 $TLN = TLA - 0.25 \Delta T$	
Partially Insulated	Wv	1.388E-03					Average daily ambient temperature range - Equation 1-11 ($\Delta TA = TAX - TAN$)	
Fully Insulated	Wv	1.360E-03					Average Daily Vapor Temperature Range (ΔTv)	

Monthly Calculations (continued)

DECEMBER

Tank No.	13316A	Symbol	Units	ROUTINE EMISSIONS CALCULATIONS	Symbol	Units	HAPS Speciation	ib/month
ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS	Symbol	Units	additive	
Total Losses (Eq. 1-1: $LT = LS + LW$)	LT	1.13	lb/month	Standing Losses; Eq. 1-2: $LS = 365 (Vv \cdot Wv \cdot KE \cdot Ks)$	LS	0.31	Total HAP Emissions =	1.130
		5.65E-04	ton/month	Vapor Space Volume	Vv	549.8	Eq. 40-6 ZVI = yM / MV	
				Stock Vapor Density	Wv	0.0010	Eq. 40-5 $y_i = P_i / PVA$	
				Vapor Space Expansion Factor ($0 < KE \leq 1$); Eq. 1-5	KE	0.019	Individual HAPS	L_{ij} (lb/month)
Nearest US Location	Bridgeport, CT			Vented Vapor Saturation Factor	Ks	1.00	hexane	0.0000
Daily total solar insolation on a horizontal surface; Table 7.1-7	I	591.0	Btu/ft ² -day	Constant; Number of Daily Events in a Year	365	31	benzene	0.0000
Absolute Pressure	Pa	14.69	psia	Working Losses; Eq. 1-35: $Lw = VQ \cdot KN \cdot Kp \cdot Wv \cdot KB$	Lw	0.82	2,2,4 TMP	0.0000
Ideal Gas Constant	R	10.73	psia ft ³ /lb-mole R	Net Working Loss Throughput (Eq. 1-39: $VQ = 5.614 \cdot Q$)	VQ	855	toluene	0.0000
Product Information				Working Loss Turnover Factor Eq. 1-35 $Ks = (180 + N)/6N$ for $N \geq 36$, else $Ks = N$	KN	1.0000	ethylbenzene	0.3312
Product Type	Diesel Additive			Working Loss Product Factor	Kp	1.00	xylene	0.7991
Vapor Molecular weight	Mv	130	lb/lb-mole	Stock Vapor Density	Wv	0.0010	naphthalene	0.0000
Average organic liquid density	WL	6.10	lb/gal	Vent Setting Correction Factor	KB	1.00	cumene	0.0000
Average Reid Vapor Pressure	RVP	0.00	psia	Vented Vapor Saturation Factor; Eq. 1-21: $Ks = 1 / (1 + 0.053 \cdot PVA \cdot Hvo)$	Ks	1.00	Liquid Mole Fraction	
Product factor; 0.4 for crude oils or 1 for other organic liquids	Kc	1.00		Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.0395	Eq. 40-4 $x_i = (Z_i \cdot M_i) / M_i$	
Vapor Pressure Equation Constant A	A	0.00		Vapor Space Outage	Hvo	0.00	Individual HAPS	Z_i
Vapor Pressure Equation Constant B (Table 7.1-2)	B	0.0	R	Vapor Space Volume (Eq. 1-3: $Vv = ((\pi / 4) \cdot D^2 \cdot Hvo)$	Vv	549.78	hexane	0.00000
Tank design data				Effective Tank diameter	Dt	13.35	benzene	0.00000
Shell height	Hs	7.85	ft	Effective Tank Height	Ht	7.85	2,2,4 TMP	0.00000
Diameter	D	13.35	ft	Vapor Space Outage Hvo = 1/2 H	Hvo	3.93	toluene	0.00000
Throughput	Q	6.400	gal/month				ethylbenzene	0.26400
Turnovers	N	9.16	per year				xylene	0.73600
Roof Type:							naphthalene	0.00000
Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft				cumene	0.00000
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA	ft				Component Vapor Pressure	
Maximum Filling Height - use (Pi/4)D if unknown	HLX	6.85	ft				Eq. 40-3 $PVA = (0.019337) \cdot 10^{(A - B / (TLA - C))}$	
Minimum Filling Height (use 0 if unknown)	HLN	1.00	ft				A	B
Liquid height (assume 1/2 H)	HL	3.93	ft				C	P _{sat}
Tank insulation (pick from drop down list)	Q	6.400	gal/month				hexane	0.00000
Tank Construction (pick from drop down list)							benzene	0.00000
Tank Shell Color (pick from drop down list)							2,2,4 TMP	0.00000
Tank Shell Condition (pick from drop down list)							toluene	0.00000
Tank Interior Condition (pick from drop down list)							ethylbenzene	0.00000
Tank paint solar absorptance, dimensionless; Table 7.1-6	α	0.25					xylene	0.00000
Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	0.03	psi				naphthalene	0.00000
True Vapor Pressure; Eq. 1-25: $PVA = \exp(A - (B/TLA))$							cumene	0.00000
Not Insulated	P _{Va}	0.0394603	psia				Average Daily Vapor Pressure Range (ΔPv)	
Partially Insulated	P _{Va}	0.0395187	psia				Eq. 1-25 $\Delta Pv = PVX - PVN$	
Fully Insulated	P _{Va}	0.0387265	psia				Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25 $PVX = \exp(A - (B/TLA))$)	
Average Daily Ambient Temperature (TAA) Eq. 1-30 $TAA = ((TAX + TAN) / 2)$	TAA	495.50	°R				Vapor pressure at ave. daily min liquid surface temp. (Eq. 1-25 $PVN = \exp(A - (B/TLN))$)	
Average daily maximum ambient temperature; Table 7.1-7	TAX	501.80	°R				Average daily max. liquid surface temp.; Fig. 7.1-17 $TLX = TLA + 0.25 \Delta T$	
Average daily minimum ambient temperature; Table 7.1-7	TAN	489.20	°R				Average daily min. liquid surface temp.; Fig. 7.1-17 $TLN = TLA - 0.25 \Delta T$	
Liquid Bulk Temperature; Eq. 1-31: $TB = TAA + 0.003 \text{ as l}$	TB	495.88	°R				Average daily ambient temperature range - Equation 1-11 ($\Delta TA = TAX - TAN$)	
Average Daily Liquid Surface Temperature (TLA)							Average Daily Vapor Temperature Range (ΔTv)	
Not Insulated; Eq. 1-28: $TLA = 0.4 \cdot TAA + 0.6 \cdot TB + 0.005 \cdot \alpha$	TLA	496.35	°R				Eq. 1-11 $\Delta TA = TAX - TAN$	
Partially Insulated; Eq. 1-29: $TLA = 0.3 \cdot TAA + 0.7 \cdot TB + 0.005 \cdot \alpha$	TLA	496.39	°R				Not Insulated - Equation 1-7 ($\Delta Tv = 0.7 \Delta TA + 0.02 \text{ or l}$)	
Fully Insulated; $TLA = TB$	TLA	495.9	°R				Partially Insulated - Equation 1-8 ($\Delta Tv = 0.6 \Delta TA + 0.02 \text{ or l}$)	
Average Vapor Temperature (Tv)							Fully Insulated, constant temperature	
Not Insulated; Eq. 1-33: $Tv = 0.7 \cdot TAA + 0.3 \cdot TB + 0.009 \cdot \alpha$	Tv	496.74	°R				Average Daily Vapor Pressure Range (ΔPv)	
Partially Insulated; Eq. 1-34: $Tv = 0.6 \cdot TAA + 0.4 \cdot TB + 0.01 \cdot \alpha$	Tv	496.90	°R				Eq. 1-25 $\Delta Pv = PVX - PVN$	
Fully Insulated; $Tv = TB$	Tv	495.88	°R				Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25 $PVX = \exp(A - (B/TLA))$)	
Stock Vapor Density; Eq. 1-22: $Wv = (Mv \cdot PVA) / (R \cdot Tv)$							Vapor pressure at ave. daily min liquid surface temp. (Eq. 1-25 $PVN = \exp(A - (B/TLN))$)	
Not Insulated	Wv	9.624E-04					Average daily max. liquid surface temp.; Fig. 7.1-17 $TLX = TLA + 0.25 \Delta T$	
Partially Insulated	Wv	9.635E-04					Average daily min. liquid surface temp.; Fig. 7.1-17 $TLN = TLA - 0.25 \Delta T$	
Fully Insulated	Wv	9.461E-04					Average daily ambient temperature range - Equation 1-11 ($\Delta TA = TAX - TAN$)	

Monthly Calculations - JANUARY

Tank No.	10456			ROUTINE EMISSIONS CALCULATIONS			Symbol			Units			HAPS Speciation			lb/month				
	ROUTINE EMISSIONS CALCULATIONS			Symbol	Units	ROUTINE EMISSIONS CALCULATIONS			Symbol	Units	HAPS Speciation			lb/month						
	LT	0.00	lb/month			Standing Losses; Eq. 1-2, $L_s = 365 (Vv \cdot Wv \cdot KE \cdot Ks)$	LS	0.00	lb/month			Total HAP Emissions =	0.000	Vapor Weight Concentration			Vapor Mole Fraction			
		2.33E-06	ton/month			Vapor Space Volume	Vv	37.7	ft ³			Eq. 40-2 $L_i = Z_{vi}(L_i)$	Eq. 40-6 $Zvi = y_i M_i / MV$			Eq. 40-5 $y_i = P_i / PVA$				
						Stock Vapor Density	Wv	0.0001	lb/ft ³			Individual HAPS	L_i (lb/month)	M	M_v	Z_{vi}	$P_i = PVA(K_i)$	P_{VA}	y_i	
						Vapor Space Expansion Factor ($0 < KE \leq 1$); Eq. 1-5	KE	0.020	per day			hexane	0.0000	86.18	130	0.00052	0.000002	0.002	0.00078	
						Vented Vapor Saturation Factor	Ks	1.00	NA			benzene	0.0000	78.11	130	0.00302	0.000015	0.002	0.00503	
						Constant Number of Daily Events in a Year	365	31	days/month			2,2,4 TMP	0.0000	114.23	130	0.00000	0.0000008	0.002	-	
						Working Losses; Eq. 1-35, $L_w = VO \cdot KN \cdot Kp \cdot Wv \cdot KB$	Lw	0.00	lb/month			toluene	0.0001	92.14	130	0.02475	0.0000085	0.002	0.03491	
						Net Working Loss Throughput (Eq. 1-39; $VQ=5.614 \cdot Q$)	VQ	55	ft ³ /month			ethylbenzene	0.0000	106.17	130	0.00280	0.0000008	0.002	0.00343	
						Working Loss Turnover Factor Eq. 1-35 $K_w = (180+N)/6N$ for $N \geq 36$, else $K_w = N$	KN	1.0000				xylene	0.0003	106.17	130	0.05394	0.000160	0.002	0.06605	
						Working Loss Product Factor	Kp	1.00				naphthalene	0.0000	128.17	130	2.72E-04	6.69E-07	0.002	2.76E-04	
						Stock Vapor Density	Wv	0.0001	lb/ft ³			cumene	0.0000	120.19	130	0.00E+00	0.00E+00	0.002	0.00E+00	
						Vent Setting Correction Factor	KB	1.00				Liquid Mole Fraction			Component Vapor Pressure					
						Vented Vapor Saturation Factor; Eq. 1-21, $K_s = 1/(1+0.053 \cdot PVA \cdot Hvo)$	Ks	1.00				Eq. 40-4 $x_i = (Z_{vi} M_i) / M_i$			PVA=(0.019337)10^4(A+B(TLA-C))					
						Vapor Pressure at Avg Daily Liq Surface Temp	PvA	0.0024	psia			Individual HAPS	Z_i	M_i	M_i	X_i	A	B	C	P_{VA}
						Vapor Space Outage	Hvo	0.00	ft			hexane	0.00000	188	86.18	0.00000	6.878	1171.5	224.37	0.8715
						Vapor Space Expansion Factor (Eq. 1-5; $(\Delta T_v/TLA) + ((\Delta P_v - \Delta P_B)/(PA - PVA))$)	KE	0.0199	per day			benzene	0.00001	188	78.11	0.00002	6.906	1211	220.79	0.5064
						Average Daily Vapor Temperature Range	ΔT_v	11.76	°R			2,2,4 TMP	0.00000	188	114.23	0.00000	6.812	1257.8	220.74	0.2495
						Average Daily Vapor Pressure Range	ΔP_v	0.0005	psia			toluene	0.00032	188	92.14	0.00065	7.017	1377.6	222.64	0.1296
						Breather Vent Pressure Setting Range (Equation 1-10; $\Delta P_B = PBP - PBV$)	PBP	0.0600	psi			ethylbenzene	0.00013	188	106.17	0.00223	6.95	1419.3	212.61	0.0361
						Vapor Pressure at Avg Daily Liq Surface Temp	PvA	0.0024	psia			xylene	0.00290	188	106.17	0.00514	7.009	1462.3	215.11	0.0312
						Average Daily Liquid Surface Temperature	TLA	491.45	°R			naphthalene	0.00076	188	128.17	0.01111	7.146	1831.6	211.82	0.0006
						Atmospheric Pressure	PA	14.69	psia			cumene	0.00000	188	120.19	0.00000	6.929	1455.8	207.2	0.0153
						Shell height	Hs	3.14	ft			Average Daily Vapor Temperature Range (ΔT_v)								
						Diameter	D	5.53	ft			Average daily ambient temperature range - Equation 1-11 ($\Delta T_A = TAX - TAA$)			ΔT_A					
						Throughput	Q	410	gal/month			Not Insulated - Equation 1-7 ($\Delta T_v = 0.7 \Delta T_A + 0.02 \sigma I$)			ΔT_v					
						Turnovers	N	8.56	per year			Partially Insulated - Equation 1-8 ($\Delta T_v = 0.6 \Delta T_A + 0.02 \sigma R I$)			ΔT_v					
						Roof Type		0.00				Fully Insulated, constant temperature			ΔT_v					
						Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft			Average Daily Vapor Pressure Range (ΔP_v)								
						Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA	ft			Not Insulated - Equation 1-9: $\Delta P_v = PVX - PVN$								
						Maximum Filling Height - use (Pi/4)D if unknown	HLX	2.14	ft			Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25 $PVX = \exp(\Delta P_v)$)								
						Minimum Filling Height (use 0 if unknown)	HLN	1.00	ft			Vapor pressure at ave daily min liquid surface temp. (Eq. 1-25 $PVN = \exp(-\Delta P_v)$)								
						Liquid height (assume 1/2 H)	HL	1.57	ft			Average daily max. liquid surface temp.; Fig. 7.1-17 $TLX = TLA + 0.25 \Delta T_v$								
						Tank Insulation (pick from drop down list)		Not Insulated				Average daily min. liquid surface temp.; Fig. 7.1-17 $TLN = TLA - 0.25 \Delta T_v$								
						Tank Construction (pick from drop down list)		Welded				Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25 us PVX)								
						Tank Shell Color (pick from drop down list)		White				Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25 us PVN)								
						Tank Shell Condition (pick from drop down list)		Average				Average daily maximum liquid surface temperature, deg R ($TLX = TLA + G \cdot TLN$)								
						Tank Interior Condition (pick from drop down list)		Light Rust				Fully Insulated ($\Delta P_v = 0$)								
						Tank paint solar absorptance, dimensionless, Table 7.1-6	σ	0.25				Average Daily Ambient Temperature (TAA) Eq. 1-30 $TAA = ((TAX + TAN) / 2)$								
						Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	0.03	psi			Average daily maximum ambient temperature, Table 7.1-7								
						True Vapor Pressure; Eq. 1-25, $PvA = \exp(A - (B/TLA))$						Average daily minimum ambient temperature, Table 7.1-7								
						Not Insulated	P_{VA}	0.0024228				Liquid Bulk Temperature; Eq. 1-31: $TB = TAA + 0.003 \sigma I$								
						Partially Insulated	P_{VA}	0.0024265				Average Daily Liquid Surface Temperature (TLA)								
						Fully Insulated	P_{VA}	0.0023756				Not Insulated; Eq. 1-28, $TLA = 0.4 \cdot TAA + 0.6 \cdot TB + 0.005 \cdot \sigma I$								
						Average Daily Ambient Temperature (TAA) Eq. 1-30 $TAA = ((TAX + TAN) / 2)$	TAA	490.50	°R			Partially Insulated; Eq. 1-29, $TLA = 0.3 \cdot TAA + 0.7 \cdot TB + 0.005 \cdot \sigma R I$								
						Average daily maximum ambient temperature, Table 7.1-7	TAX	496.90	°R			Fully Insulated; $TLA = TB$								
						Average daily minimum ambient temperature, Table 7.1-7	TAN	484.10	°R			Average Vapor Temperature (Tv)								
						Liquid Bulk Temperature; Eq. 1-31: $TB = TAA + 0.003 \sigma I$	TB	490.92	°R			Not Insulated; Eq. 1-33, $Tv = 0.7 \cdot TAA + 0.3 \cdot TB + 0.009 \cdot \sigma I$								
						Average Daily Liquid Surface Temperature (TLA)						Partially Insulated; Eq. 1-34, $Tv = 0.6 \cdot TAA + 0.4 \cdot TB + 0.01 \cdot \sigma R I$								
						Not Insulated; Eq. 1-28, $TLA = 0.4 \cdot TAA + 0.6 \cdot TB + 0.005 \cdot \sigma I$	TLA	491.45	°R			Fully Insulated; $Tv = TB$								
						Partially Insulated; Eq. 1-29, $TLA = 0.3 \cdot TAA + 0.7 \cdot TB + 0.005 \cdot \sigma R I$	TLA	491.49	°R			Stock Vapor Density; Eq. 1-22, $Wv = (Mv \cdot PVA) / (R \cdot Tv)$								
						Fully Insulated; $TLA = TB$	TLA	490.9	°R			Not Insulated								
						Average Vapor Temperature (Tv)						Partially Insulated								
						Not Insulated; Eq. 1-33, $Tv = 0.7 \cdot TAA + 0.3 \cdot TB + 0.009 \cdot \sigma I$	Tv	491.89	°R			Fully Insulated								
						Partially Insulated; Eq. 1-34, $Tv = 0.6 \cdot TAA + 0.4 \cdot TB + 0.01 \cdot \sigma R I$	Tv	492.07	°R											
						Fully Insulated; $Tv = TB$	Tv	490.92	°R											
						Stock Vapor Density; Eq. 1-22, $Wv = (Mv \cdot PVA) / (R \cdot Tv)$														
						Not Insulated	Wv	5.967E-05												
						Partially Insulated	Wv	5.974E-05												
						Fully Insulated	Wv	5.862E-05												

Monthly Calculations (continued)

Tank No.	10456			ROUTINE EMISSIONS CALCULATIONS			Symbol			Units			HAPS Speciation			lb/month				
	ROUTINE EMISSIONS CALCULATIONS			Symbol	Units	ROUTINE EMISSIONS CALCULATIONS			Symbol	Units	HAPS Speciation			lb/month						
	LT	0.01	lb/month			Standing Losses; Eq. 1-2, $L_s = 365 (Vv \cdot Wv \cdot KE \cdot Ks)$	LS	0.00	lb/month			Total HAP Emissions =	0.000	Vapor Weight Concentration			Vapor Mole Fraction			
		2.55E-06	ton/month			Vapor Space Volume	Vv	37.7	ft ³			Eq. 40-2 $L_i = Z_{vi}(L_i)$	Eq. 40-6 $Zvi = y_i M_i / MV$			Eq. 40-5 $y_i = P_i / PVA$				
						Stock Vapor Density	Wv	0.0001	lb/ft ³			Individual HAPS	L_i (lb/month)	M	M_v	Z_{vi}	$P_i = PVA(K_i)$	P_{VA}	y_i	
						Vapor Space Expansion Factor ($0 < KE \leq 1$); Eq. 1-5	KE	0.023	per day			hexane	0.0000	86.18	130	0.00051	0.000002	0.003	0.00077	
						Vented Vapor Saturation Factor	Ks	1.00	NA			benzene	0.0000	78.11	130	0.00299	0.000015	0.003	0.00498	
						Constant Number of Daily Events in a Year	365	28	days/month			2,2,4 TMP	0.0000	114.23	130	0.00000	0.0000008	0.003	-	
						Working Losses; Eq. 1-35, $L_w = VO \cdot KN \cdot Kp \cdot Wv \cdot KB$	Lw	0.00	lb/month			toluene	0.0001	92.14	130	0.02467	0.0000091	0.003	0.03481	
						Net Working Loss Throughput (Eq. 1-39; $VQ=5.614 \cdot Q$)	VQ	55	ft ³ /month			ethylbenzene	0.0000	106.17	130	0.00282	0.0000009	0.003	0.00345	
						Working Loss Turnover Factor Eq. 1-35 $K_w = (180+N)/6N$ for $N \geq 36$, else $K_w = N$	KN	1.0000				xylene	0.0003	106.17	130	0.05436	0.000175	0.003	0.06656	
						Working Loss Product Factor	Kp	1.00				naphthalene	0.0000	128.17	130	2.82E-04	7.50E-07	0.003	2.86E-04	
						Stock Vapor Density	Wv	0.0001	lb/ft ³			cumene	0.0000	120.19	130	0.00E+00	0.00E+00	0.003	0.00E+00	
						Vent Setting Correction Factor	KB	1.00				Liquid Mole Fraction			Component Vapor Pressure					
						Vented Vapor Saturation Factor; Eq. 1-21, $K_s = 1/(1+0.053 \cdot PVA \cdot Hvo)$	Ks	1.00				Eq. 40-4 $x_i = (Z_{vi} M_i) / M_i$			PVA=(0.019337)10^4(A+B(TLA-C))					
						Vapor Pressure at Avg Daily Liq Surface Temp	PvA	0.0026	psia			Individual HAPS	Z_i	M_i	M_i	X_i	A	B	C	P_{VA}
						Vapor Space Outage	Hvo	0.00	ft			hexane	0.00000	188	86.18	0.00000	6.878	1171.5	224.37	0.9299
						Vapor Space Expansion Factor (Eq. 1-5; $(\Delta T_v/TLA) + ((\Delta P_v - \Delta P_B)/(PA - PVA))$)	KE	0.0233	per day			benzene	0.00001	188	78.11	0.00002	6.906	1211	220.79	0.542

Monthly Calculations (continued)

SEPTEMBER

Tank No.	10456	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	HAPS Speciation	lb/month	Vapor Mole Fraction					
ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	HAPS Speciation		lb/month	Vapor Mole Fraction						
Total Losses (Eq. 1-1: LT = LS+LW)	LT	0.02	lb/month	Standing Losses; Eq. 1-2, $LS = 365 (V_v \cdot W_v \cdot KE \cdot K_s)$	LS	0.01	lb/month	Product		Diesel	Total HAP Emissions = 0.002						
Time Period	September	8.48E-06	ton/month	Vapor Space Volume	Vv	37.7	ft ³	Eq. 40-2 $L_i = z_i(L_i)$		Eq. 40-6 $ZV_i = y_iM_i / MV$		Eq. 40-5 $y_i = P_i / PVA$					
Nearest US Location	Bridgeport, CT			Stock Vapor Density	Wv	0.0002	lb/ft ³	Individual HAPS		hexane	0.0000	86.18	130	0.00040	0.000005	0.009	0.00061
Daily total solar insolation on a horizontal surface; Table 7.1-7	I	1320.0	Btu/ft ² -day	Vapor Space Expansion Factor ($0 < KE \leq 1$); Eq. 1-5	KE	0.028	per day	benzene	0.0000	78.11	130	0.00250	0.000036	0.009	0.00415		
Absolute Pressure	Pa	14.69	psi	Vented Vapor Saturation Factor	Ks	1.00	NA	toluene	0.0000	92.14	130	0.02323	0.000282	0.009	0.03277		
Ideal Gas Constant	R	10.73	psia ft ³ /lb-mole R	Constant Number of Daily Events in a Year	365	30	days/month	ethylbenzene	0.0001	106.17	130	0.00305	0.000032	0.009	0.00374		
Product Information				Working Losses; Eq. 1-35, $L_w = VO \cdot KN \cdot K_p \cdot W_v \cdot KB$	Lw	0.01	lb/month	xylene	0.0010	106.17	130	0.05948	0.000627	0.009	0.07283		
Product Type	Distillate Fuel Oil No.2			Net Working Loss Throughput (Eq. 1-39: $VO=5.614 \cdot Q$)	VO	55	ft ³ /month	naphthalene	0.0000	128.17	130	4.46E-04	3.89E-06	0.009	4.53E-04		
Vapor Molecular weight	Mv	130	lb/lb-mole	Working Loss Turnover Factor Eq. 1-35 $K_w=(180+N)/6N$ for N=36, else $K_w=KN$	KN	1.0000		cumene	0.0000	120.19	130	0.00E+00	0.00E+00	0.009	0.00E+00		
Average organic liquid density	WL	7.10	lb/gal	Working Loss Product Factor	Kp	1.00		Liquid Mole Fraction		Eq. 40-4 $x_i = (Z_iM_i) / \sum M_i$		Component Vapor Pressure		PV _{Ai} =(0.01937) ^{0.710} P _A ·(B·(TLA+C))			
Average Reid Vapor Pressure	RVP	0.02	psi	Stock Vapor Density	Wv	0.0002	lb/ft ³	hexane	0.00000	188	86.18	0.00000	6.878	1171.5	224.37	2.3895	
Product factor; 0.4 for crude oils or 1 for other organic liquids	Kc	1.00		Vent Setting Correction Factor	KB	1.00		benzene	0.00001	188	78.11	0.00002	6.906	1211	220.79	1.4842	
Vapor Pressure Equation Constant A	A	12.10		Vented Vapor Saturation Factor; Eq. 1-21, $K_s = 1/(1+0.053 \cdot PVA \cdot Hvo)$	Ks	1.00		toluene	0.00000	188	114.23	0.00000	6.812	1257.8	220.74	0.7627	
Vapor Pressure Equation Constant B (Table 7.1-2)	B	8907.0	R	Vapor Pressure at Avg Daily Liq Surface Temp	PvA	0.0086	psia	ethylbenzene	0.00013	188	106.17	0.00023	6.95	1419.3	212.61	0.1397	
				Vapor Space Outage	Hvo	0.00	ft	naphthalene	0.00076	188	128.17	0.00111	7.146	1831.6	211.82	0.0035	
								cumene	0.00000	188	120.19	0.00000	6.929	1455.8	207.2	0.0659	
Tank design data				Vapor Space Expansion Factor (Eq. 1-5: $(\Delta T_v/TLA) + (\Delta P_v - \Delta P_B)/(PA - PVA)$)	KE	0.0278	per day	Individual HAPS		Eq. 40-4 $x_i = (Z_iM_i) / \sum M_i$		Component Vapor Pressure		PV _{Ai} =(0.01937) ^{0.710} P _A ·(B·(TLA+C))			
Shell height	Hs	3.14	ft	Average Daily Vapor Temperature Range	ΔTv	16.75	°R	hexane	0.00000	188	86.18	0.00000	6.878	1171.5	224.37	2.3895	
Diameter	D	5.53	ft	Average Daily Vapor Pressure Range	ΔPv	0.0023	psi	benzene	0.00001	188	78.11	0.00002	6.906	1211	220.79	1.4842	
Throughput	Q	419	gal/month	Partially Insulated - Equation 1-7 ($\Delta T_v = 0.7 \Delta T_A + 0.02 \text{ or } 1$)	ΔTv	16.75	°R	toluene	0.00000	188	114.23	0.00000	6.812	1257.8	220.74	0.7627	
Turnovers	N	8.84	per year	Breather Vent Pressure Setting Range (Equation 1-10: $\Delta P_B = PBP - PBV$)	ΔPv	0.0023	psi	ethylbenzene	0.00013	188	106.17	0.00023	6.95	1419.3	212.61	0.1397	
Roof type		0.00		Vapor Pressure at Avg Daily Liq Surface Temp	PvA	0.0086	psia	naphthalene	0.00076	188	128.17	0.00111	7.146	1831.6	211.82	0.0035	
Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft	Average Daily Liquid Surface Temperature	TLA	528.39	°R	cumene	0.00000	188	120.19	0.00000	6.929	1455.8	207.2	0.0659	
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA	ft	Atmospheric Pressure	PA	14.69	psia	Liquid Mole Fraction		Eq. 40-4 $x_i = (Z_iM_i) / \sum M_i$		Component Vapor Pressure		PV _{Ai} =(0.01937) ^{0.710} P _A ·(B·(TLA+C))			
Maximum Filling Height -use (Pi/4)D if unknown	HLX	2.14	ft					hexane	0.00000	188	86.18	0.00000	6.878	1171.5	224.37	2.3895	
Minimum Filling Height (use 0 if unknown)	HLN	1.00	ft	Average Daily Vapor Temperature Range (ΔTv)	ΔTv	14.5	°R	benzene	0.00001	188	78.11	0.00002	6.906	1211	220.79	1.4842	
Liquid height (assume 1/2 H)	HL	1.57	ft	Average daily ambient temperature range - Equation 1-11 ($\Delta T_A = TAX - TA$)	ΔTA	14.5	°R	toluene	0.00000	188	114.23	0.00000	6.812	1257.8	220.74	0.7627	
Tank insulation (pick from drop down list)		Not Insulated		Partially Insulated - Equation 1-7 ($\Delta T_v = 0.7 \Delta T_A + 0.02 \text{ or } 1$)	ΔTv	16.75	°R	ethylbenzene	0.00013	188	106.17	0.00023	6.95	1419.3	212.61	0.1397	
Tank Construction (pick from drop down list)		Welded		Fully Insulated - Equation 1-8 ($\Delta T_v = 0.6 \Delta T_A + 0.02 \text{ or } 1$)	ΔTv	15.30	°R	naphthalene	0.00076	188	128.17	0.00111	7.146	1831.6	211.82	0.0035	
Tank Shell Color (pick from drop down list)		White		Fully Insulated, constant temperature	ΔTv	0.00	°R	cumene	0.00000	188	120.19	0.00000	6.929	1455.8	207.2	0.0659	
Tank Shell Condition (pick from drop down list)		Average						Liquid Mole Fraction		Eq. 40-4 $x_i = (Z_iM_i) / \sum M_i$		Component Vapor Pressure		PV _{Ai} =(0.01937) ^{0.710} P _A ·(B·(TLA+C))			
Tank Interior Condition (pick from drop down list)		Light Rust		Average Daily Vapor Pressure Range (ΔPv)	ΔPv	0.00230	psi	hexane	0.00000	188	86.18	0.00000	6.878	1171.5	224.37	2.3895	
Tank paint solar absorptance, dimensionless; Table 7.1-6	α	0.25		Not Insulated - Equation 1-9: $\Delta P_v = PVX - PVN$	ΔPv	0.00230	psi	benzene	0.00001	188	78.11	0.00002	6.906	1211	220.79	1.4842	
Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	0.03	psi	Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25 $PVX = \text{ex}$)	PvX	0.00862	psia	toluene	0.00000	188	106.17	0.00514	7.009	1462.3	215.11	0.1220	
		-0.03		Average daily max. liquid surface temp.; Fig. 7.1-17 $TLX = TLA + 0.25 \Delta T$	TLX	522.58	°R	ethylbenzene	0.00013	188	106.17	0.00023	6.95	1419.3	212.61	0.1397	
True Vapor Pressure; Eq. 1-25, $PvA = \text{exp}(A - (B/TLA))$				Average daily min. liquid surface temp.; Fig. 7.1-17 $TLN = TLA - 0.25 \Delta T$	TLN	524.21	°R	naphthalene	0.00076	188	128.17	0.00111	7.146	1831.6	211.82	0.0035	
Not Insulated	PvA	0.0086022						cumene	0.00000	188	120.19	0.00000	6.929	1455.8	207.2	0.0659	
Partially Insulated	PvA	0.0086294		Partially Insulated - Equation 1-9: $\Delta P_v = PVX - PVN$	ΔPv	0.00211	psi	hexane	0.00000	188	86.18	0.00000	6.878	1171.5	224.37	2.3895	
Fully Insulated	PvA	0.0082641		Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25 u)	PvX	0.00974	psia	benzene	0.00001	188	78.11	0.00002	6.906	1211	220.79	1.4842	
Average Daily Ambient Temperature (TAA) Eq. 1-30 $TAA = ((TAX+1)$	TAA	526.15	°R	Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25 u)	PvN	0.007617	psia	toluene	0.00000	188	114.23	0.00000	6.812	1257.8	220.74	0.7627	
Average daily maximum ambient temperature; Table 7.1-7	TAX	533.40	°R					ethylbenzene	0.00013	188	106.17	0.00023	6.95	1419.3	212.61	0.1397	
Average daily minimum ambient temperature; Table 7.1-7	TAN	518.90	°R					naphthalene	0.00076	188	128.17	0.00111	7.146	1831.6	211.82	0.0035	
								cumene	0.00000	188	120.19	0.00000	6.929	1455.8	207.2	0.0659	
Liquid Bulk Temperature; Eq. 1-31: $TB = TAA + 0.003 \text{ or } 1$	TB	527.14	°R	Fully Insulated (ΔPv = 0)	ΔPv	0.00	psi	Liquid Mole Fraction		Eq. 40-4 $x_i = (Z_iM_i) / \sum M_i$		Component Vapor Pressure		PV _{Ai} =(0.01937) ^{0.710} P _A ·(B·(TLA+C))			
Average Daily Liquid Surface Temperature (TLA)				Vapor Space Volume (Eq. 1-3: $Vv = ((\pi/4) D^2 H)vo$)	Vv	37.70	ft ³	hexane	0.00000	188	86.18	0.00000	6.878	1171.5	224.37	2.3895	
Not Insulated; Eq. 1-28, $TLA = 0.4 \cdot TAA + 0.6 \cdot TB + 0.005 \cdot \alpha \cdot I$	TLA	528.39	°R	Effective Tank diameter	D _e	5.53	ft	benzene	0.00001	188	78.11	0.00002	6.906	1211	220.79	1.4842	
Partially Insulated; Eq. 1-29, $TLA = 0.3 \cdot TAA + 0.7 \cdot TB + 0.005 \cdot \alpha \cdot R$	TLA	528.49	°R	Effective Tank Height	H _e	3.14	ft	toluene	0.00000	188	114.23	0.00000	6.812	1257.8	220.74	0.7627	
Fully Insulated; $TLA = TB$	TLA	527.1	°R	Vapor Space Outage $Hvo = 1/2 H$	Hvo	1.57	ft	ethylbenzene	0.00013	188	106.17	0.00023	6.95	1419.3	212.61	0.1397	
Average Vapor Temperature (Tv)								naphthalene	0.00076	188	128.17	0.00111	7.146	1831.6	211.82	0.0035	
Not Insulated; Eq. 1-33, $Tv = 0.7 \cdot TAA + 0.3 \cdot TB + 0.009 \cdot \alpha \cdot I$	Tv	529.42	°R					cumene	0.00000	188	120.19	0.00000	6.929	1455.8	207.2	0.0659	
Partially Insulated; Eq. 1-34, $Tv = 0.6 \cdot TAA + 0.4 \cdot TB + 0.01 \cdot \alpha \cdot R$	Tv	529.85	°R					Liquid Mole Fraction		Eq. 40-4 $x_i = (Z_iM_i) / \sum M_i$		Component Vapor Pressure		PV _{Ai} =(0.01937) ^{0.710} P _A ·(B·(TLA+C))			
Fully Insulated; $Tv = TB$	Tv	527.14	°R					hexane	0.00000	188	86.18	0.00000	6.878	1171.5	224.37	2.3895	
Stock Vapor Density; Eq. 1-22, $Wv = (Mv \cdot PvA) / (R \cdot Tv)$				Not Insulated - Equation 1-9: $\Delta P_v = PVX - PVN$	ΔPv	0.00150	psi	benzene	0.00001	188	78.11	0.00002	6.906	1211	220.79	1.4842	
Not Insulated	Wv	1.968E-04		Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25 $PVX = \text{ex}$)	PvX	0.00860	psia	toluene	0.00000	188	106.17	0.00514	7.009	1462.3	215.11	0.1220	
Partially Insulated	Wv	1.973E-04		Average daily max. liquid surface temp.; Fig. 7.1-17 $TLX = TLA + 0.25 \Delta T$	TLX	520.22	°R	ethylbenzene	0.00013	188	106.17	0.00023	6.95	1419.3	212.61	0.1397	
Fully Insulated	Wv	1.899E-04		Average daily min. liquid surface temp.; Fig. 7.1-17 $TLN = TLA - 0.25 \Delta T$	TLN	512.50	°R	naphthalene	0.00076	188	128.17	0.00111	7.146	1831.6	211.82	0.0035	
								cumene	0.00000	188	120.19	0.00000	6.929	1455.8	207.2	0.0659	

Monthly Calculations (continued)

OCTOBER

Tank No.	10456	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	HAPS Speciation	lb/month	Vapor Mole Fraction					
ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	HAPS Speciation		lb/month	Vapor Mole Fraction						
Total Losses (Eq. 1-1: LT = LS+LW)	LT	0.01	lb/month	Standing Losses; Eq. 1-2, $LS = 365 (V_v \cdot W_v \cdot KE \cdot K_s)$	LS	0.00	lb/month	Product		Diesel	Total HAP Emissions = 0.001						
Time Period	October	5.79E-06	ton/month	Vapor Space Volume	Vv	37.7	ft ³	Eq. 40-2 $L_i = z_i(L_i)$		Eq. 40-6 $ZV_i = y_iM_i / MV$		Eq. 40-5 $y_i = P_i / PVA$					
Nearest US Location	Bridgeport, CT			Stock Vapor Density	Wv	0.0001	lb/ft ³	Individual HAPS		hexane	0.0000	86.18	130	0.00044	0.000005	0.006	0.00066
Daily total solar insolation on a horizontal surface; Table 7.																	

Monthly Calculations (continued)

NOVEMBER

Tank No.	10456	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	HAPS Speciation	lb/month	Vapor Mole Fraction														
													Diesel													
													Total HAP Emissions = 0.001		Vapor Weight Concentration											
													Eq. 40-2 L ₁ = z ₁ (L ₁)		Eq. 40-5 y ₁ = P ₁ / PVA											
													Individual HAPS		L ₁ (lb/month)		M _v		Z ₁		P ₁ = P _{v,i} (K)		P _{v,i}		y _i	
Total Losses (Eq. 1-1: LT = LS+LW)	LT	0.01	lb/month			Standing Losses; Eq. 1-2, L _s = 365 (V _v * W _v * K _e * K _s)	Ls	0.00	lb/month			Eq. 40-6 ZV ₁ = y ₁ M ₁ / MV		Eq. 40-5 y ₁ = P ₁ / PVA												
Throughput	Q	3.87E-06	ton/month			Vapor Space Volume	Vv	37.7	ft ³																	
Nearest US Location						Stock Vapor Density	Wv	0.0001	lb/ft ³																	
Daily total solar insolation on a horizontal surface; Table 7.1-7	I	621.0	Btu/ft ² -day			Vapor Space Expansion Factor (0 < KE <= 1); Eq. 1-5	KE	0.021	per day																	
Absolute Pressure	P _a	14.69	psia			Vented Vapor Saturation Factor	Ks	1.00	NA																	
Ideal Gas Constant	R	10.73	psia ft ³ /lb-mole R			Constant Number of Daily Events in a Year	365	31	days/month																	
Product Information						Working Losses; Eq. 1-35, L _w = V _o * K _N * K _p * W _v * K _B	Lw	0.01	lb/month																	
Product Type	Distillate Fuel Oil No.2					Net Working Loss Throughput (Eq. 1-39: V _o =5.614*Q)	VO	55	ft ³ /month																	
Vapor Molecular weight	Mv	130	lb/lb-mole			Working Loss Turnover Factor Eq. 1-35 K _N =(180+N)/6N for N=36, else K _N =KN	KN	1.0000																		
Average organic liquid density	WL	7.10	lb/gal			Working Loss Product Factor	Kp	1.00																		
Average Reid Vapor Pressure	RVP	0.02	psia			Stock Vapor Density	Wv	0.0001	lb/ft ³																	
Product factor; 0.4 for crude oils or 1 for other organic liquids	Kc	1.00				Vent Setting Correction Factor	KB	1.00																		
Vapor Pressure Equation Constant A	A	12.10				Vented Vapor Saturation Factor; Eq. 1-21, K _s = 1/(1+0.053*PVA*Hvo)	Ks	1.00																		
Vapor Pressure Equation Constant B (Table 7.1-2)	B	8907.0	R			Vapor Pressure at Avg Daily Lq Surface Temp	PVA	0.0041	psia																	
						Vapor Space Outage	Hvo	0.00	ft																	
Tank design data						Vapor Space Expansion Factor (Eq. 1-5: (ΔT _v /TLA)+(ΔP _v -ΔPB)/(PA-PVA)	KE	0.0208	per day																	
Shell height	Hs	3.14	ft			Average Daily Vapor Temperature Range	ΔT _v	12.56	R																	
Diameter	D	5.53	ft			Average Daily Vapor Pressure Range	ΔP _v	0.0030	psia																	
Throughput	Q	4.10	gal/month			Breather Vent Pressure Setting Range (Equation 1-10: ΔPB = PBP - PBV)	PBP	0.0600	psi																	
Turnovers	N	8.84	per year			Vapor Pressure at Avg Daily Lq Surface Temp	PVA	0.0041	psia																	
Roof type		0.00				Average Daily Liquid Surface Temperature	TLA	506.41	R																	
Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft			Atmospheric Pressure	PA	14.69	psia																	
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA	ft			Average Daily Vapor Temperature Range (ΔT _v)	ΔT _v	13.5	R																	
Maximum Filling Height -use (Pi/4)D if unknown	HLX	2.14	ft			Not Insulated - Equation 1-7 (ΔT _v = 0.7 ΔT _A + 0.02 or I)	ΔT _v	12.56	R																	
Minimum Filling Height (use 0 if unknown)	HLN	1.00	ft			Partially Insulated - Equation 1-8 (ΔT _v = 0.6 ΔT _A + 0.02 or II)	ΔT _v	11.21	R																	
Liquid height (assume 1/2 H)	HL	1.57	ft			Fully Insulated, constant temperature	ΔT _v	0.00	R																	
Tank insulation (pick from drop down list)		Not Insulated				Average Daily Vapor Pressure Range (ΔP _v)	ΔP _v	0.00090	psia																	
Tank Construction (pick from drop down list)		Welded				Not Insulated - Equation 1-9: ΔP _v = P _{VX} - P _{VN}	ΔP _v	0.00090	psia																	
Tank Shell Color (pick from drop down list)		White				Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25 P _{VX} = ex P _{VN})	P _{VX}	0.00461	psia																	
Tank Shell Condition (pick from drop down list)		Average				Vapor pressure at ave daily min liquid surface temp. (Eq. 1-25 P _{VN} = ex P _{VN})	P _{VN}	0.00371	psia																	
Tank Interior Condition (pick from drop down list)		Light Rust				Average daily max. liquid surface temp.; Fig. 7.1-17 TLX = TLA + 0.25ΔT	TLX	509.54	R																	
Tank paint solar absorptance, dimensionless; Table 7.1-6	α	0.25				Average daily min. liquid surface temp.; Fig. 7.1-17 TLN = TLA - 0.25ΔT	TLN	503.27	R																	
Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	0.03	psi			Partially Insulated - Equation 1-9: ΔP _v = P _{VX} - P _{VN}	ΔP _v	0.00081	psia																	
True Vapor Pressure; Eq. 1-25, P _V A = exp(A-(B/TLA))						Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25 u _{P_{VX})}	P _{VX}	0.00457	psia																	
Not Insulated	P _V A	0.0041375				Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25 u _{P_{VN})}	P _{VN}	0.003780	psia																	
Partially Insulated	P _V A	0.0041442				Average daily maximum liquid surface temperature, deg R (TLX = TLA + TLX)	TLX	509.25	R																	
Fully Insulated	P _V A	0.0040535				Average daily minimum liquid surface temperature, deg R (TLN = TLA - TLN)	TLN	503.65	R																	
Average Daily Ambient Temperature (TAA) Eq. 1-30 TAA = ((TAX+1)	TAA	505.35	R			Fully Insulated (ΔP _v = 0)	ΔP _v	0.00	psia																	
Average daily maximum ambient temperature, Table 7.1-7	TAX	512.10	R			Vapor Space Volume (Eq. 1-3: V _v = ((Pi / 4) D ² H)vo	Vv	37.70	ft ³																	
Average daily minimum ambient temperature, Table 7.1-7	TAN	498.60	R			Effective Tank diameter	D _e	5.53	ft																	
Liquid Bulk Temperature; Eq. 1-31: TB = TAA + 0.003 as I	TB	505.82	R			Effective Tank Height	H _e	3.14	ft																	
Average Daily Liquid Surface Temperature (TLA)						Vapor Space Outage Hvo = 1/2 H	Hvo	1.57	ft																	
Not Insulated; Eq. 1-28, TLA = 0.4*TAA + 0.6*TB + 0.005*α ¹	TLA	506.41	R																							
Partially Insulated; Eq. 1-29, TLA = 0.3*TAA + 0.7*TB + 0.005*α ¹	TLA	506.45	R																							
Fully Insulated; TLA = TB	TLA	505.8	R																							
Average Vapor Temperature (Tv)																										
Not Insulated; Eq. 1-33, Tv = 0.7*TAA + 0.3*TB + 0.009*α ¹	Tv	506.89	R																							
Partially Insulated; Eq. 1-34, Tv = 0.6*TAA + 0.4*TB + 0.01*α ¹	Tv	507.09	R																							
Fully Insulated; Tv = TB	Tv	505.82	R																							
Stock Vapor Density; Eq. 1-22, Wv = (Mv/PVA)/(R*Tv)																										
Not Insulated	Wv	9.888E-05																								
Partially Insulated	Wv	9.901E-05																								
Fully Insulated	Wv	9.708E-05																								

Monthly Calculations (continued)

DECEMBER

Tank No.	10456	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	HAPS Speciation	lb/month	Vapor Mole Fraction														
													Diesel													
													Total HAP Emissions = 0.000		Vapor Weight Concentration											
													Eq. 40-2 L ₁ = z ₁ (L ₁)		Eq. 40-5 y ₁ = P ₁ / PVA											
													Individual HAPS		L ₁ (lb/month)		M _v		Z ₁		P ₁ = P _{v,i} (K)		P _{v,i}		y _i	
Total Losses (Eq. 1-1: LT = LS+LW)	LT	0.01	lb/month			Standing Losses; Eq. 1-2, L _s = 365 (V _v * W _v * K _e * K _s)	Ls	0.00	lb/month			Eq. 40-6 ZV ₁ = y ₁ M ₁ / MV		Eq. 40-5 y ₁ = P ₁ / PVA												
Throughput	Q	2.71E-06	ton/month			Vapor Space Volume	Vv	37.7	ft ³																	
Nearest US Location						Stock Vapor Density	Wv	0.0001	lb/ft ³																	
Daily total solar insolation on a horizontal surface; Table 7.1-7	I	501.0	Btu/ft ² -day			Vapor Space Expansion Factor (0 < KE <= 1); Eq. 1-5	KE	0.019	per day																	
Absolute Pressure	P _a	14.69	psia			Vented Vapor Saturation Factor	Ks	1.00	NA																	
Ideal Gas Constant	R	10.73	psia ft ³ /lb-mole R			Constant Number of Daily Events in a Year	365	31	days/month																	
Product Information						Working Losses; Eq. 1-35, L _w = V _o * K _N * K _p * W _v * K _B	Lw	0.00	lb/month																	
Product Type	Distillate Fuel Oil No.2					Net Working Loss Throughput (Eq. 1-39: V _o =5.614*Q)	VO	55	ft ³ /month																	
Vapor Molecular weight	Mv	130	lb/lb-mole			Working Loss Turnover Factor Eq. 1-35 K _N =(180+N)/6N for N=36, else K _N =KN	KN	1.0000																		
Average organic liquid density	WL	7.10	lb/gal			Working Loss Product Factor	Kp	1.00																		
Average Reid Vapor Pressure	RVP	0.02	psia			Stock Vapor Density	Wv	0.0001	lb/ft ³																	
Product factor; 0.4 for crude oils or 1 for other organic liquids	Kc	1.00				Vent Setting Correction Factor	KB	1.00																		
Vapor Pressure Equation Constant A	A	12.10				Vented Vapor Saturation Factor; Eq. 1-21, K _s = 1/(1+0.053*PVA*Hvo)	Ks	1.00																		
Vapor Pressure Equation Constant B (Table 7.1-2)	B	8907.0	R			Vapor Pressure at Avg Daily Lq Surface Temp	PVA	0.0029	psia																	
						Vapor Space Outage	Hvo	0.00	ft																	
Tank design data						Vapor Space Expansion Factor (Eq. 1-5: (ΔT _v /TLA)+(ΔP _v -ΔPB)/(PA-PVA)	KE	0.0188	per day																	
Shell height	Hs	3.14	ft			Average Daily Vapor Temperature Range	ΔT _v	11.33	R																	
Diameter	D	5.53	ft			Average Daily Vapor Pressure Range	ΔP _v	0.0006	psia																	
Throughput	Q	4.10	gal/month			Breather Vent Pressure Setting Range (Equation 1-10: ΔPB = PBP - PBV)	PBP	0.0600	psi																	

Monthly Calculations - JANUARY

Tank No.	10457			FEBRUARY			ROUTINE EMISSIONS CALCULATIONS			Symbol			Units			HAPS Speciation			lb/month			additive																				
	ROUTINE EMISSIONS CALCULATIONS			Symbol	Units	ROUTINE EMISSIONS CALCULATIONS			Symbol	Units	HAPS Speciation			lb/month			additive																									
	Total Losses (Eq. 1-1: $LT = LS + LW$)			LT	0.95	lb/month	Standing Losses; Eq. 1-2: $LS = 365 (Vv \cdot Wv \cdot KE \cdot Ks)$			LS	0.26	lb/month	Product			Total HAP Emissions = 0.953			Vapor Weight Concentration			Vapor Mole Fraction																				
	Daily total solar insolation on a horizontal surface; Table 7.1-7			I	560.0	Btu/ft ² -day	Vapor Space Volume			Vv	536.2	ft ³	Eq. 40-2: $L_{ij} = Z_{ij}(L_i)$			Eq. 40-6: $Z_i V_i = y_i M_i / M_v$			Eq. 40-5: $y_i = P_i / P_{VA}$																							
	Nearest US Location			I	Bridgeport, CT		Stock Vapor Density			Wv	0.0008	lb/ft ³	Individual HAPS			hexane			0.0000			0.000000			0.032																	
	Absolute Pressure			P _a	14.69	psi	Vapor Space Expansion Factor (0 < KE ≤ 1); Eq. 1-5			KE	0.020	per day	benzene			0.0000			78.11			0.00000			0.000000			0.032														
	Ideal Gas Constant			R	10.73	psia ft ³ /lb-mole R	Constant; Number of Daily Events in a Year			365	31	days/month	2,2,4 TMP			toluene			0.0000			92.14			0.00000			0.000000			0.032											
	Product Information						Working Losses; Eq. 1-35: $L_w = VQ \cdot KN \cdot Kp \cdot Wv \cdot KB$			LW	0.69	lb/month	ethylbenzene			0.2794			106.17			130			0.29329			0.011655			0.032											
	Product Type			Diesel Additive			Net Working Loss Throughput (Eq. 1-39: $VQ = 5.614 \cdot Q$)			VQ	862	ft ³ /month	xylene			0.6733			106.17			130			0.70671			0.028084			0.032											
	Average organic liquid density			WL	6.10	lb/gal	Working Loss Turnover Factor Eq. 1-35: $K_w = (180 + N)/6N$ for N>36, else $K_w = 1$			KN	1.0000		naphthalene			0.0000			128.17			130			0.00E+00			0.00E+00			0.032											
	Average Reid Vapor Pressure			RVP	0.00	psi	Stock Vapor Density			Wv	0.0008	lb/ft ³	cumene			0.0000			120.19			130			0.00E+00			0.00E+00			0.032											
	Product factor; 0.4 for crude oils or 1 for other organic liquids			Kc	1.00		Vent Setting Correction Factor			KB	1.00		Liquid Mole Fraction			Eq. 40-4: $x_i = (Z_i M_i) / \sum (Z_i M_i)$			Component Vapor Pressure			Eq. 40-3: $P_{VA} = (0.019337)^{0.71} (P_A \cdot B) / (TLA \cdot C)$			A			B			C			P _{VA}								
	Vapor Pressure Equation Constant A			A	0.00		Vent Vapor Saturation Factor; Eq. 1-21: $K_s = 1 / (1 + 0.053 \cdot P_{VA} \cdot H_v)$			Ks	1.00		hexane			0.00000			130			86.18			0.00000			6.878			1171.5			224.37			0.8715					
	Vapor Pressure Equation Constant B (Table 7.1-2)			B	0.0	R	Vapor Pressure at Avg Daily Liq Surface Temp			P _{vA}	0.0325	psia	benzene			0.00000			130			78.11			0.00000			6.906			1211			220.79			0.5064					
	Tank design data						Vapor Space Outage			Hvo	0.00	ft	2,2,4 TMP			toluene			0.00000			130			114.23			0.00000			6.812			1257.8			220.74			0.2495		
	Shell height			Hs	6.28	ft	Vapor Space Expansion Factor (Eq. 1-5: $(\Delta T_v / TLA) \cdot [(APV - APB) / (PA - PVA)]$)			KE	0.0198	per day	ethylbenzene			0.00000			130			92.14			0.00000			7.017			1377.6			222.64			0.1296					
	Diameter			D	14.74	ft	Average Daily Vapor Temperature Range			ΔT _v	11.76	°R	benzene			0.26400			130			106.17			0.32326			6.95			1419.3			212.61			0.0361					
	Throughput			Q	6.450	gal/month	Average Daily Vapor Pressure Range			ΔP _v	0.0000	psi	2,2,4 TMP			toluene			0.00000			130			114.23			0.00000			6.812			1257.8			220.74			0.2495		
	Turnovers			N	9.47	per year	Breather Vent Pressure Setting Range (Equation 1-10: $\Delta P_B = P_B - P_{BV}$)			ΔP _B	0.0600	psi	xylene			0.73600			130			106.17			0.90120			7.009			1462.3			215.11			0.0312					
	Roof Type			0.00			Vapor Pressure at Avg Daily Liq Surface Temp			P _{vA}	0.0325	psia	naphthalene			0.00000			130			128.17			0.00000			7.148			1831.6			211.82			0.0006					
	Tank Cone Roof Slope (If unknown, use 0.0625)			SR	0.0625	ft/ft	Average Daily Liquid Surface Temperature			TLA	491.45	°R	cumene			0.00000			130			120.19			0.00000			6.929			1455.8			207.2			0.0153					
	Dome Roof Radius (If unknown, use tank diameter (D) or (2R _s))			RR	NA	ft	Atmospheric Pressure			P _a	14.69	psia																														
	Maximum Filling Height - use (Pi/4)D if unknown			HLX	5.28	ft																																				
	Minimum Filling Height (use 0 if unknown)			HLN	1.00	ft	Average Daily Vapor Temperature Range (ΔT _v)			ΔT _v	12.8	°R																														
	Liquid height (assume 1/2 H)			HL	3.14	ft	Not Insulated - Equation 1-7 (ΔT _v = 0.7 ΔT _A + 0.02 q _R)			ΔT _v	11.76	°R																														
	Tank Insulation (pick from drop down list)			Not Insulated			Partially Insulated - Equation 1-8 (ΔT _v = 0.6 ΔT _A + 0.02 q _R)			ΔT _v	10.48	°R																														
	Tank Construction (pick from drop down list)			Welded			Fully Insulated, constant temperature			ΔT _v	0.00	°R																														
	Tank Shell Color (pick from drop down list)			White																																						
	Tank Shell Condition (pick from drop down list)			Average																																						
	Tank Interior Condition (pick from drop down list)			Light Rust			Average Daily Vapor Pressure Range (ΔP _v)			ΔP _v	0.00000	psia																														
	Tank paint solar absorptance, dimensionless; Table 7.1-6			α	0.25		Not Insulated - Equation 1-9: ΔP _v = P _{VX} - P _{VN}			ΔP _v	0.00000	psia																														
	Breather Vent Setting Range (Default Assumption: +/- 0.03)			PBP	0.03	psi	Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25: P _{VX} = ex ^{ΔT_v})			P _{VX}	1.00000	psia																														
	Breather Vent Setting Range (Default Assumption: +/- 0.03)			PBP	-0.03	psi	Vapor pressure at ave. daily min liquid surface temp. (Eq. 1-25: P _{VN} = ex ^{-ΔT_v})			P _{VN}	1.00000	psia																														
	True Vapor Pressure; Eq. 1-25: $P_{vA} = \exp(A - (B/TLA))$						Average daily max. liquid surface temp.; Fig. 7.1-17: $TLX = TLA + 0.25 \Delta T_v$			TLX	494.39	°R																														
	Not Insulated			P _{vA}	0.032455		Average daily min. liquid surface temp.; Fig. 7.1-17: $TLN = TLA - 0.25 \Delta T_v$			TLN	488.51	°R																														
	Partially Insulated			P _{vA}	0.0325101																																					
	Fully Insulated			P _{vA}	0.031764		Partially Insulated - Equation 1-9: ΔP _v = P _{VX} - P _{VN}			ΔP _v	0.00000	psia																														
	Average Daily Ambient Temperature (TAA) Eq. 1-30: $TAA = ((TAX + TAN) / 2)$			TAA	490.50	°R	Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25: P _{VX})			P _{VX}	1.00000	psia																														
	Average daily maximum ambient temperature; Table 7.1-7			TAX	496.90	°R	Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25: P _{VN})			P _{VN}	1.000000	psia																														
	Average daily minimum ambient temperature; Table 7.1-7			TAN	484.10	°R	Average daily maximum liquid surface temperature, deg R (TLX = TLA + TLX)			TLX	494.11	°R																														
	Average daily minimum liquid surface temperature; Table 7.1-7			TAN	484.10	°R	Average daily minimum liquid surface temperature, deg R (TLN = TLA - TLN)			TLN	488.87	°R																														
	Liquid Bulk Temperature; Eq. 1-31: $T_B = TAA + 0.003 \text{ as l}$			TB	490.92	°R	Fully Insulated (ΔP _v = 0)			ΔP _v	0.00	psia																														
	Average Daily Liquid Surface Temperature (TLA)						Vapor Space Volume (Eq. 1-3: $V_v = ((\pi/4) D^2 H_v)$)			Vv	536.17	ft ³																														
	Not Insulated; Eq. 1-28: $TLA = 0.4 \cdot TAA + 0.6 \cdot TB + 0.005 \cdot q \cdot I$			TLA	491.45	°R	Effective Tank diameter			D _e	14.74	ft																														
	Partially Insulated; Eq. 1-29: $TLA = 0.3 \cdot TAA + 0.7 \cdot TB + 0.005 \cdot q \cdot R$			TLA	491.49	°R	Effective Tank Height			H _e	6.28	ft																														
	Fully Insulated; TLA = TB			TLA	490.9	°R	Vapor Space Outage Hvo = 1/2 H			Hvo	3.14	ft																														
	Average Vapor Temperature (T _v)																																									
	Not Insulated; Eq. 1-33: $T_v = 0.7 \cdot TAA + 0.3 \cdot TB + 0.009 \cdot q \cdot I$			Tv	491.89	°R																																				
	Partially Insulated; Eq. 1-34: $T_v = 0.6 \cdot TAA + 0.4 \cdot TB + 0.01 \cdot q \cdot R$			Tv	492.07	°R																																				
	Fully Insulated; T _v = TB			Tv	490.92	°R																																				
	Stock Vapor Density; Eq. 1-22: $W_v = (M_v \cdot P_{vA}) / (R \cdot T_v)$																																									
	Not Insulated			Wv	7.993E-04																																					
	Partially Insulated			Wv	8.004E-04																																					
	Fully Insulated			Wv	7.838E-04																																					

Monthly Calculations (continued)

Tank No.	10457			FEBRUARY			ROUTINE EMISSIONS CALCULATIONS			Symbol			Units			HAPS Speciation			lb/month			additive											
	ROUTINE EMISSIONS CALCULATIONS			Symbol	Units	ROUTINE EMISSIONS CALCULATIONS			Symbol	Units	HAPS Speciation			lb/month			additive																
	Total Losses (Eq. 1-1: $LT = LS + LW$)			LT	1.05	lb/month	Standing Losses; Eq. 1-2: $LS = 365 (Vv \cdot Wv \cdot KE \cdot Ks)$			LS	0.30	lb/month	Product			Total HAP Emissions = 1.051			Vapor Weight Concentration			Vapor Mole Fraction											
	Daily total solar insolation on a horizontal surface; Table 7.1-7			I	567.0	Btu/ft ² -day	Vapor Space Volume			Vv	536.2	ft ³	Eq. 40-2: $L_{ij} = Z_{ij}(L_i)$			Eq. 40-6: $Z_i V_i = y_i M_i / M_v$			Eq. 40-5: $y_i = P_i / P_{VA}$														
	Nearest US Location			I	Bridgeport, CT		Stock Vapor Density			Wv	0.0009	lb/ft ³	Individual HAPS			hexane			0.0000			0.000000			0.035								
	Absolute Pressure			P _a	14.69	psi	Vapor Space Expansion Factor (0 < KE ≤ 1); Eq. 1-5			KE	0.023	per day	benzene			0.0000			78.11			0.00000			0.035								
	Ideal Gas Constant			R	10.73	psia ft ³ /lb-mole R	Constant; Number of Daily Events in a Year			365	28	days/month	2,2,4 TMP			toluene			0.0000			92.14			0.00000			0.000000			0.035		
	Product Information						Working Losses; Eq. 1-35: $L_w = VQ \cdot KN \cdot Kp \cdot Wv \cdot KB$			LW	0.75	lb/month	ethylbenzene			0.3082			106.17			130			0.29318			0.012721			0.035		
	Product Type			Diesel Additive			Net Working Loss Throughput (Eq. 1-39: $VQ = 5.614 \cdot Q$)			VQ	862	ft ³ /month	xylene			0.7431			106.17			130			0.70682			0.030669			0.035		
	Average organic liquid density			WL	6.10	lb/gal	Working Loss Turnover Factor Eq. 1-35: $K_w = (180 + N)/6N$ for N>36, else $K_w = 1$			KN	1.0000		naphthalene			0.0000			128.17			130			0.00E+00			0.035					
	Average Reid Vapor Pressure			RVP	0.00	psi	Stock Vapor Density			Wv	0.0009	lb/ft ³	cumene			0.0000			120.19			130			0.00E+00			0.035					
	Product factor; 0.4 for crude oils or 1 for other organic liquids			Kc	1.00		Vent Setting Correction Factor			KB	1.00		Liquid Mole Fraction			Eq. 40-4: $x_i = (Z_i M_i) / \sum (Z_i$																	

Monthly Calculations (continued)

MAY

Tank No.	ROUTINE EMISSIONS CALCULATIONS		ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	HAPS Speciation		Product	lb/month	addl/vol		
	Symbol	Units	Symbol	Units			Product	lb/month									
	LT	3.31	lb/month	Vapor Space Volume	Vv	536.2	ft ³	Total HAP Emissions =	3.313	Vapor Weight Concentration	Eq. 40-6 Zvi = yiMi / MV	Vapor Mole Fraction	Eq. 40-5 yi = Pi / PVA				
		1.66E-03	ton/month	Stock Vapor Density	Wv	0.0023	lb/ft ³	Eq. 40-2 L _{ij} = Zi _{ij} (L _i)		Individual HAPS	L _{ij} (lb/month)	M _i	M _v	Z _{vi}	P _i = P _{VA} (X _i)	P _{VA}	y _i
	Time Period	May		Vapor Space Expansion Factor (0 < KE <= 1); Eq. 1-5	KE	0.034	per day	Eq. 40-5 yi = Pi / PVA		hexane	0.0000	86.18	130	0.00000	0.000000	0.101	-
	Nearest US Location	Bridgeport, CT		Vented Vapor Saturation Factor	Ks	1.00	NA	Constant: Number of Daily Events in a Year	365	benzene	0.0000	78.11	130	0.00000	0.000000	0.101	-
	Daily total solar insolation on a horizontal surface; Table 7.1-7	I	1750.0	Working Losses; Eq. 1-35, Lw = VQ * KN * Kp * Wv * KB	Lw	2.01	lb/month	Eq. 1-39: VQ=(5.614*Q)		2,2,4 TMP	0.0000	114.23	130	0.00000	0.000000	0.101	-
	Absolute Pressure	Pa	14.89	Net Working Loss Throughput (Eq. 1-39: VQ=(5.614*Q))	VQ	862	ft ³ /month	Eq. 1-35, Lw = VQ * KN * Kp * Wv * KB		toluene	0.0000	92.14	130	0.00000	0.000000	0.101	-
	Ideal Gas Constant	R	10.73	Working Loss Turnover Factor Eq 1-35 K _w =(180+N)/6N for N>=36, else K _w =N	KN	1.0000		Net Working Loss Throughput (Eq. 1-39: VQ=(5.614*Q))		ethylbenzene	0.9659	106.17	130	0.29159	0.035886	0.101	0.35704
	Product Information			Working Loss Product Factor	Kp	1.00		Working Loss Turnover Factor Eq 1-35 K _w =(180+N)/6N for N>=36, else K _w =N		xylene	2.3467	106.17	130	0.70841	0.087184	0.101	0.86742
	Product Type	Diesel Additive		Stock Vapor Density	Wv	0.0023	lb/ft ³	Working Loss Product Factor	Kp	1.00					0.00E+00	0.101	0.00E+00
	Vapor Molecular weight	Mv	130	Vent Setting Correction Factor	KB	1.00		Stock Vapor Density	Wv	0.0023	lb/ft ³			0.00E+00	0.101	0.00E+00	
	Average organic liquid density	WL	6.10	Vented Vapor Saturation Factor; Eq. 1-21, Ks = 1/(1+0.053*PVA*Hvo)	Ks	1.00		Vent Setting Correction Factor	KB	1.00				0.00E+00	0.101	0.00E+00	
	Average Reid Vapor Pressure	RVP	0.00	Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.1005	psia	Vented Vapor Saturation Factor; Eq. 1-21, Ks = 1/(1+0.053*PVA*Hvo)	Ks	1.00				0.00E+00	0.101	0.00E+00	
	Product factor; 0.4 for crude oils or 1 for other organic liquids	Kc	1.00	Vapor Space Outage	Hvo	0.00	ft	Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.1005	psia			0.00E+00	0.101	0.00E+00	
	Vapor Pressure Equation Constant A	A	0.00	Vapor Space Expansion Factor (Eq. 1-5: (ΔT _v /TLA)-((ΔP _v -ΔPB)/(PA-PVA))	KE	0.0337	per day	Vapor Space Outage	Hvo	0.00	ft			0.00E+00	0.101	0.00E+00	
	Vapor Pressure Equation Constant B (Table 7.1-2)	B	0.0	Average Daily Vapor Temperature Range (ΔT _v)	ΔT _v	19.74	°R	Vapor Space Expansion Factor (Eq. 1-5: (ΔT _v /TLA)-((ΔP _v -ΔPB)/(PA-PVA))	KE	0.0337	per day			0.00E+00	0.101	0.00E+00	
	Tank design data			Average Daily Vapor Pressure Range	ΔP _v	0.0000	psia	Average Daily Vapor Temperature Range (ΔT _v)	ΔT _v	19.74	°R			0.00E+00	0.101	0.00E+00	
	Shell height	Hs	6.28	Not Insulated - Equation 1-7 (ΔT _v = 0.7 ΔT _A + 0.02 α I)	ΔT _v	18.74	°R	Average Daily Vapor Pressure Range	ΔP _v	0.0000	psia			0.00E+00	0.101	0.00E+00	
	Diameter	D	14.74	Partially Insulated - Equation 1-8 (ΔT _v = 0.6 ΔT _A + 0.02 α R I)	ΔT _v	18.17	°R	Not Insulated - Equation 1-9: ΔP _v = P _{VX} - P _{VN}	ΔP _v	0.00000	psia			0.00E+00	0.101	0.00E+00	
	Throughput	Q	6,450	Fully Insulated, constant temperature	ΔT _v	0.00	°R	Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25 P _{VX} = exP _{VN})	P _{VX}	1.00000	psia			0.00E+00	0.101	0.00E+00	
	Turnovers	N	9.47	Average Daily Vapor Pressure Range (ΔP _v)	ΔP _v	0.00000	psia	Vapor pressure at ave. daily min liquid surface temp. (Eq. 1-25 P _{VN} = exP _{VN})	P _{VN}	1.00000	psia			0.00E+00	0.101	0.00E+00	
	Roof Type:			Not Insulated - Equation 1-9: ΔP _v = P _{VX} - P _{VN}	ΔP _v	0.00000	psia	Breather Vent Pressure Setting Range (Equation 1-10: ΔPB = PBP - PBPB)	ΔPB	0.0600	psi			0.00E+00	0.101	0.00E+00	
	Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25 u _{PVX})	P _{VX}	0.10000	psia	Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.1005	psia			0.00E+00	0.101	0.00E+00	
	Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA	Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25 u _{PVN})	P _{VN}	0.10000	psia	Average Daily Liquid Surface Temperature	TLA	521.63	°R			0.00E+00	0.101	0.00E+00	
	Maximum Filling Height -use (Pi/4)D if unknown	HLX	5.28	Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25 u _{PVX})	P _{VX}	0.10000	psia	Average Daily Liquid Surface Temperature	TLA	521.63	°R			0.00E+00	0.101	0.00E+00	
	Minimum Filling Height (use 0 if unknown)	HLN	1.00	Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25 u _{PVN})	P _{VN}	0.10000	psia	Atmospheric Pressure	PA	14.69	psia			0.00E+00	0.101	0.00E+00	
	Liquid height (assume 1/2 H)	HL	3.14	Fully Insulated (ΔP _v = 0)	ΔP _v	0.00	psia	Average Daily Vapor Temperature Range (ΔT _v)	ΔT _v	15.7	°R			0.00E+00	0.101	0.00E+00	
	Tank insulation (pick from drop down list)		Not Insulated	Vapor Space Volume (Eq. 1-3: Vv = ((Pi/4) D ² H)vo)	Vv	536.17	ft ³	Average daily ambient temperature range - Equation 1-11 (ΔTA=TAX-TA)	ΔTA	15.7	°R			0.00E+00	0.101	0.00E+00	
	Tank Construction (pick from drop down list)		Welded	Effective Tank diameter	D _e	14.74	ft	Partially Insulated - Equation 1-7 (ΔT _v = 0.7 ΔT _A + 0.02 α I)	ΔT _v	18.74	°R			0.00E+00	0.101	0.00E+00	
	Tank Shell Color (pick from drop down list)		White	Effective Tank Height	H _e	6.28	ft	Partially Insulated - Equation 1-8 (ΔT _v = 0.6 ΔT _A + 0.02 α R I)	ΔT _v	18.17	°R			0.00E+00	0.101	0.00E+00	
	Tank Shell Condition (pick from drop down list)		Average	Vapor Space Outage Hvo = 1/2 H	Hvo	3.14	ft	Fully Insulated, constant temperature	ΔT _v	0.00	°R			0.00E+00	0.101	0.00E+00	
	Tank Interior Condition (pick from drop down list)		Light Rust					Average Daily Vapor Pressure Range (ΔP _v)	ΔP _v	0.00000	psia			0.00E+00	0.101	0.00E+00	
	Tank paint solar absorptance, dimensionless; Table 7.1-6	α	0.25					Not Insulated - Equation 1-9: ΔP _v = P _{VX} - P _{VN}	ΔP _v	0.00000	psia			0.00E+00	0.101	0.00E+00	
	Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	0.03					Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25 P _{VX} = exP _{VN})	P _{VX}	1.00000	psia			0.00E+00	0.101	0.00E+00	
	True Vapor Pressure; Eq. 1-25, P _V A = exp(A-(B/TLA))							Vapor pressure at ave. daily min liquid surface temp. (Eq. 1-25 P _{VN} = exP _{VN})	P _{VN}	1.00000	psia			0.00E+00	0.101	0.00E+00	
	Not Insulated	P _V A	0.1005102					Average daily max. liquid surface temp.; Fig. 7.1-17 TLX = TLA + 0.25ΔT TLX	TLX	526.56	°R			0.00E+00	0.101	0.00E+00	
	Partially Insulated	P _V A	0.1009694					Average daily min. liquid surface temp.; Fig. 7.1-17 TLN = TLA - 0.25ΔT TLN	TLN	516.69	°R			0.00E+00	0.101	0.00E+00	
	Fully Insulated	P _V A	0.0948467					Partially Insulated - Equation 1-9: ΔP _v = P _{VX} - P _{VN}	ΔP _v	0.00000	psia			0.00E+00	0.101	0.00E+00	
	Average Daily Ambient Temperature (TAA) Eq. 1-30 TAA = ((TAX+TAN)/2)	TAA	518.65					Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25 u _{PVX})	P _{VX}	1.00000	psia			0.00E+00	0.101	0.00E+00	
	Average daily maximum ambient temperature; Table 7.1-7	TAX	526.50					Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25 u _{PVN})	P _{VN}	1.00000	psia			0.00E+00	0.101	0.00E+00	
	Average daily minimum ambient temperature; Table 7.1-7	TAN	510.80					Average daily maximum liquid surface temperature, deg R (TLX = TLA + TLX)	TLX	526.30	°R			0.00E+00	0.101	0.00E+00	
	Liquid Bulk Temperature; Eq 1-31: TB = TAA + 0.003 α s I	TB	519.96					Average daily minimum liquid surface temperature, deg R (TLN = TLA - TLN)	TLN	517.21	°R			0.00E+00	0.101	0.00E+00	
	Average Daily Liquid Surface Temperature (TLA)							Fully Insulated (ΔP _v = 0)	ΔP _v	0.00	psia			0.00E+00	0.101	0.00E+00	
	Not Insulated; Eq. 1-28, TLA = 0.4*TAA + 0.6*TB + 0.005*α*I	TLA	521.63					Vapor Space Volume (Eq. 1-3: Vv = ((Pi/4) D ² H)vo)	Vv	536.17	ft ³			0.00E+00	0.101	0.00E+00	
	Partially Insulated; Eq. 1-29, TLA = 0.3*TAA + 0.7*TB + 0.005*α*R	TLA	521.76					Effective Tank diameter	D _e	14.74	ft			0.00E+00	0.101	0.00E+00	
	Fully Insulated; TLA = TB	TLA	520.0					Effective Tank Height	H _e	6.28	ft			0.00E+00	0.101	0.00E+00	
	Average Vapor Temperature (Tv)							Vapor Space Outage Hvo = 1/2 H	Hvo	3.14	ft			0.00E+00	0.101	0.00E+00	
	Not Insulated; Eq. 1-33, Tv = 0.7*TAA + 0.3*TB + 0.009*α*I	Tv	522.98											0.00E+00	0.101	0.00E+00	
	Partially Insulated; Eq. 1-34, Tv = 0.6*TAA + 0.4*TB + 0.01*α*R*I	Tv	523.55											0.00E+00	0.101	0.00E+00	
	Fully Insulated; Tv = TB	Tv	519.96											0.00E+00	0.101	0.00E+00	
	Stock Vapor Density; Eq. 1-22, Wv = (Mv/PVA)/(R*Tv)													0.00E+00	0.101	0.00E+00	
	Not Insulated	Wv	2.328E-03											0.00E+00	0.101	0.00E+00	
	Partially Insulated	Wv	2.336E-03											0.00E+00	0.101	0.00E+00	
	Fully Insulated	Wv	2.210E-03											0.00E+00	0.101	0.00E+00	

Monthly Calculations (continued)

JUNE

Tank No.	ROUTINE EMISSIONS CALCULATIONS		ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	HAPS Speciation		Product	lb/month	addl/vol		
	Symbol	Units	Symbol	Units			Product	lb/month									
	LT	4.49	lb/month	Vapor Space Volume	Vv	536.2	ft ³	Total HAP Emissions =	4.493	Vapor Weight Concentration	Eq. 40-6 Zvi = yiMi / MV	Vapor Mole Fraction	Eq. 40-5 yi = Pi / PVA				
		2.25E-03	ton/month	Stock Vapor Density	Wv	0.0032	lb/ft ³	Eq. 40-2 L _{ij} = Zi _{ij} (L _i)		Individual HAPS	L _{ij} (lb/month)	M _i	M _v	Z _{vi}	P _i = P _{VA} (X _i)	P _{VA}	y _i
	Time Period	June		Vapor Space Expansion Factor (0 < KE <= 1); Eq. 1-5	KE	0.033	per day	Eq. 40-5 yi = Pi / PVA		hexane	0.0000	86.18	130	0.00000	0.000000	0.142	-
	Nearest US Location	Bridgeport, CT		Vented Vapor Saturation Factor	Ks	1.00	NA	Constant: Number of Daily Events in a Year	365	benzene	0.0000	78.11	130	0.00000	0.000000	0.142	-
	Daily total solar insolation on a horizontal surface; Table 7.1-7	I	1862.0	Working Losses; Eq. 1-35, Lw = VQ * KN * Kp * Wv * KB	Lw	2.78	lb/month	Eq. 1-39: VQ=(5.614*Q)		2,2,4 TMP	0.0000	114.23	130	0.00000	0.000000	0.142	-
	Absolute Pressure	Pa	14.89	Net Working Loss Throughput (Eq. 1-39: VQ=(5.614*Q))	VQ	862	ft ³ /month	Eq. 1-35, Lw = VQ * KN * Kp * Wv * KB		toluene	0.0000	92.14	130	0.00000	0.000000	0.142	-
	Ideal Gas Constant	R	10.73	Working Loss Turnover Factor Eq 1-35 K _w =(180+N)/6N for N>=36, else K _w =N	KN	1.0000		Net Working Loss Throughput (Eq. 1-39: VQ=(5.614*Q))		ethylbenzene	1.3075	106.17	130	0.29099	0.050514	0.142	0.35631
	Product Information			Working Loss Product Factor	Kp	1.00		Working Loss Turnover Factor Eq 1-35 K _w =(180+N)/6N for N>=36, else K _w =N		xylene	3.1859	106.17	130	0.70901	0.123078	0.142	0.86815
	Product Type	Diesel Additive		Stock Vapor Density	Wv	0.0032	lb/ft ³	Working Loss Product Factor	Kp	1.00							

Monthly Calculations (continued)

JULY

Tank No.	ROUTINE EMISSIONS CALCULATIONS			ROUTINE EMISSIONS CALCULATIONS			HAPS Speciation		Vapor Mole Fraction	
	Symbol	Units	Symbol	Units	Symbol	Units	Product	lb/month	addl/vol	addl/vol
10457	LT	5.32	lb/month	LS	2.04	lb/month	Total HAP Emissions =	5.321		
		2.66E-03	ton/month	VV	536.2	ft ³	Eq. 40-2 L _{ij} =Z _{ij} (L _i)			
	Time Period	July		KE	0.032	per day	Individual HAPS	L _{ij} (lb/month)	M _i	M _v
	Nearest US Location	Bridgeport, CT		KS	1.00	NA	hexane	0.0000	86.18	130
	Daily total solar insolation on a horizontal surface; Table 7.1-7	I	1904.0	Btu/ft ² -day	Constant: Number of Daily Events in a Year	365	benzene	0.0000	78.11	130
	Absolute Pressure	P _A	14.89	psi	Working Losses; Eq. 1-35, L _w = VQ * KN * Kp * Wv * KB	LW	2.24 TMP	0.0000	114.23	130
	Ideal Gas Constant	R	10.73	psi ft ³ /lb-mole R	Net Working Loss Throughput (Eq. 1-39: VQ=5.614*Q)	VQ	toluene	0.0000	92.14	130
	Product Information				Working Loss Turnover Factor Eq. 1-35 K _w =(180+N)/6N for N>36, else K _w =1	KN	ethylbenzene	1.5467	106.17	130
	Product Type	Diesel Additive			Working Loss Product Factor	Kp	xylene	3.7745	106.17	130
	Vapor Molecular weight	Mv	130	lb/lb-mole	Stock Vapor Density	Wv	naphthalene	0.0000	128.17	130
	Average organic liquid density	WL	6.10	lb/gal	Vent Setting Correction Factor	KB	cumene	0.0000	120.19	130
	Average Reid Vapor Pressure	RVP	0.00	psi	Vent Setting Correction Factor	KB				
	Product factor: 0.4 for crude oils or 1 for other organic liquids	Kc	1.00		Vented Vapor Saturation Factor; Eq. 1-21, K _s = 1/(1+0.053*P _v ^{0.7} H _v ^{0.2})	Ks				
	Vapor Pressure Equation Constant A	A	0.00		Vapor Pressure at Avg Daily Liq Surface Temp	P _v A				
	Vapor Pressure Equation Constant B (Table 7.1-2)	B	0.0	R	Vapor Space Outage	H _v o				
	Tank design data				Vapor Space Expansion Factor (Eq. 1-5: (ΔT _v /TLA)-((ΔP _v -ΔPB)/(PA-PVA))	KE				
	Shell height	H _s	6.28	ft	Average Daily Vapor Temperature Range	ΔT _v				
	Diameter	D	14.74	ft	Average Daily Vapor Pressure Range	ΔP _v				
	Throughput	Q	6.450	gal/month	Breather Vent Pressure Setting Range (Equation 1-10: ΔPB = PBP - P _v BP)	P _v BP				
	Turnovers	N	9.47	per year	Vapor Pressure at Avg Daily Liq Surface Temp	P _v A				
	Roof Type:		0.00		Average Daily Liquid Surface Temperature	TLA				
	Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft	Atmospheric Pressure	P _A				
	Dome Roof Radius (If unknown, use tank diameter (D) or (2R _s))	RR	NA	ft	Average Daily Vapor Temperature Range (ΔT _v)					
	Maximum Filling Height -use (Pi/4)D if unknown	HLX	5.28	ft	Eq. 40-4 XI = (ΣL _{ij} M _i)/M _v	Z _{ij}				
	Minimum Filling Height (use 0 if unknown)	HLN	1.00	ft	Eq. 40-6 Z _{vi} = y _i M _i / M _v	M _i				
	Liquid height (assume 1/2 H)	HL	3.14	ft	Eq. 40-5 y _i = P _i / P _{vA}	P _{vA}				
	Tank insulation (pick from drop down list)		Not Insulated		Eq. 1-25 P _{vX} = exp(P _{vA} (B-TLA)/C)	B				
	Tank Construction (pick from drop down list)		Welded		Eq. 1-25 P _{vN} = exp(P _{vN} (B-TLN)/C)	C				
	Tank Shell Color (pick from drop down list)		White							
	Tank Shell Condition (pick from drop down list)		Average							
	Tank Interior Condition (pick from drop down list)		Light Rust							
	Tank paint solar absorptance, dimensionless; Table 7.1-6	α	0.25							
	Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	0.03	psi						
	True Vapor Pressure; Eq. 1-25, P _{vA} = exp(A-(B/TLA))		-0.03	psi						
	Not Insulated	P _{vA}	0.168992	psi						
	Partially Insulated	P _{vA}	0.1697728	psi						
	Fully Insulated	P _{vA}	0.1593647	psi						
	Average Daily Ambient Temperature (TAA) Eq. 1-30 TAA = ((TAX+TAN)/2)	TAA	53.90	R						
	Average daily maximum ambient temperature; Table 7.1-7	TAX	54.10	R						
	Average daily minimum ambient temperature; Table 7.1-7	TAN	52.60	R						
	Liquid Bulk Temperature; Eq. 1-31: TB = TAA + 0.003 α I	TB	53.53	R						
	Average Daily Liquid Surface Temperature (TLA)									
	Not Insulated; Eq. 1-28, TLA = 0.4*TAA + 0.6*TB + 0.005*α I	TLA	53.74	R						
	Partially Insulated; Eq. 1-29, TLA = 0.3*TAA + 0.7*TB + 0.005*α I	TLA	53.78	R						
	Fully Insulated; TLA = TB	TLA	53.53	R						
	Average Vapor Temperature (Tv)									
	Not Insulated; Eq. 1-33, Tv = 0.7*TAA + 0.3*TB + 0.009*α I	Tv	53.61	R						
	Partially Insulated; Eq. 1-34, Tv = 0.6*TAA + 0.4*TB + 0.01*α I	Tv	53.23	R						
	Fully Insulated; Tv = TB	Tv	53.53	R						
	Stock Vapor Density; Eq. 1-22, Wv = (Mv/PVA)/(R*Tv)									
	Not Insulated	Wv	3.801E-03							
	Partially Insulated	Wv	3.814E-03							
	Fully Insulated	Wv	3.606E-03							

Monthly Calculations (continued)

AUGUST

Tank No.	ROUTINE EMISSIONS CALCULATIONS			ROUTINE EMISSIONS CALCULATIONS			HAPS Speciation		Vapor Mole Fraction	
	Symbol	Units	Symbol	Units	Symbol	Units	Product	lb/month	addl/vol	addl/vol
10457	LT	4.98	lb/month	LS	1.81	lb/month	Total HAP Emissions =	4.983		
		2.49E-03	ton/month	VV	536.2	ft ³	Eq. 40-2 L _{ij} =Z _{ij} (L _i)			
	Time Period	August		KE	0.030	per day	Individual HAPS	L _{ij} (lb/month)	M _i	M _v
	Nearest US Location	Bridgeport, CT		KS	1.00	NA	hexane	0.0000	86.18	130
	Daily total solar insolation on a horizontal surface; Table 7.1-7	I	1685.0	Btu/ft ² -day	Constant: Number of Daily Events in a Year	365	benzene	0.0000	78.11	130
	Absolute Pressure	P _A	14.89	psi	Working Losses; Eq. 1-35, L _w = VQ * KN * Kp * Wv * KB	LW	2.24 TMP	0.0000	114.23	130
	Ideal Gas Constant	R	10.73	psi ft ³ /lb-mole R	Net Working Loss Throughput (Eq. 1-39: VQ=5.614*Q)	VQ	toluene	0.0000	92.14	130
	Product Information				Working Loss Turnover Factor Eq. 1-35 K _w =(180+N)/6N for N>36, else K _w =1	KN	ethylbenzene	1.4488	106.17	130
	Product Type	Diesel Additive			Working Loss Product Factor	Kp	xylene	3.5345	106.17	130
	Vapor Molecular weight	Mv	130	lb/lb-mole	Stock Vapor Density	Wv	naphthalene	0.0000	128.17	130
	Average organic liquid density	WL	6.10	lb/gal	Vent Setting Correction Factor	KB	cumene	0.0000	120.19	130
	Average Reid Vapor Pressure	RVP	0.00	psi	Vent Setting Correction Factor	KB				
	Product factor: 0.4 for crude oils or 1 for other organic liquids	Kc	1.00		Vented Vapor Saturation Factor; Eq. 1-21, K _s = 1/(1+0.053*P _v ^{0.7} H _v ^{0.2})	Ks				
	Vapor Pressure Equation Constant A	A	0.00		Vapor Pressure at Avg Daily Liq Surface Temp	P _v A				
	Vapor Pressure Equation Constant B (Table 7.1-2)	B	0.0	R	Vapor Space Outage	H _v o				
	Tank design data				Vapor Space Expansion Factor (Eq. 1-5: (ΔT _v /TLA)-((ΔP _v -ΔPB)/(PA-PVA))	KE				
	Shell height	H _s	6.28	ft	Average Daily Vapor Temperature Range	ΔT _v				
	Diameter	D	14.74	ft	Average Daily Vapor Pressure Range	ΔP _v				
	Throughput	Q	6.450	gal/month	Breather Vent Pressure Setting Range (Equation 1-10: ΔPB = PBP - P _v BP)	P _v BP				
	Turnovers	N	9.47	per year	Vapor Pressure at Avg Daily Liq Surface Temp	P _v A				
	Roof Type:		0.00		Average Daily Liquid Surface Temperature	TLA				
	Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft	Atmospheric Pressure	P _A				
	Dome Roof Radius (If unknown, use tank diameter (D) or (2R _s))	RR	NA	ft	Average Daily Vapor Temperature Range (ΔT _v)					
	Maximum Filling Height -use (Pi/4)D if unknown	HLX	5.28	ft	Eq. 40-4 XI = (ΣL _{ij} M _i)/M _v	Z _{ij}				
	Minimum Filling Height (use 0 if unknown)	HLN	1.00	ft	Eq. 40-6 Z _{vi} = y _i M _i / M _v	M _i				
	Liquid height (assume 1/2 H)	HL	3.14	ft	Eq. 40-5 y _i = P _i / P _{vA}	P _{vA}				
	Tank insulation (pick from drop down list)		Not Insulated		Eq. 1-25 P _{vX} = exp(P _{vA} (B-TLA)/C)	B				
	Tank Construction (pick from drop down list)		Welded		Eq. 1-25 P _{vN} = exp(P _{vN} (B-TLN)/C)	C				
	Tank Shell Color (pick from drop down list)		White							
	Tank Shell Condition (pick from drop down list)		Average							
	Tank Interior Condition (pick from drop down list)		Light Rust							
	Tank paint solar absorptance, dimensionless; Table 7.1-6	α	0.25							
	Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	0.03	psi						
	True Vapor Pressure; Eq. 1-25, P _{vA} = exp(A-(B/TLA))		-0.03	psi						
	Not Insulated	P _{vA}	0.1632264	psi						
	Partially Insulated	P _{vA}	0.163897	psi						
	Fully Insulated	P _{vA}	0.1549333	psi						
	Average Daily Ambient Temperature (TAA) Eq. 1-30 TAA = ((TAX+TAN)/2)	TAA	53.20	R						
	Average daily maximum ambient temperature; Table 7.1-7	TAX	54.10	R						
	Average daily minimum ambient temperature; Table 7.1-7	TAN	52.30	R						
	Liquid Bulk Temperature; Eq. 1-31: TB = TAA + 0.003 α I	TB	53.46	R						
	Average Daily Liquid Surface Temperature (TLA)									
	Not Insulated; Eq. 1-28, TLA = 0.4*TAA + 0.6*TB + 0.005*α I	TLA	53.06	R						
	Partially Insulated; Eq. 1-29, TLA = 0.3*TAA + 0.7*TB + 0.005*α I	TLA	53.19	R						
	Fully Insulated; TLA = TB	TLA	53.45	R						
	Average Vapor Temperature (Tv)									
	Not Insulated; Eq. 1-33, Tv = 0.7*TAA + 0.3*TB + 0.009*α I	Tv	53.37	R						
	Partially Insulated; Eq. 1-34, Tv = 0.6*TAA + 0.4*TB + 0.01*α I	Tv	53.92	R						
	Fully Insulated; Tv = TB	Tv	53.46	R						
	Stock Vapor Density; Eq. 1-22, Wv = (Mv/PVA)/(R*Tv)									
	Not Insulated	Wv	3.680E-03							
	Partially Insulated	Wv	3.691E-03							
	Fully Insulated	Wv	3.512E-03							

Monthly Calculations - JANUARY

Tank No.	10458			ROUTINE EMISSIONS CALCULATIONS			Symbol			Units			HAPS Speciation			lb/month			additive												
	ROUTINE EMISSIONS CALCULATIONS			Symbol	Units	ROUTINE EMISSIONS CALCULATIONS			Symbol	Units	HAPS Speciation			lb/month			additive														
Total Losses (Eq.1-1: LT = LS+LW)																															
LT		0.95		lb/month		Vapor Space Volume		Vv		535.3		ft ³		Total HAP Emissions =		0.952		Vapor Weight Concentration		Vapor Mole Fraction											
Daily total solar insolation on a horizontal surface, Table 7.1-7		I		560.0		Stock Vapor Density		Wv		0.0008		lb/ft ³		Eq. 40-2 L _{ij} = Z _{ij} (L _i)		Eq. 40-6 Z _{vi} = yM _i / MV		Eq. 40-5 y _i = P _i / P _{VA}													
Nearest US Location		Bridgeport, CT				Vapor Space Expansion Factor (0 < KE <= 1); Eq. 1-5		KE		0.020		per day		Individual HAPS		L _{ij} (lb/month)		M _i		M _v		Z _{vi}		P _i = P _{VA} (x _i)		P _{VA}		y _i			
Absolute Pressure		P _a		14.69		psi		Constant; Number of Daily Events in a Year		Ks		365		days/month		hexane		0.0000		86.18		130		0.00000		0.000000		0.032		-	
Ideal Gas Constant		R		10.73		psia ft ³ /lb-mole R		Working Losses; Eq. 1-35, L _w = VQ * KN * K _p * W _v * KB		LW		0.69		lb/month		benzene		0.0000		78.11		130		0.00000		0.000000		0.032		-	
Product Information						Net Working Loss Throughput (Eq. 1-39: VQ=5.614*Q)		VQ		862		ft ³ /month		toluene		0.0000		92.14		130		0.00000		0.000000		0.032		-			
Product Type		Diesel Additive				Working Loss Turnover Factor Eq. 1-35 K _w =(180+N)/6N for N>36, else K _w =KN		KN		1.0000				ethylbenzene		0.2793		106.17		130		0.29329		0.011655		0.032		0.35912			
Vapor Molecular weight		Mv		130		lb/lb-mole		Working Loss Product Factor		Kp		1.00		xylene		0.6730		106.17		130		0.70671		0.028084		0.032		0.86533			
Average organic liquid density		WL		6.10		lb/gal		Stock Vapor Density		Wv		0.0008		naphthalene		0.0000		128.17		130		0.00E+00		0.00E+00		0.032		0.00E+00			
Average Reid Vapor Pressure		RVP		0.00		psi		Vent Setting Correction Factor		KB		1.00		cumene		0.0000		120.19		130		0.00E+00		0.00E+00		0.032		0.00E+00			
Product factor; 0.4 for crude oils or 1 for other organic liquids		Kc		1.00				Vent Setting Correction Factor		KB		1.00		Liquid Mole Fraction		Eq. 40-4 xi _i = (Z _i M _i)/M _i															
Vapor Pressure Equation Constant A		A		0.00				Vent Vapor Saturation Factor; Eq. 1-21, K _s = 1/(1+0.053*P _{VA} ^{0.7} H _v)		Ks		1.00		Individual HAPS		Z _i		M _i		M _v		X _i		A		B		C		P _{VA}	
Vapor Pressure Equation Constant B (Table 7.1-2)		B		0.0		R		Vapor Pressure at Avg Daily Liq Surface Temp		P _{VA}		0.0325		hexane		0.00000		130		86.18		0.00000		6.878		1171.5		224.37		0.8715	
Vapor Space Outage		Hvo		0.00		ft		Vapor Space Outage		Hvo		0.00		benzene		0.00000		130		78.11		0.00000		6.906		1211		220.79		0.5064	
Tank design data														2,2,4 TMP		0.00000		130		114.23		0.00000		6.812		1257.8		220.74		0.2495	
Shell height		Hs		6.28		ft		Vapor Space Expansion Factor (Eq. 1-5: (ΔTv/TLA)=[(ΔPv-ΔPB)/(PA-Pv)])		KE		0.0198		toluene		0.00000		130		92.14		0.00000		7.017		1377.6		222.64		0.1296	
Diameter		D		14.73		ft		Average Daily Vapor Temperature Range		ΔTv		11.76		ethylbenzene		0.26400		130		106.17		0.32326		6.95		1419.3		212.61		0.0361	
Throughput		Q		6.450		gal/month		Average Daily Vapor Pressure Range		ΔPv		0.0000		xylene		0.73600		130		106.17		0.90120		7.009		1462.3		215.11		0.0312	
Turnovers		N		9.48		per year		Breather Vent Pressure Setting Range (Equation 1-10: ΔPB = PBP - PBV)		ΔPB		0.0600		naphthalene		0.00000		130		128.17		0.00000		7.148		1831.6		211.82		0.0006	
Roof Type:								Vapor Pressure at Avg Daily Liq Surface Temp		P _{VA}		0.0325		cumene		0.00000		130		120.19		0.00000		6.929		1455.8		207.2		0.0153	
Tank Cone Roof Slope (If unknown, use 0.0625)		SR		0.0625		ft/ft		Average Daily Liquid Surface Temperature		TLA		491.45																			
Dome Roof Radius (If unknown, use tank diameter (D) or (2R _s))		RR		NA		ft		Atmospheric Pressure		P _a		14.69																			
Maximum Filling Height - use (Pi/4)D if unknown		HLX		5.28		ft																									
Minimum Filling Height (use 0 if unknown)		HLN		1.00		ft		Average Daily Vapor Temperature Range (ΔTv)																							
Liquid height (assume 1/2 H)		HL		3.14		ft		Not Insulated - Equation 1-7 (ΔTv = 0.7 ΔTA + 0.02 q R)		ΔTv		12.8																			
Tank Insulation (pick from drop down list)		Not Insulated						Partially Insulated - Equation 1-8 (ΔTv = 0.6 ΔTA + 0.02 q R)		ΔTv		10.48																			
Tank Construction (pick from drop down list)		Welded						Fully Insulated, constant temperature		ΔTv		0.00																			
Tank Shell Color (pick from drop down list)		White																													
Tank Shell Condition (pick from drop down list)		Average																													
Tank Interior Condition (pick from drop down list)		Light Rust						Average Daily Vapor Pressure Range (ΔPv)																							
Tank paint solar absorptance, dimensionless, Table 7.1-6		α		0.25				Not Insulated - Equation 1-9: ΔPv = PvX - PVN		ΔPv		0.00000																			
Breather Vent Setting Range (Default Assumption: +/- 0.03)		PBP		0.03		psi		Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25 PvX = exPvX)		PvX		1.00000																			
Breather Vent Setting Range (Default Assumption: +/- 0.03)		PBP		-0.03		psi		Vapor pressure at ave daily min liquid surface temp. (Eq. 1-25 PVN = exPVN)		PVN		1.00000																			
True Vapor Pressure; Eq. 1-25, P _{VA} = exp(A-(B/TLA))								Average daily max. liquid surface temp.; Fig. 7.1-17 TLX = TLA + 0.25ΔTv		TLX		494.39																			
Not Insulated		P _{VA}		0.032455				Average daily min. liquid surface temp.; Fig. 7.1-17 TLN = TLA - 0.25ΔTv		TLN		488.51																			
Partially Insulated		P _{VA}		0.0325101																											
Fully Insulated		P _{VA}		0.031764				Partially Insulated - Equation 1-9: ΔPv = PvX - PVN		ΔPv		0.00000																			
Average Daily Ambient Temperature (TAA) Eq. 1-30 TAA = ((TAX+TAN)/2)		TAA		490.50		R		Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25 PvX)		PvX		1.00000																			
Average daily maximum ambient temperature, Table 7.1-7		TAX		496.90		R		Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25 PVN)		PVN		1.000000																			
Average daily minimum ambient temperature, Table 7.1-7		TAN		484.10		R		Average daily maximum liquid surface temperature, deg R (TLX = TLA + TLX)		TLX		494.11																			
Average daily minimum ambient temperature, Table 7.1-7		TAN		484.10		R		Average daily minimum liquid surface temperature, deg R (TLN = TLA - TLN)		TLN		488.87																			
Liquid Bulk Temperature; Eq. 1-31: TB = TAA + 0.003 as l		TB		490.92		R		Fully Insulated (ΔPv = 0)		ΔPv		0.00																			
Average Daily Liquid Surface Temperature (TLA)																															
Not Insulated; Eq. 1-28, TLA = 0.4*TAA + 0.6*TB + 0.005*α ^{0.1}		TLA		491.45		R		Vapor Space Volume (Eq. 1-3: Vv = ((Pi/4) D ² Hvo)		Vv		535.33																			
Partially Insulated; Eq. 1-29, TLA = 0.3*TAA + 0.7*TB + 0.005*α ^{0.1}		TLA		491.49		R		Effective Tank diameter		D _e		14.73																			
Fully Insulated; TLA = TB		TLA		490.9		R		Effective Tank Height		H _e		6.28																			
Fully Insulated; TLA = TB		TLA		490.9		R		Vapor Space Outage Hvo = 1/2 H		Hvo		3.14																			
Average Vapor Temperature (Tv)																															
Not Insulated; Eq. 1-33, Tv = 0.7*TAA + 0.3*TB + 0.009*α ^{0.1}		Tv		491.89		R																									
Partially Insulated; Eq. 1-34, Tv = 0.6*TAA + 0.4*TB + 0.01*α ^{0.1}		Tv		492.07		R																									
Fully Insulated; Tv = TB		Tv		490.92		R																									
Stock Vapor Density; Eq. 1-22, Wv = (Mv*PVA)/(R*TV)																															
Not Insulated		Wv		7.993E-04																											
Partially Insulated		Wv		8.004E-04																											
Fully Insulated		Wv		7.838E-04																											

Monthly Calculations (continued)

Tank No.	10458			ROUTINE EMISSIONS CALCULATIONS			Symbol			Units			HAPS Speciation			lb/month			additive												
	ROUTINE EMISSIONS CALCULATIONS			Symbol	Units	ROUTINE EMISSIONS CALCULATIONS			Symbol	Units	HAPS Speciation			lb/month			additive														
Total Losses (Eq.1-1: LT = LS+LW)																															
LT		1.05		lb/month		Vapor Space Volume		Vv		535.3		ft ³		Total HAP Emissions =		1.051		Vapor Weight Concentration		Vapor Mole Fraction											
Daily total solar insolation on a horizontal surface, Table 7.1-7		I		847.0		Btu/ft ² -day		Stock Vapor Density		Wv		0.0009		lb/ft ³		Eq. 40-2 L _{ij} = Z _{ij} (L _i)		Eq. 40-6 Z _{vi} = yM _i / MV		Eq. 40-5 y _i = P _i / P _{VA}											
Nearest US Location		Bridgeport, CT				Vapor Space Expansion Factor (0 < KE <= 1); Eq. 1-5		KE		0.023		per day		Individual HAPS		L _{ij} (lb/month)		M _i		M _v		Z _{vi}		P _i = P _{VA} (x _i)		P _{VA}		y _i			
Absolute Pressure		P _a		14.69		psi		Constant; Number of Daily Events in a Year		Ks		365		days/month		hexane		0.0000		86.18		130		0.00000		0.000000		0.035		-	
Ideal Gas Constant		R		10.73		psia ft ³ /lb-mole R		Working Losses; Eq. 1-35, L _w = VQ * KN * K _p * W _v * KB																							

Monthly Calculations (continued)

SEPTEMBER

Tank No.	10458	Units		Units		Units		Units		lb/month		addl/vol							
ROUTINE EMISSIONS CALCULATIONS		Symbol		ROUTINE EMISSIONS CALCULATIONS		Symbol		ROUTINE EMISSIONS CALCULATIONS		HAPS Speciation		Vapor Mole Fraction							
Total Losses (Eq. 1-1: LT = LS+LW)		LT	3.78	lb/month	Standing Losses; Eq. 1-2: Ls = 365 (Vv * Wv * Ke * Ks)		Ls	1.28	lb/month	Product		Total HAP Emissions = 3.783							
Time Period		September			Vapor Space Volume		Vv	535.3	ft ³	Eq. 40-2 L _{ij} = Z _{ij} (L _i)		Eq. 40-5 y _i = P _i / PVA							
Nearest US Location		Bridgeport, CT			Stock Vapor Density		Wv	0.0029	lb/ft ³	Individual HAPS		Eq. 40-6 Z _{vi} = y _i M _i / MV							
Daily total solar insolation on a horizontal surface; Table 7.1-7		I	1320.0	Btu/ft ² -day	Vapor Space Expansion Factor (0 < KE <= 1); Eq. 1-5		KE	0.028	per day	hexane		0.0000	0.000000						
Absolute Pressure		Pa	14.89	psi	Vented Vapor Saturation Factor		Ks	1.00	NA	benzene		0.0000	0.000000						
Ideal Gas Constant		R	10.73	psi ft ³ /lb-mole R	Constant: Number of Daily Events in a Year		365	30	days/month	2,2,4 TMP		0.0000	0.000000						
Product Information				Working Losses; Eq. 1-35: Lw = VQ * KN * Kp * Wv * KB		Lw	2.50	lb/month	toluene		0.0000	0.000000							
Product Type		Diesel Additive			Net Working Loss Throughput (Eq. 1-39: VQ=5.614*Q)		VQ	862	ft ³ /month	ethylbenzene		1.1016	0.029119						
Vapor Molecular weight		Mv	130	lb/lb-mole	Working Loss Turnover Factor Eq 1-35 Kp=(180+N)/6N for N>=36, else Kp=		KN	1.0000		xylene		2.6816	0.109948						
Average organic liquid density		WL	6.10	lb/gal	Working Loss Product Factor		Kp	1.00		naphthalene		0.0000	0.000000						
Average Reid Vapor Pressure		RVP	0.00	psi	Stock Vapor Density		Wv	0.0029	lb/ft ³	cumene		0.0000	0.000000						
Product factor: 0.4 for crude oils or 1 for other organic liquids		Kc	1.00		Vent Setting Correction Factor		KB	1.00		Liquid Mole Fraction		Component Vapor Pressure							
Vapor Pressure Equation Constant A		A	0.00		Vented Vapor Saturation Factor; Eq. 1-21: Ks = 1/(1+0.053*PVA*Hvo)		Ks	1.00		Eq. 40-4 xi = (Z _i M _i)/M _i		PVA=(0.019337)(PVA-B)(TLA-C)							
Vapor Pressure Equation Constant B (Table 7.1-2)		B	0.0	R	Vapor Pressure at Avg Daily Liq Surface Temp		PVA	0.1267	psia	Individual HAPS		A B C P _{vi}							
Tank design data				Vapor Space Outage		Hvo	0.00	ft	hexane		0.000000	130	86.18	0.000000	6.878	1171.5	224.37	2.3895	
Shell height		Hs	6.28	ft	Vapor Space Expansion Factor (Eq. 1-5: (ΔTv/TLA)-((ΔPv-ΔPB)/(PA-PVA))		KE	0.0276	per day	benzene		0.000000	130	78.11	0.000000	6.906	1211	220.79	1.4842
Diameter		D	14.73	ft	Average Daily Vapor Temperature Range		ΔTv	16.75	°R	2,2,4 TMP		0.000000	130	114.23	0.000000	6.812	1257.8	220.74	0.7627
Throughput		Q	6,450	gal/month	Average Daily Vapor Pressure Range		ΔPv	0.0000	psi	toluene		0.000000	130	92.14	0.000000	7.017	1377.6	222.64	0.4318
Turnovers		N	3.80	per year	Breather Vent Pressure Setting Range (Equation 1-10: APB = PBP - PBPB)		PBP	0.0600	psi	ethylbenzene		0.26400	130	106.17	0.32326	6.95	1419.3	212.61	0.1397
Roof type:		0.00 <td></td> <td></td> <th colspan="2">Vapor Pressure at Avg Daily Liq Surface Temp</th> <th>PVA</th> <td>0.1267</td> <td>psia</td> <th colspan="2">xylene</th> <td>0.73620</td> <td>130</td> <td>106.17</td> <td>0.90120</td> <td>7.009</td> <td>1462.3</td> <td>215.11</td> <td>0.1220</td>			Vapor Pressure at Avg Daily Liq Surface Temp		PVA	0.1267	psia	xylene		0.73620	130	106.17	0.90120	7.009	1462.3	215.11	0.1220
Tank Cone Roof Slope (If unknown, use 0.0625)		SR	0.0625	ft/ft	Average Daily Liquid Surface Temperature		TLA	528.39	°R	naphthalene		0.000000	130	128.17	0.000000	7.146	1831.6	211.82	0.0035
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))		RR	NA	ft	Atmospheric Pressure		PA	14.69	psia	cumene		0.000000	130	120.19	0.000000	6.929	1455.8	207.2	0.0659
Maximum Filling Height -use (Pi/4)D if unknown		HLX	5.28	ft	Average Daily Vapor Temperature Range (ΔTv)		ΔTv	14.5	°R	Individual HAPS		Eq. 40-4 xi = (Z _i M _i)/M _i		A B C P _{vi}					
Minimum Filling Height (use 0 if unknown)		HLN	1.00	ft	Average daily ambient temperature range - Equation 1-11 (ΔTA=TAX-TA)		ΔTA	14.5	°R	hexane		0.000000	130	86.18	0.000000	6.878	1171.5	224.37	2.3895
Liquid height (assume 1/2 H)		HL	3.14	ft	Not Insulated - Equation 1-7 (ΔTv = 0.7 ΔTA + 0.02 α I)		ΔTv	16.75	°R	benzene		0.000000	130	78.11	0.000000	6.906	1211	220.79	1.4842
Tank insulation (pick from drop down list)		Not Insulated			Partially Insulated - Equation 1-8 (ΔTv = 0.6 ΔTA + 0.02 α R I)		ΔTv	13.92	°R	2,2,4 TMP		0.000000	130	114.23	0.000000	6.812	1257.8	220.74	0.7627
Tank Construction (pick from drop down list)		Welded			Fully Insulated, constant temperature		ΔTv	0.00	°R	toluene		0.000000	130	92.14	0.000000	7.017	1377.6	222.64	0.4318
Tank Shell Color (pick from drop down list)		White			Average Daily Vapor Pressure Range (ΔPv)		ΔPv	0.000000	psia	ethylbenzene		0.26400	130	106.17	0.32326	6.95	1419.3	212.61	0.1397
Tank Shell Condition (pick from drop down list)		Average			Not Insulated - Equation 1-9: ΔPv = PVX - PVN		ΔPv	0.000000	psia	xylene		0.73620	130	106.17	0.90120	7.009	1462.3	215.11	0.1220
Tank Interior Condition (pick from drop down list)		Light Rust			Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25 PVX = exPvN)		PvX	1.000000	psia	naphthalene		0.000000	130	128.17	0.000000	7.146	1831.6	211.82	0.0035
Tank paint solar absorptance, dimensionless, Table 7.1-6		α	0.25		Average daily max. liquid surface temp.; Fig. 7.1-17 TLX = TLA + 0.25ΔT TLX		TLX	528.39	°R	cumene		0.000000	130	120.19	0.000000	6.929	1455.8	207.2	0.0659
Breather Vent Setting Range (Default Assumption: +/- 0.03)		PBP	0.03	psi	Vapor pressure at ave. daily min liquid surface temp. (Eq. 1-25 uPvN)		uPvN	1.000000	psia	Liquid Mole Fraction		Component Vapor Pressure							
True Vapor Pressure; Eq. 1-25: PVA = exp(A-(B/TLA))		PVA	0.1266829	psi	Average daily min. liquid surface temp.; Fig. 7.1-17 TLN = TLA - 0.25ΔT TLN		TLN	524.21	°R	Eq. 40-4 xi = (Z _i M _i)/M _i		PVA=(0.019337)(PVA-B)(TLA-C)							
Not Insulated		PVA	0.1266829	psi	Partially Insulated - Equation 1-9: ΔPv = PVX - PVN		ΔPv	0.000000	psia	Individual HAPS		A B C P _{vi}							
Partially Insulated		PVA	0.1271055	psi	Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25 uPvX)		uPvX	1.000000	psia	hexane		0.000000	130	86.18	0.000000	6.878	1171.5	224.37	2.3895
Fully Insulated		PVA	0.1214345	psi	Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25 uPvN)		uPvN	1.000000	psia	benzene		0.000000	130	78.11	0.000000	6.906	1211	220.79	1.4842
Average Daily Ambient Temperature (TAA) Eq. 1-30 TAA = ((TAX+TAN)/2)		TAA	526.15	°R	Average daily maximum liquid surface temperature, deg R (TLX = TLA + TLX)		TLX	532.32	°R	toluene		0.000000	130	92.14	0.000000	7.017	1377.6	222.64	0.4318
Average daily maximum ambient temperature, Table 7.1-7		TAX	533.40	°R	Average daily minimum liquid surface temperature, deg R (TLN = TLA - TLN)		TLN	524.67	°R	ethylbenzene		0.26400	130	106.17	0.32326	6.95	1419.3	212.61	0.1397
Average daily minimum ambient temperature, Table 7.1-7		TAN	518.90	°R	Fully Insulated (ΔPv = 0)		ΔPv	0.00	psia	xylene		0.73620	130	106.17	0.90120	7.009	1462.3	215.11	0.1220
Liquid Bulk Temperature; Eq 1-31: TB = TAA + 0.003 α s I		TB	527.14	°R	Vapor Space Volume (Eq. 1-3: Vv = ((Pi/4) D ²)Hvo)		Vv	535.33	ft ³	naphthalene		0.000000	130	128.17	0.000000	7.146	1831.6	211.82	0.0035
Average Daily Liquid Surface Temperature (TLA)				Effective Tank diameter		D _e	14.73	ft	cumene		0.000000	130	120.19	0.000000	6.929	1455.8	207.2	0.0659	
Not Insulated; Eq. 1-28: TLA = 0.4*TAA + 0.6*TB + 0.005*α*I		TLA	528.39	°R	Vapor Space Outage Hvo = 1/2 H		Hvo	3.14	ft	Liquid Mole Fraction		Component Vapor Pressure							
Partially Insulated; Eq. 1-29: TLA = 0.3*TAA + 0.7*TB + 0.005*α*R		TLA	528.49	°R	Effective Tank Height		H _e	6.28	ft	Eq. 40-4 xi = (Z _i M _i)/M _i		PVA=(0.019337)(PVA-B)(TLA-C)							
Fully Insulated: TLA = TB		TLA	527.1	°R	Average Vapor Temperature (Tv)				Individual HAPS		A B C P _{vi}								
Average Vapor Temperature (Tv)				Not Insulated; Eq. 1-33: Tv = 0.7*TAA + 0.3*TB + 0.009*α*I		Tv	529.42	°R	hexane		0.000000	130	86.18	0.000000	6.878	1171.5	224.37	2.3895	
Not Insulated; Eq. 1-33: Tv = 0.7*TAA + 0.3*TB + 0.009*α*I		Tv	529.42	°R	Partially Insulated; Eq. 1-34: Tv = 0.6*TAA + 0.4*TB + 0.01*α*R		Tv	529.85	°R	benzene		0.000000	130	78.11	0.000000	6.906	1211	220.79	1.4842
Partially Insulated; Eq. 1-34: Tv = 0.6*TAA + 0.4*TB + 0.01*α*R		Tv	529.85	°R	Fully Insulated; Tv = TB		Tv	527.14	°R	2,2,4 TMP		0.000000	130	114.23	0.000000	6.812	1257.8	220.74	0.7627
Fully Insulated; Tv = TB		Tv	527.14	°R	Stock Vapor Density; Eq. 1-22: Wv = (Mv/PVA)/(R*TV)				toluene		0.000000	130	92.14	0.000000	7.017	1377.6	222.64	0.4318	
Stock Vapor Density; Eq. 1-22: Wv = (Mv/PVA)/(R*TV)				Not Insulated		Wv	2.899E-03		ethylbenzene		0.26400	130	106.17	0.32326	6.95	1419.3	212.61	0.1397	
Not Insulated		Wv	2.899E-03		Partially Insulated		Wv	2.906E-03		xylene		0.73620	130	106.17	0.90120	7.009	1462.3	215.11	0.1220
Partially Insulated		Wv	2.906E-03		Fully Insulated		Wv	2.791E-03		naphthalene		0.000000	130	128.17	0.000000	7.146	1831.6	211.82	0.0035
Fully Insulated		Wv	2.791E-03						cumene		0.000000	130	120.19	0.000000	6.929	1455.8	207.2	0.0659	

Monthly Calculations (continued)

OCTOBER

Tank No.	10458	Units		Units		Units		Units		lb/month		addl/vol						
ROUTINE EMISSIONS CALCULATIONS		Symbol		ROUTINE EMISSIONS CALCULATIONS		Symbol		ROUTINE EMISSIONS CALCULATIONS		HAPS Speciation		Vapor Mole Fraction						
Total Losses (Eq. 1-1: LT = LS+LW)		LT	2.53	lb/month	Standing Losses; Eq. 1-2: Ls = 365 (Vv * Wv * Ke * Ks)		Ls	0.84	lb/month	Product		Total HAP Emissions = 2.525						
Time Period		October			Vapor Space Volume		Vv	535.3	ft ³	Eq. 40-2 L _{ij} = Z _{ij} (L _i)		Eq. 40-5 y _i = P _i / PVA						
Nearest US Location		Bridgeport, CT			Stock Vapor Density		Wv	0.0020	lb/ft ³	Individual HAPS		Eq. 40-6 Z _{vi} = y _i M _i / MV						
Daily total solar insolation on a horizontal surface; Table 7.1-7		I	948.0	Btu/ft ² -day	Vapor Space Expansion Factor (0 < KE <= 1); Eq. 1-5		KE	0.026	per day	hexane		0.0000	0.000000					
Absolute Pressure		Pa	14.89	psi	Vented Vapor Saturation Factor		Ks	1.00	NA	benzene		0.0000	0.000000					
Ideal Gas Constant		R	10.73	psi ft ³ /lb-mole R	Constant: Number of Daily Events in a Year		365	31	days/month	2,2,4 TMP		0.0000	0.000000					
Product Information				Working Losses; Eq. 1-35: Lw = VQ * KN * Kp * Wv * KB		Lw	1.69	lb/month	toluene		0.0000	0.000000						
Product Type		Diesel Additive			Net Working Loss Throughput (Eq. 1-39: VQ=5.614*Q)		VQ	862	ft ³ /month	ethylbenzene		0.7370	0.029189					
Vapor Molecular weight		Mv	130	lb/lb-mole	Working Loss Turnover Factor Eq 1-35 Kp=(180+N)/6N for N>=36, else Kp=		KN	1.0000		xylene		1.7880	0.072411					
Average organic liquid density		WL	6.10	lb/gal	Working Loss Product Factor		Kp	1.00		naphthalene		0.0000	0.000000					
Average Reid Vapor Pressure		RVP	0.00	psi	Stock Vapor Density		Wv	0.0020	lb/ft ³	cumene		0.0000	0.000000					
Product factor: 0.4 for crude oils or 1 for other organic liquids		Kc	1.00		Vent Setting Correction Factor		KB	1.00		Liquid Mole Fraction		Component Vapor Pressure						
Vapor Pressure Equation Constant A		A	0.00		Vented Vapor Saturation Factor; Eq. 1-21: Ks = 1/(1+0.053*PVA*Hvo)		Ks	1.00		Eq. 40-4 xi = (Z _i M _i)/M _i		PVA=(0.019337)(PVA-B)(TLA-C)						
Vapor Pressure Equation Constant B (Table 7.1-2)		B	0.0	R	Vapor Pressure at Avg Daily Liq Surface Temp		PVA	0.0835	psia	Individual HAPS		A B C P _{vi}						
Tank design data				Vapor Space Outage		Hvo	0.00	ft	hexane		0.000000	130	86.18	0.000000	6.878	1171.5	224.37	2.3895
Shell height		Hs	6.28	ft	Vapor Space Expansion Factor (Eq. 1-5: (ΔTv/TLA)-((ΔPv-ΔPB)/(PA-PVA))		KE	0.0258	per day	benzene		0.000000	1					

Monthly Calculations - JANUARY

Tank No.	10459B			FEBRUARY			ROUTINE EMISSIONS CALCULATIONS			Symbol			Units						
	ROUTINE EMISSIONS CALCULATIONS			Symbol			Units			ROUTINE EMISSIONS CALCULATIONS			Symbol			Units			
Total Losses (Eq. 1-1: $LT = LS + LW$)	LT	0.04	lb/month	Standing Losses; Eq. 1-2, $LS = 365 (Vv \cdot Wv \cdot KE \cdot Ks)$	LS	0.01	lb/month	Vapor Space Volume	Vv	19.7	ft ³	Stock Vapor Density	Wv	0.0008	lb/ft ³	Vapor Space Expansion Factor ($0 < KE <= 1$); Eq. 1-5	KE	0.020	per day
Daily total solar insolation on a horizontal surface; Table 7.1-7	I	847.9	Btu/ft ² -day	Vented Vapor Saturation Factor	Ks	1.00	NA	Constant; Number of Daily Events in a Year	365	28	days/month	Working Losses; Eq. 1-35, $Lw = VQ \cdot KN \cdot Kp \cdot Wv \cdot KB$	Lw	0.03	lb/month	Net Working Loss Throughput (Eq. 1-39: $VQ = 5.614 \cdot Q$)	VQ	33	ft ³ /month
Nearst US Location	Bridgeport, CT			Working Loss Turnover Factor Eq. 1-35 $Ks = (180 + N)/6N$ for $N > 36$, else $Ks = 1$	KN	1.0000		Working Loss Product Factor	Kp	1.00		Stock Vapor Density	Wv	0.0009	lb/ft ³	Vent Setting Correction Factor	KB	1.00	
Absolute Pressure	P _a	14.69	psi	Product Information				Product Type	Diesel Additive			Vapor Pressure Equation Constant A	A	0.00		Vapor Pressure Equation Constant B (Table 7.1-2)	B	0.0	R
Ideal Gas Constant	R	10.73	ft ³ ·lb/(lb-mole·°R)	Product Factor: 0.4 for crude oils or 1 for other organic liquids	Kc	1.00		Vapor Pressure Equation Constant A	A	0.00		Vapor Pressure Equation Constant B (Table 7.1-2)	B	0.0	R				
Product Information				Vapor Pressure Equation Constant B (Table 7.1-2)	B	0.0	R	Vapor Pressure Equation Constant B (Table 7.1-2)	B	0.0	R								
Tank design data																			
Shell height	H _s	2.49	ft	Vapor Space Expansion Factor (Eq. 1-5: $(\Delta T_v/TLA) + (\Delta P_v - \Delta P_B)/(PA - PVA)$)	KE	0.0198	per day	Shell height	H _s	2.49	ft	Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Average Daily Vapor Temperature Range (Eq. 1-11: $\Delta T_A = T_{AX} - T_{AL}$)	ΔT _A	12.8	°R
Diameter	D	4.29	ft	Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Throughput	Q	250	gal/month	Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Average Daily Vapor Temperature Range (Eq. 1-11: $\Delta T_A = T_{AX} - T_{AL}$)	ΔT _A	12.8	°R
Throughput	Q	250	gal/month	Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Turnovers	N	9.99	per year	Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Average Daily Vapor Temperature Range (Eq. 1-11: $\Delta T_A = T_{AX} - T_{AL}$)	ΔT _A	12.8	°R
Turnovers	N	9.99	per year	Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Roof Type:		0.00		Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Average Daily Vapor Temperature Range (Eq. 1-11: $\Delta T_A = T_{AX} - T_{AL}$)	ΔT _A	12.8	°R
Roof Type:		0.00		Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft	Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Average Daily Vapor Temperature Range (Eq. 1-11: $\Delta T_A = T_{AX} - T_{AL}$)	ΔT _A	12.8	°R
Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft	Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Dome Roof Radius (If unknown, use tank diameter (D) or (2R _s))	RR	NA	ft	Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Average Daily Vapor Temperature Range (Eq. 1-11: $\Delta T_A = T_{AX} - T_{AL}$)	ΔT _A	12.8	°R
Dome Roof Radius (If unknown, use tank diameter (D) or (2R _s))	RR	NA	ft	Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Maximum Filling Height - use (Pi/4)D if unknown	HLX	1.49	ft	Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Average Daily Vapor Temperature Range (Eq. 1-11: $\Delta T_A = T_{AX} - T_{AL}$)	ΔT _A	12.8	°R
Maximum Filling Height - use (Pi/4)D if unknown	HLX	1.49	ft	Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Minimum Filling Height (use 0 if unknown)	HLN	1.00	ft	Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Average Daily Vapor Temperature Range (Eq. 1-11: $\Delta T_A = T_{AX} - T_{AL}$)	ΔT _A	12.8	°R
Minimum Filling Height (use 0 if unknown)	HLN	1.00	ft	Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Liquid height (assume 1.2 ft)	HL	1.24	ft	Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Average Daily Vapor Temperature Range (Eq. 1-11: $\Delta T_A = T_{AX} - T_{AL}$)	ΔT _A	12.8	°R
Liquid height (assume 1.2 ft)	HL	1.24	ft	Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Tank Insulation (pick from drop down list)		Not Insulated		Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Average Daily Vapor Temperature Range (Eq. 1-11: $\Delta T_A = T_{AX} - T_{AL}$)	ΔT _A	12.8	°R
Tank Insulation (pick from drop down list)		Not Insulated		Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Tank Construction (pick from drop down list)		Welded		Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Average Daily Vapor Temperature Range (Eq. 1-11: $\Delta T_A = T_{AX} - T_{AL}$)	ΔT _A	12.8	°R
Tank Construction (pick from drop down list)		Welded		Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Tank Shell Color (pick from drop down list)		White		Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Average Daily Vapor Temperature Range (Eq. 1-11: $\Delta T_A = T_{AX} - T_{AL}$)	ΔT _A	12.8	°R
Tank Shell Color (pick from drop down list)		White		Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Tank Shell Condition (pick from drop down list)		Average		Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Average Daily Vapor Temperature Range (Eq. 1-11: $\Delta T_A = T_{AX} - T_{AL}$)	ΔT _A	12.8	°R
Tank Shell Condition (pick from drop down list)		Average		Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Tank Interior Condition (pick from drop down list)		Light Rust		Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Average Daily Vapor Temperature Range (Eq. 1-11: $\Delta T_A = T_{AX} - T_{AL}$)	ΔT _A	12.8	°R
Tank Interior Condition (pick from drop down list)		Light Rust		Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Tank paint solar absorptance, dimensionless; Table 7.1-6	α	0.25		Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Average Daily Vapor Temperature Range (Eq. 1-11: $\Delta T_A = T_{AX} - T_{AL}$)	ΔT _A	12.8	°R
Tank paint solar absorptance, dimensionless; Table 7.1-6	α	0.25		Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	-0.03	psi	Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Average Daily Vapor Temperature Range (Eq. 1-11: $\Delta T_A = T_{AX} - T_{AL}$)	ΔT _A	12.8	°R
Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	-0.03	psi	Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	True Vapor Pressure; Eq. 1-25, $PVA = \exp(A - (B/TLA))$	P _{VA}	0.0354363	psi	Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Average Daily Vapor Temperature Range (Eq. 1-11: $\Delta T_A = T_{AX} - T_{AL}$)	ΔT _A	12.8	°R
True Vapor Pressure; Eq. 1-25, $PVA = \exp(A - (B/TLA))$	P _{VA}	0.0354363	psi	Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Not Insulated	P _{VA}	0.0354363	psi	Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Average Daily Vapor Temperature Range (Eq. 1-11: $\Delta T_A = T_{AX} - T_{AL}$)	ΔT _A	12.8	°R
Not Insulated	P _{VA}	0.0354363	psi	Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Partially Insulated	P _{VA}	0.0355263	psi	Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Average Daily Vapor Temperature Range (Eq. 1-11: $\Delta T_A = T_{AX} - T_{AL}$)	ΔT _A	12.8	°R
Partially Insulated	P _{VA}	0.0355263	psi	Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Fully Insulated	P _{VA}	0.0343132	psi	Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Average Daily Vapor Temperature Range (Eq. 1-11: $\Delta T_A = T_{AX} - T_{AL}$)	ΔT _A	12.8	°R
Fully Insulated	P _{VA}	0.0343132	psi	Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Average Daily Ambient Temperature (TAA) Eq. 1-30 $TAA = ((TAX + TAN) / 2)$	TAA	492.20	°R	Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Average Daily Vapor Temperature Range (Eq. 1-11: $\Delta T_A = T_{AX} - T_{AL}$)	ΔT _A	12.8	°R
Average Daily Ambient Temperature (TAA) Eq. 1-30 $TAA = ((TAX + TAN) / 2)$	TAA	492.20	°R	Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Average daily maximum ambient temperature; Table 7.1-7	TAX	498.80	°R	Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Average Daily Vapor Temperature Range (Eq. 1-11: $\Delta T_A = T_{AX} - T_{AL}$)	ΔT _A	12.8	°R
Average daily maximum ambient temperature; Table 7.1-7	TAX	498.80	°R	Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Average daily minimum ambient temperature; Table 7.1-7	TAN	485.60	°R	Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Average Daily Vapor Temperature Range (Eq. 1-11: $\Delta T_A = T_{AX} - T_{AL}$)	ΔT _A	12.8	°R
Average daily minimum ambient temperature; Table 7.1-7	TAN	485.60	°R	Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Liquid Bulk Temperature; Eq. 1-31: $TB = TAA + 0.003 \text{ or } 1$	TB	492.84	°R	Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Average Daily Vapor Temperature Range (Eq. 1-11: $\Delta T_A = T_{AX} - T_{AL}$)	ΔT _A	12.8	°R
Liquid Bulk Temperature; Eq. 1-31: $TB = TAA + 0.003 \text{ or } 1$	TB	492.84	°R	Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Average Daily Liquid Surface Temperature (TLA) Eq. 1-28, $TLA = 0.4 \cdot TAA + 0.6 \cdot TB + 0.005 \cdot \alpha \cdot I$	TLA	493.64	°R	Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Average Daily Vapor Temperature Range (Eq. 1-11: $\Delta T_A = T_{AX} - T_{AL}$)	ΔT _A	12.8	°R
Average Daily Liquid Surface Temperature (TLA) Eq. 1-28, $TLA = 0.4 \cdot TAA + 0.6 \cdot TB + 0.005 \cdot \alpha \cdot I$	TLA	493.64	°R	Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Partially Insulated; Eq. 1-29, $TLA = 0.3 \cdot TAA + 0.7 \cdot TB + 0.005 \cdot \alpha \cdot I$	TLA	493.70	°R	Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Average Daily Vapor Temperature Range (Eq. 1-11: $\Delta T_A = T_{AX} - T_{AL}$)	ΔT _A	12.8	°R
Partially Insulated; Eq. 1-29, $TLA = 0.3 \cdot TAA + 0.7 \cdot TB + 0.005 \cdot \alpha \cdot I$	TLA	493.70	°R	Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Fully Insulated; $TLA = TB$	TLA	492.8	°R	Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Average Daily Vapor Temperature Range (Eq. 1-11: $\Delta T_A = T_{AX} - T_{AL}$)	ΔT _A	12.8	°R
Fully Insulated; $TLA = TB$	TLA	492.8	°R	Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Average Vapor Temperature (Tv) Eq. 1-33, $Tv = 0.7 \cdot TAA + 0.3 \cdot TB + 0.009 \cdot \alpha \cdot I$	Tv	494.30	°R	Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Average Daily Vapor Temperature Range (Eq. 1-11: $\Delta T_A = T_{AX} - T_{AL}$)	ΔT _A	12.8	°R
Average Vapor Temperature (Tv) Eq. 1-33, $Tv = 0.7 \cdot TAA + 0.3 \cdot TB + 0.009 \cdot \alpha \cdot I$	Tv	494.30	°R	Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Partially Insulated; Eq. 1-34, $Tv = 0.6 \cdot TAA + 0.4 \cdot TB + 0.01 \cdot \alpha \cdot I$	Tv	494.57	°R	Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Average Daily Vapor Temperature Range (Eq. 1-11: $\Delta T_A = T_{AX} - T_{AL}$)	ΔT _A	12.8	°R
Partially Insulated; Eq. 1-34, $Tv = 0.6 \cdot TAA + 0.4 \cdot TB + 0.01 \cdot \alpha \cdot I$	Tv	494.57	°R	Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Fully Insulated; $Tv = TB$	Tv	492.84	°R	Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Average Daily Vapor Temperature Range (Eq. 1-11: $\Delta T_A = T_{AX} - T_{AL}$)	ΔT _A	12.8	°R
Fully Insulated; $Tv = TB$	Tv	492.84	°R	Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Stock Vapor Density; Eq. 1-22, $Wv = (Mv \cdot PVA) / (R \cdot Tv)$	Wv	8.685E-04		Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Average Daily Vapor Temperature Range (Eq. 1-11: $\Delta T_A = T_{AX} - T_{AL}$)	ΔT _A	12.8	°R
Stock Vapor Density; Eq. 1-22, $Wv = (Mv \cdot PVA) / (R \cdot Tv)$	Wv	8.685E-04		Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Not Insulated	Wv	8.685E-04		Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Average Daily Vapor Temperature Range (Eq. 1-11: $\Delta T_A = T_{AX} - T_{AL}$)	ΔT _A	12.8	°R
Not Insulated	Wv	8.685E-04		Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Partially Insulated	Wv	8.702E-04		Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Average Daily Vapor Temperature Range (Eq. 1-11: $\Delta T_A = T_{AX} - T_{AL}$)	ΔT _A	12.8	°R
Partially Insulated	Wv	8.702E-04		Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Fully Insulated	Wv	8.435E-04		Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Average Daily Vapor Temperature Range (Eq. 1-11: $\Delta T_A = T_{AX} - T_{AL}$)	ΔT _A	12.8	°R
Fully Insulated	Wv	8.435E-04		Average Daily Vapor Temperature Range	ΔT _v	11.76	°R					Average Daily Vapor Temperature Range	ΔT _v	11.76	°R	Average Daily Vapor Temperature Range (Eq. 1-11: $\Delta T_A = T_{AX} - T_{AL}$)	ΔT _A	12.8	°R

HAPS Speciation		lb/month		Vapor Mole Fraction	
Product	Eq. 40-2 $L_i = z_i(L_i)$	Eq. 40-6 $ZV_i = y_i M_i / MV$	Eq. 40-5 $y_i = P_i / PVA$		
Total HAP Emissions =	0.036				
Individual HAPS	L _i (lb/month)	M _i	M _v	Z _v	P _i = P _{v,i} (x _i)
hexane	0.0000	86.18	130	0.00000	0.00000
benzene	0.0000	78.11	130	0.00000	0.00000
2,2,4 TMP	0.0000	114.23	130	0.00000	0.00000
toluene	0.0000	92.14	130	0.00000	0.00000
ethylbenzene	0.0107	106.17	130	0.29329	0.011655
xylene	0.0257	106.17	130	0.70671	0.028084
naphthalene	0.0000	128.17	130	0.00E+00	0.00E+00
cumene	0.0000	120.19	130	0.00E+00	0.00E+00
Component Vapor Pressure	PVA _i = (0.0191537) ¹⁰ P _{v,i} (A-B)(TLA+C) _i				
Individual HAPS	Z _v	M _i	M _v	X _i	P _{v,i}
hexane	0.00000	130	86.18	0.00000	6.878
benzene	0.00000	130	78.11	0.00000	6.906
2,2,4 TMP	0.00000	130	114.23	0.00000	6.812
toluene	0.00000	130	92.14	0.00000	7.017
ethylbenzene	0.26400	130	106.17	0.32328	6.95
xylene	0.73600	130	106.17	0.90120	7.009
naphthalene	0.00000	130	128.17	0.00000	7.146
cumene	0.00000	130	120.19	0.00000	6.929

Monthly Calculations (continued)

SEPTEMBER

Tank No.	10459B	Symbol	Units	ROUTINE EMISSIONS CALCULATIONS	Symbol	Units
ROUTINE EMISSIONS CALCULATIONS						
Total Losses (Eq. 1-1: $LT = LS + LW$)	LT	0.14	lb/month	Standing Losses; Eq. 1-2: $LS = 365 (Vv \cdot Wv \cdot KE \cdot Ks)$	LS	0.05 lb/month
		7.20E-05	ton/month	Vapor Space Volume	Vv	19.7 ft ³
				Stock Vapor Density	Wv	0.0029 lb/ft ³
				Vapor Space Expansion Factor ($0 < KE <= 1$); Eq. 1-5	KE	0.028 per day
Nearest US Location	Bridgeport, CT			Vented Vapor Saturation Factor	Ks	1.00 NA
Daily total solar insolation on a horizontal surface; Table 7.1-7	I	1320.0	Btu/ft ² -day	Constant; Number of Daily Events in a Year	365	30 days/month
Absolute Pressure	P _a	14.69	psia	Working Losses; Eq. 1-35: $Lw = VQ \cdot KN \cdot Kp \cdot Wv \cdot KB$	Lw	0.10 lb/month
Ideal Gas Constant	R	10.73	psia ft ³ /lb-mole R	Net Working Loss Throughput (Eq. 1-39: $VO = 5.614 \cdot Q$)	VO	33 ft ³ /month
Product Information						
Product Type	Diesel Additive			Working Loss Turnover Factor Eq. 1-35 $Ks = (180 + N)/6N$ for N=36, else $Ks = 1$	KN	1.0000
Vapor Molecular weight	Mv	130	Lb/lb-mole	Working Loss Product Factor	Kp	1.00
Average organic liquid density	WL	6.10	lb/gal	Stock Vapor Density	Wv	0.0029 lb/ft ³
Average Reid Vapor Pressure	RVP	0.00	psi	Vent Setting Correction Factor	KB	1.00
Product factor: 0.4 for crude oils or 1 for other organic liquids	Kc	1.00		Vented Vapor Saturation Factor; Eq. 1-21: $Ks = 1 / (1 + 0.053 \cdot PVA \cdot Hvo)$	Ks	1.00
Vapor Pressure Equation Constant A	A	0.00		Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.1267 psia
Vapor Pressure Equation Constant B (Table 7.1-2)	B	0.0	R	Vapor Space Outage	Hvo	0.00 ft
Tank design data						
Shell height	Hs	2.49	ft	Vapor Space Expansion Factor (Eq. 1-5: $(\Delta Tv / TLA) \cdot (\Delta Pv - \Delta PVB) / (PA - PVA)$)	KE	0.0276 per day
Diameter	D	4.49	ft	Average Daily Vapor Temperature Range	ΔTv	16.75 °R
Throughput	Q	290	gal/month	Average Daily Vapor Pressure Range	ΔPv	0.0000 psia
Turnovers	N	10.32	per year	Breather Vent Pressure Setting Range (Equation 1-10: $\Delta PVB = PBP - PVB$)	ΔPVB	0.0000 psi
Roof type:		0.00		Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.1267 psia
Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft	Average Daily Liquid Surface Temperature	TLA	528.39 °R
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA	ft	Atmospheric Pressure	PA	14.69 psia
Maximum Filling Height - use (Pi/4)D if unknown	HLX	1.49	ft			
Minimum Filling Height (use 0 if unknown)	HLN	1.00	ft	Average Daily Vapor Temperature Range (ΔTv)		
Liquid height (assume 1/2 H)	HL	1.24	ft	Average daily ambient temperature range - Equation 1-11 ($\Delta TA = TAX - TA$)	ΔTA	14.5 °R
Tank insulation (pick from drop down list)		Not Insulated		Not Insulated - Equation 1-7 ($\Delta TV = 0.7 \Delta TA + 0.02 \alpha I$)	ΔTv	16.75 °R
Tank Construction (pick from drop down list)		Welded		Partially Insulated - Equation 1-8 ($\Delta TV = 0.6 \Delta TA + 0.02 \alpha R I$)	ΔTv	15.30 °R
Tank Shell Color (pick from drop down list)		White		Fully Insulated, constant temperature	ΔTv	0.00 °R
Tank Shell Condition (pick from drop down list)		Average				
Tank Interior Condition (pick from drop down list)		Light Rust		Average Daily Vapor Pressure Range (ΔPv)		
Tank paint solar absorptance, dimensionless; Table 7.1-6	α	0.25		Not Insulated - Equation 1-9: $\Delta Pv = PVX - PVN$	ΔPv	0.00000 psia
Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	-0.03	psi	Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25 $PVX = e^{PVA}$)	PVX	1.00000 psia
				Vapor pressure at ave daily min liquid surface temp. (Eq. 1-25 $PVN = e^{PVA}$)	PVN	1.00000 psia
				Average daily max. liquid surface temp.; Fig. 7.1-17 $TLX = TLA + 0.25 \Delta T$	TLX	532.58 °R
				Average daily min. liquid surface temp.; Fig. 7.1-17 $TLN = TLA - 0.25 \Delta T$	TLN	524.21 °R
True Vapor Pressure; Eq. 1-25: $PVA = \exp(A - (B/TLA))$						
Not Insulated	P _{VA}	0.1266829	psia	Partially Insulated - Equation 1-9: $\Delta Pv = PVX - PVN$	ΔPv	0.00000 psia
Partially Insulated	P _{VA}	0.1271055	psia	Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25 PVX)	PVX	1.00000 psia
Fully Insulated	P _{VA}	0.1214345	psia	Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25 PVN)	PVN	1.0000000 psia
Average Daily Ambient Temperature (TAA) Eq. 1-30 $TAA = ((TAX + TAN) / 2)$						
Average daily maximum ambient temperature; Table 7.1-7	TAX	533.40	°R	Average daily maximum liquid surface temperature, deg R ($TLX = TLA + TLX$)	TLX	532.32 °R
Average daily minimum ambient temperature; Table 7.1-7	TAN	518.90	°R	Average daily minimum liquid surface temperature, deg R ($TLN = TLA - TLN$)	TLN	524.67 °R
Liquid Bulk Temperature; Eq. 1-31: $TB = TAA + 0.003 \alpha I$						
	TB	527.14	°R	Fully Insulated ($\Delta Pv = 0$)	ΔPv	0.00 psia
Average Daily Liquid Surface Temperature (TLA)						
Not Insulated; Eq. 1-28: $TLA = 0.4 \cdot TAA + 0.6 \cdot TB + 0.005 \cdot \alpha I$	TLA	528.39	°R	Vapor Space Volume (Eq. 1-3: $Vv = (PI / 4) \cdot D^2 \cdot Hvo$)	Vv	19.69 ft ³
Partially Insulated; Eq. 1-29: $TLA = 0.3 \cdot TAA + 0.7 \cdot TB + 0.005 \cdot \alpha I$	TLA	528.49	°R	Effective Tank diameter	D _e	4.49 ft
Fully Insulated; $TLA = TB$	TLA	527.1	°R	Effective Tank Height	H _e	2.49 ft
				Vapor Space Outage $Hvo = 1/2 H$	Hvo	1.24 ft
Average Vapor Temperature (Tv)						
Not Insulated; Eq. 1-33: $Tv = 0.7 \cdot TAA + 0.3 \cdot TB + 0.009 \cdot \alpha I$	Tv	529.42	°R			
Partially Insulated; Eq. 1-34: $Tv = 0.6 \cdot TAA + 0.4 \cdot TB + 0.01 \cdot \alpha I$	Tv	529.85	°R			
Fully Insulated; $Tv = TB$	Tv	527.14	°R			
Stock Vapor Density; Eq. 1-22: $Wv = (Mv \cdot PVA) / (R \cdot Tv)$						
Not Insulated	Wv	2.899E-03				
Partially Insulated	Wv	2.906E-03				
Fully Insulated	Wv	2.791E-03				

HAPS Speciation	lb/month	Vapor Weight Concentration	Vapor Mole Fraction
Product			
Total HAP Emissions =	0.144	Eq. 40-6 $Zvi = yiMi / MV$	Eq. 40-5 $yi = Pi / PVA$
Eq. 40-2 $L_{i1} = Z_{i1}(L_1)$			
Individual HAPS			
hexane	0.0000	86.18	130
benzene	0.0000	78.11	130
2,2,4 TMP	0.0000	114.23	130
toluene	0.0000	92.14	130
ethylbenzene	0.0420	106.17	130
xylene	0.1021	106.17	130
naphthalene	0.0000	128.17	130
cumene	0.0000	120.19	130

Monthly Calculations (continued)

OCTOBER

Tank No.	10459B	Symbol	Units	ROUTINE EMISSIONS CALCULATIONS	Symbol	Units
ROUTINE EMISSIONS CALCULATIONS						
Total Losses (Eq. 1-1: $LT = LS + LW$)	LT	0.10	lb/month	Standing Losses; Eq. 1-2: $LS = 365 (Vv \cdot Wv \cdot KE \cdot Ks)$	LS	0.03 lb/month
		4.81E-05	ton/month	Vapor Space Volume	Vv	19.7 ft ³
				Stock Vapor Density	Wv	0.0020 lb/ft ³
				Vapor Space Expansion Factor ($0 < KE <= 1$); Eq. 1-5	KE	0.026 per day
Nearest US Location	Bridgeport, CT			Vented Vapor Saturation Factor	Ks	1.00 NA
Daily total solar insolation on a horizontal surface; Table 7.1-7	I	948.0	Btu/ft ² -day	Constant; Number of Daily Events in a Year	365	31 days/month
Absolute Pressure	P _a	14.69	psia	Working Losses; Eq. 1-35: $Lw = VQ \cdot KN \cdot Kp \cdot Wv \cdot KB$	Lw	0.07 lb/month
Ideal Gas Constant	R	10.73	psia ft ³ /lb-mole R	Net Working Loss Throughput (Eq. 1-39: $VO = 5.614 \cdot Q$)	VO	33 ft ³ /month
Product Information						
Product Type	Diesel Additive			Working Loss Turnover Factor Eq. 1-35 $Ks = (180 + N)/6N$ for N=36, else $Ks = 1$	KN	1.0000
Vapor Molecular weight	Mv	130	Lb/lb-mole	Working Loss Product Factor	Kp	1.00
Average organic liquid density	WL	6.10	lb/gal	Stock Vapor Density	Wv	0.0020 lb/ft ³
Average Reid Vapor Pressure	RVP	0.00	psi	Vent Setting Correction Factor	KB	1.00
Product factor: 0.4 for crude oils or 1 for other organic liquids	Kc	1.00		Vented Vapor Saturation Factor; Eq. 1-21: $Ks = 1 / (1 + 0.053 \cdot PVA \cdot Hvo)$	Ks	1.00
Vapor Pressure Equation Constant A	A	0.00		Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.0835 psia
Vapor Pressure Equation Constant B (Table 7.1-2)	B	0.0	R	Vapor Space Outage	Hvo	0.00 ft
Tank design data						
Shell height	Hs	2.49	ft	Vapor Space Expansion Factor (Eq. 1-5: $(\Delta Tv / TLA) \cdot (\Delta Pv - \Delta PVB) / (PA - PVA)$)	KE	0.0258 per day
Diameter	D	4.49	ft	Average Daily Vapor Temperature Range	ΔTv	15.45 °R
Throughput	Q	290	gal/month	Average Daily Vapor Pressure Range	ΔPv	0.0000 psia
Turnovers	N	9.99	per year	Breather Vent Pressure Setting Range (Equation 1-10: $\Delta PVB = PBP - PVB$)	ΔPVB	0.0000 psi
Roof type:		0.00		Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.0835 psia
Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft	Average Daily Liquid Surface Temperature	TLA	516.36 °R
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA	ft	Atmospheric Pressure	PA	14.69 psia
Maximum Filling Height - use (Pi/4)D if unknown	HLX	1.49	ft			
Minimum Filling Height (use 0 if unknown)	HLN	1.00	ft	Average Daily Vapor Temperature Range (ΔTv)		
Liquid height (assume 1/2 H)	HL	1.24	ft	Average daily ambient temperature range - Equation 1-11 ($\Delta TA = TAX - TA$)	ΔTA	15.3 °R
Tank insulation (pick from drop down list)		Not Insulated		Not Insulated - Equation 1-7 ($\Delta TV = 0.7 \Delta TA + 0.02 \alpha I$)	ΔTv	15.45 °R
Tank Construction (pick from drop down list)		Welded		Partially Insulated - Equation 1-8 ($\Delta TV = 0.6 \Delta TA + 0.02 \alpha R I$)	ΔTv	13.92 °R
Tank Shell Color (pick from drop down list)		White		Fully Insulated, constant temperature	ΔTv	0.00 °R
Tank Shell Condition (pick from drop down list)		Average				
Tank Interior Condition (pick from drop down list)		Light Rust		Average Daily Vapor Pressure Range (ΔPv)		
Tank paint solar absorptance, dimensionless; Table 7.1-6	α	0.25		Not Insulated - Equation 1-9: $\Delta Pv = PVX - PVN$	ΔPv	0.00000 psia
Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	0.03	psi	Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25 $PVX = e^{PVA}$)	PVX	1.00000 psia
				Vapor pressure at ave daily min liquid surface temp. (Eq. 1-25 $PVN = e^{PVA}$)	PVN	1.00000 psia
				Average daily max. liquid surface temp.; Fig. 7.1-17 $TLX = TLA + 0.25 \Delta T$	TLX	520.22 °R
				Average daily min. liquid surface temp.; Fig. 7.1-17 $TLN = TLA - 0.25 \Delta T$	TLN	512.50 °R
True Vapor Pressure; Eq. 1-25: $PVA = \exp(A - (B/TLA))$						
Not Insulated	P _{VA}	0.0835155	psia	Partially Insulated - Equation 1-9: $\Delta Pv = PVX - PVN$	ΔPv	0.00000 psia
Partially Insulated	P _{VA}	0.0837274	psia	Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25 PVX)	PVX	1.00000 psia
Fully Insulated	P _{VA}	0.0808716	psia	Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25 PVN)	PVN	1.0000000 psia
Average Daily Ambient Temperature (TAA) Eq. 1-30 $TAA = ((TAX + TAN) / 2)$						
Average daily maximum ambient temperature; Table 7.1-7	TAX	514.75	°R	Average daily maximum liquid surface temperature, deg R ($TLX = TLA + TLX$)	TLX	519.91 °R
Average daily minimum ambient temperature; Table 7.1-7	TAN	507.10	°R	Average daily minimum liquid surface temperature, deg R ($TLN = TLA - TLN$)	TLN	512.95 °R
Liquid Bulk Temperature; Eq. 1-31: $TB = TAA + 0.003 \alpha I$						
	TB	515.46	°R	Fully Insulated ($\Delta Pv = 0$)	ΔPv	0.00 psia
Average Daily Liquid Surface Temperature (TLA)						
Not Insulated; Eq. 1-28: $TLA = 0.4 \cdot TAA + 0.6 \cdot TB + 0.005 \cdot \alpha I$	TLA	516.36	°R	Vapor Space Volume (Eq. 1-3: $Vv = (PI / 4) \cdot D^2 \cdot Hvo$)	Vv	19.69 ft ³
Partially Insulated; Eq. 1-29: $TLA = 0.3 \cdot TAA + 0.7 \cdot TB + 0.005 \cdot \alpha I$	TLA	516.43	°R	Effective Tank diameter	D _e	4.49 ft
Fully Insulated; $TLA = TB$	TLA	515.5	°R	Effective Tank Height	H _e	2.49 ft
				Vapor Space Outage $Hvo = 1/2 H$	Hvo	1.24 ft
Average Vapor Temperature (Tv)						
Not Insulated; Eq. 1-33: $Tv = 0.7 \cdot TAA + 0.3 \cdot TB + 0.009 \cdot \alpha I$	Tv	517.10	°R			
Partially Insulated; Eq. 1-34: $Tv = 0.6 \cdot TAA + 0.4 \cdot TB + 0.01 \cdot \alpha I$	Tv	517.40	°R			
Fully Insulated; $Tv = TB$	Tv	515.46	°R			
Stock Vapor Density; Eq. 1-22: $Wv = (Mv \cdot PVA) / (R \cdot Tv)$						
Not Insulated	Wv	1.957E-03				
Partially Insulated	Wv	1.960E-03				
Fully Insulated	Wv	1.901E-03				

HAPS Speciation	lb/month	Vapor Weight Concentration	Vapor Mole Fraction
Product			
Total HAP Emissions =	0.096	Eq. 40-6 $Zvi = yiMi / MV$	Eq. 40-5 $yi = Pi / PVA$
Eq. 40-2 $L_{i1} = Z_{i1}(L_1)$			
Individual HAPS			
hexane	0.0000	86.18	130
benzene	0.0000	78.11	130
2,2,4 TMP	0.0000	114.23	130
toluene	0.0000	92.14	130
ethylbenzene	0.0281	106.17	130
xylene	0.0681	106.17	130
naphthalene	0.0000	128.17	130
cumene	0.0000	120.19	130

Monthly Calculations (continued)

NOVEMBER

Tank No.	10459B		NOVEMBER		Symbol		Units	
ROUTINE EMISSIONS CALCULATIONS				ROUTINE EMISSIONS CALCULATIONS				
Symbol	Units	Symbol	Units	Symbol	Units	Symbol	Units	
Total Losses (Eq. 1-1: LT = LS+LW)	LT	0.06 lb/month	Standing Losses; Eq. 1-2: LS = 365 (Vv * Wv * KE * Ks)	LS	0.02 lb/month	Vapor Space Volume	Vv	19.7 ft ³
		3.17E-05 ton/month	Stock Vapor Density	Wv	0.0014 lb/ft ³	Stock Vapor Density	Wv	0.0014 lb/ft ³
			Vapor Space Expansion Factor (0 < KE <= 1); Eq. 1-5	KE	0.021 per day	Vented Vapor Saturation Factor	Ks	1.00 NA
			Constant; Number of Daily Events in a Year	365		Net Working Loss Throughput (Eq. 1-35: LW = VQ * KN * Kp * Wv * KB)	LW	0.05 lb/month
Nearest US Location	Bridgeport, CT		Working Losses; Eq. 1-35: LW = VQ * KN * Kp * Wv * KB	LW	0.05 lb/month	Net Working Loss Throughput (Eq. 1-39: VQ=5.614*Q)	VQ	33 ft ³ /month
Daily total solar insolation on a horizontal surface; Table 7.1-7	I	621.0 Btu/ft ² -day	Working Loss Turnover Factor Eq. 1-35: Kp=(180+N)/6N for N>=36, else Kp=1	KN	1.0000	Working Loss Product Factor	Kp	1.00
Absolute Pressure	Pa	14.69 psia	Stock Vapor Density	Wv	0.0014 lb/ft ³	Vent Setting Correction Factor	KB	1.00
Ideal Gas Constant	R	10.73 psia ft ³ /lb-mole R	Vented Vapor Saturation Factor; Eq. 1-21: Ks = 1/(1+(0.053*Pv/A*Hvo))	Ks	1.00	Vapor Pressure at Avg Daily Liq Surface Temp	PvA	0.0581 psia
Product Information			Vapor Space Volume (Eq. 1-3: Vv = (PI / 4) D² Hvo)	Vv	19.69 ft ³	Vapor Space Outage	Hvo	0.00 ft
Product Type	Diesel Additive		Effective Tank diameter	Dt	4.49 ft			
Vapor Molecular weight	Mv	130 lb/lb-mole	Effective Tank Height	Ht	2.49 ft			
Average organic liquid density	WL	6.10 lb/gal	Vapor Space Outage Hvo = 1/2 Ht	Hvo	1.24 ft			
Average Reid Vapor Pressure	RVP	0.00						
Product factor: 0.4 for crude oils or 1 for other organic liquids	Kc	1.00						
Vapor Pressure Equation Constant A	A	0.00						
Vapor Pressure Equation Constant B (Table 7.1-2)	B	0.0 R						
Tank design data								
Shell height	Hs	2.49 ft						
Diameter	D	4.49 ft						
Throughput	Q	250 gal/month						
Turnovers	N	10.32 per year						
Roof type:	0.00							
Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625 ft/ft						
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA ft						
Maximum Filling Height -use (Pi/4)D if unknown	HLX	1.49 ft						
Minimum Filling Height (use 0 if unknown)	HLN	1.00 ft						
Liquid height (assume 1/2 Ht)	HL	1.24 ft						
Tank insulation (pick from drop down list)	Not Insulated							
Tank Construction (pick from drop down list)	Welded							
Tank Shell Color (pick from drop down list)	White							
Tank Shell Condition (pick from drop down list)	Average							
Tank Interior Condition (pick from drop down list)	Light Rust							
Tank paint solar absorptance, dimensionless, Table 7.1-6	alpha	0.25						
Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	-0.03 psi						
True Vapor Pressure; Eq. 1-25: PvA = exp(A-(B/TLA))								
Not Insulated	PvA	0.0580534						
Partially Insulated	PvA	0.0581547						
Fully Insulated	PvA	0.0567834						
Average Daily Ambient Temperature (TAA) Eq. 1-30 TAA = ((TAX+1)	TAA	505.35 °R						
Average daily maximum ambient temperature, Table 7.1-7	TAX	512.10 °R						
Average daily minimum ambient temperature, Table 7.1-7	TAN	498.60 °R						
Liquid Bulk Temperature; Eq. 1-31: TB = TAA + 0.003 as l	TB	505.62 °R						
Average Daily Liquid Surface Temperature (TLA)								
Not Insulated; Eq. 1-28: TLA = 0.4*TAA + 0.6*TB + 0.005*alpha	TLA	506.41 °R						
Partially Insulated; Eq. 1-29: TLA = 0.3*TAA + 0.7*TB + 0.005*alpha	TLA	506.45 °R						
Fully Insulated: TLA = TB	TLA	505.8 °R						
Average Vapor Temperature (Tv)								
Not Insulated; Eq. 1-33: Tv = 0.7*TAA + 0.3*TB + 0.009*alpha	Tv	506.89 °R						
Partially Insulated; Eq. 1-34: Tv = 0.6*TAA + 0.4*TB + 0.01*alpha	Tv	507.09 °R						
Fully Insulated; Tv = TB	Tv	505.82 °R						
Stock Vapor Density; Eq. 1-22: Wv = (Mv/PvA)/(R*Tv)								
Not Insulated	Wv	1.387E-03						
Partially Insulated	Wv	1.389E-03						
Fully Insulated	Wv	1.360E-03						

HAPS Speciation		lb/month		Vapor Mole Fraction	
Product	additive			Eq. 40-5 yi = Pi / PVA	
Total HAP Emissions =	0.063	Vapor Weight Concentration		Eq. 40-6 Zvi = yiMi / MV	
Eq. 40-2 L _i = Z _i (L _T)					
Individual HAPS	L _i (lb/month)	M _i	M _v	Z _{vi}	P _i = P _{vA} (X _i)
hexane	0.0000	86.18	130	0.00000	0.00000
benzene	0.0000	78.11	130	0.00000	0.00000
2,2,4 TMP	0.0000	114.23	130	0.00000	0.00000
toluene	0.0000	92.14	130	0.00000	0.00000
ethylbenzene	0.0185	106.17	130	0.29247	0.020789
xylene	0.0448	106.17	130	0.70753	0.050294
naphthalene	0.0000	128.17	130	0.00E+00	0.00E+00
cumene	0.0000	120.19	130	0.00E+00	0.00E+00

Monthly Calculations (continued)

DECEMBER

Tank No.	10459B		DECEMBER		Symbol		Units	
ROUTINE EMISSIONS CALCULATIONS				ROUTINE EMISSIONS CALCULATIONS				
Symbol	Units	Symbol	Units	Symbol	Units	Symbol	Units	
Total Losses (Eq. 1-1: LT = LS+LW)	LT	0.04 lb/month	Standing Losses; Eq. 1-2: LS = 365 (Vv * Wv * KE * Ks)	LS	0.01 lb/month	Vapor Space Volume	Vv	19.7 ft ³
		2.16E-05 ton/month	Stock Vapor Density	Wv	0.0010 lb/ft ³	Stock Vapor Density	Wv	0.0010 lb/ft ³
			Vapor Space Expansion Factor (0 < KE <= 1); Eq. 1-5	KE	0.019 per day	Vented Vapor Saturation Factor	Ks	1.00 NA
			Constant; Number of Daily Events in a Year	365		Net Working Loss Throughput (Eq. 1-35: LW = VQ * KN * Kp * Wv * KB)	LW	0.03 lb/month
Nearest US Location	Bridgeport, CT		Working Losses; Eq. 1-35: LW = VQ * KN * Kp * Wv * KB	LW	0.03 lb/month	Net Working Loss Throughput (Eq. 1-39: VQ=5.614*Q)	VQ	33 ft ³ /month
Daily total solar insolation on a horizontal surface; Table 7.1-7	I	501.0 Btu/ft ² -day	Working Loss Turnover Factor Eq. 1-35: Kp=(180+N)/6N for N>=36, else Kp=1	KN	1.0000	Working Loss Product Factor	Kp	1.00
Absolute Pressure	Pa	14.69 psia	Stock Vapor Density	Wv	0.0010 lb/ft ³	Vent Setting Correction Factor	KB	1.00
Ideal Gas Constant	R	10.73 psia ft ³ /lb-mole R	Vented Vapor Saturation Factor; Eq. 1-21: Ks = 1/(1+(0.053*Pv/A*Hvo))	Ks	1.00	Vapor Pressure at Avg Daily Liq Surface Temp	PvA	0.0395 psia
Product Information			Vapor Space Volume (Eq. 1-3: Vv = (PI / 4) D² Hvo)	Vv	19.69 ft ³	Vapor Space Outage	Hvo	0.00 ft
Product Type	Diesel Additive		Effective Tank diameter	Dt	4.49 ft			
Vapor Molecular weight	Mv	130 lb/lb-mole	Effective Tank Height	Ht	2.49 ft			
Average organic liquid density	WL	6.10 lb/gal	Vapor Space Outage Hvo = 1/2 Ht	Hvo	1.24 ft			
Average Reid Vapor Pressure	RVP	0.00						
Product factor: 0.4 for crude oils or 1 for other organic liquids	Kc	1.00						
Vapor Pressure Equation Constant A	A	0.00						
Vapor Pressure Equation Constant B (Table 7.1-2)	B	0.0 R						
Tank design data								
Shell height	Hs	2.49 ft						
Diameter	D	4.49 ft						
Throughput	Q	250 gal/month						
Turnovers	N	9.99 per year						
Roof type:	0.00							
Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625 ft/ft						
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA ft						
Maximum Filling Height -use (Pi/4)D if unknown	HLX	1.49 ft						
Minimum Filling Height (use 0 if unknown)	HLN	1.00 ft						
Liquid height (assume 1/2 Ht)	HL	1.24 ft						
Tank insulation (pick from drop down list)	Not Insulated							
Tank Construction (pick from drop down list)	Welded							
Tank Shell Color (pick from drop down list)	White							
Tank Shell Condition (pick from drop down list)	Average							
Tank Interior Condition (pick from drop down list)	Light Rust							
Tank paint solar absorptance, dimensionless, Table 7.1-6	alpha	0.25						
Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	0.03 psi						
True Vapor Pressure; Eq. 1-25: PvA = exp(A-(B/TLA))								
Not Insulated	PvA	0.0394603						
Partially Insulated	PvA	0.0395187						
Fully Insulated	PvA	0.0387265						
Average Daily Ambient Temperature (TAA) Eq. 1-30 TAA = ((TAX+1)	TAA	495.50 °R						
Average daily maximum ambient temperature, Table 7.1-7	TAX	501.80 °R						
Average daily minimum ambient temperature, Table 7.1-7	TAN	489.20 °R						
Liquid Bulk Temperature; Eq. 1-31: TB = TAA + 0.003 as l	TB	495.88 °R						
Average Daily Liquid Surface Temperature (TLA)								
Not Insulated; Eq. 1-28: TLA = 0.4*TAA + 0.6*TB + 0.005*alpha	TLA	496.35 °R						
Partially Insulated; Eq. 1-29: TLA = 0.3*TAA + 0.7*TB + 0.005*alpha	TLA	496.39 °R						
Fully Insulated: TLA = TB	TLA	495.9 °R						
Average Vapor Temperature (Tv)								
Not Insulated; Eq. 1-33: Tv = 0.7*TAA + 0.3*TB + 0.009*alpha	Tv	496.74 °R						
Partially Insulated; Eq. 1-34: Tv = 0.6*TAA + 0.4*TB + 0.01*alpha	Tv	496.90 °R						
Fully Insulated; Tv = TB	Tv	495.88 °R						
Stock Vapor Density; Eq. 1-22: Wv = (Mv/PvA)/(R*Tv)								
Not Insulated	Wv	9.624E-04						
Partially Insulated	Wv	9.635E-04						
Fully Insulated	Wv	9.461E-04						

HAPS Speciation		lb/month		Vapor Mole Fraction	
Product	additive			Eq. 40-5 yi = Pi / PVA	
Total HAP Emissions =	0.043	Vapor Weight Concentration		Eq. 40-6 Zvi = yiMi / MV	
Eq. 40-2 L _i = Z _i (L _T)					
Individual HAPS	L _i (lb/month)	M _i	M _v	Z _{vi}	P _i = P _{vA} (X _i)
hexane	0.0000	86.18	130	0.00000	0.00000
benzene	0.0000	78.11	130	0.00000	0.00000
2,2,4 TMP	0.0000	114.23	130	0.00000	0.00000
toluene	0.0000	92.14	130	0.00000	0.00000
ethylbenzene	0.0126	106.17	130	0.29303	0.014158
xylene	0.0305	106.17	130	0.70697	0.034159
naphthalene	0.0000	128.17	130	0.00E+00	0.0

Monthly Calculations - JANUARY

10460		BRIDGEPORT, CT		ROUTINE EMISSIONS CALCULATIONS		ROUTINE EMISSIONS CALCULATIONS		HAPS Speciation		Diesel						
Symbol	Units	Symbol	Units	Symbol	Units	Symbol	Units	Product	ib/month	Vapor Mole Fraction						
Total Losses (Eq. 1-1: LT = LS+LW)	LT	0.01	lb/month	Standing Losses: Eq. 1-2, $L_s = 365 (V_v \cdot W_v \cdot K_e \cdot K_s)$	Ls	0.00	lb/month	Total HAP Emissions =	0.000	Vapor Weight Concentration						
Daily total solar insolation on a horizontal surface, Table 7.1-7	I	560.0	Btu/ft ² -day	Vapor Space Volume	Vv	47.5	ft ³	Eq. 40-2 $L_i = Z_i(L_s)$		Vapor Mole Fraction						
Nearest US Location		Bridgeport, CT		Stock Vapor Density	Wv	0.0001	lb/ft ³			Eq. 40-5 $y_i = P_i / PVA$						
Absolute Pressure	P _a	14.69	psi	Vapor Space Expansion Factor (0 < K _e <= 1); Eq. 1-5	KE	0.020	per day	Individual HAPS	L_i (lb/month)	M_i	M_v	Z_{0i}	P_i = P_{v,i}(K_e)	P_{v,i}	y_i	
Ideal Gas Constant	R	10.73	psia ft ³ /lb-mole R	Vented Vapor Saturation Factor	Ks	1.00	NA	hexane	0.0000	86.18	130	0.00052	0.000002	0.002	0.00078	
Product Information				Working Losses: Eq. 1-35, $L_w = VQ \cdot KN \cdot K_p \cdot W_v \cdot KB$	Lw	0.00	lb/month	benzene	0.0000	78.11	130	0.00302	0.000012	0.002	0.00503	
Product Type	Distillate Fuel Oil No. 2			Net Working Loss Throughput (Eq. 1-39: $VQ=5.614 \cdot Q$)	VQ	55	ft ³ /month	toluene	0.0001	92.14	130	0.02475	0.000095	0.002	0.03491	
Vapor Molecular weight	Mv	130	lb/lb-mole	Working Loss Turnover Factor Eq. 1-35 $K_e=(180+N)/6N$ for N=36, else $K_e=KN$	KN	1.0000		ethylbenzene	0.0000	106.17	130	0.00280	0.000008	0.002	0.0343	
Average organic liquid density	WL	7.10	lb/gal	Stock Vapor Density	Wv	0.0001	lb/ft ³	xylene	0.0003	106.17	130	0.05394	0.000160	0.002	0.06605	
Average Reid Vapor Pressure	RVP	0.02	psi	Vent Setting Correction Factor	KB	1.00		naphthalene	0.0000	128.17	130	2.72E-04	6.69E-07	0.002	2.76E-04	
Product factor: 0.4 for crude oils or 1 for other organic liquids	Kc	1.00		Vented Vapor Saturation Factor; Eq. 1-21, $K_s = 1/(1+0.053 \cdot PVA \cdot Hvo)$	Ks	1.00		cumene	0.0000	120.19	130	0.00E+00	0.00E+00	0.002	0.00E+00	
Vapor Pressure Equation Constant A	A	12.10		Vapor Pressure at Avg Daily Liq Surface Temp	PvA	0.0024	psia	Liquid Mole Fraction								
Vapor Pressure Equation Constant B (Table 7.1-2)	B	8907.0	°R	Vapor Space Outage	Hvo	0.00	ft	Eq. 40-4 $x_i = (Z_i M_i) / M_i$								
Tank design data				Vapor Space Expansion Factor (Eq. 1-5: $(\Delta T_v / TLA) + (\Delta P_v - \Delta P_B) / (P_A - P_vA)$)	KE	0.0199	per day	Component Vapor Pressure								
Shell height	Hs	4.32	ft	Average Daily Vapor Temperature Range	ΔTv	11.76	°R	Eq. 40-3 $PVA_i = (0.019337) / (PVA_i \cdot B / (TLA \cdot C))$								
Diameter	D	5.29	ft	Average Daily Vapor Pressure Range	ΔPv	0.0005	psia	hexane	0.00000	188	86.18	0.00000	6.878	1171.5	224.37	0.8715
Throughput	Q	410	gal/month	Not Insulated - Equation 1-7 ($\Delta T_v = 0.7 \Delta T_A + 0.02 \sigma I$)	ΔTv	11.76	°R	benzene	0.00001	188	78.11	0.00002	6.906	1211	220.79	0.5064
Turnovers	N	6.79	per year	Partially Insulated - Equation 1-8 ($\Delta T_v = 0.6 \Delta T_A + 0.02 \sigma R I$)	ΔTv	10.48	°R	2,2,4 TMP	0.00000	188	114.23	0.00000	6.812	1257.8	220.74	0.2495
Roof Type:		0.00		Fully Insulated, constant temperature	ΔTv	0.00	°R	toluene	0.00032	188	92.14	0.00065	7.017	1377.6	222.64	0.1296
Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft					ethylbenzene	0.00013	188	106.17	0.00023	6.95	1419.3	212.61	0.3361
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA	ft					xylene	0.00230	188	106.17	0.00514	7.009	1462.3	215.11	0.0312
Maximum Filling Height - use (Pi/4)D if unknown	HLX	3.32	ft					naphthalene	0.00076	188	128.17	0.00111	7.146	1831.6	211.82	0.0006
Minimum Filling Height (use 0 if unknown)	HLN	1.00	ft					cumene	0.00000	188	120.19	0.00000	6.929	1455.8	207.2	0.0153
Liquid height (assume 1/2 H)	HL	2.16	ft	Average Daily Vapor Pressure Range (ΔPv)	ΔPv	0.00053	psia	Eq. 40-6 $ZV_i = y_i M_i / MV$								
Tank Insulation (pick from drop down list)		Not Insulated		Not Insulated - Equation 1-9: $\Delta P_v = P_v X - P_v N$	ΔPv	0.00270	psia	Eq. 40-5 $y_i = P_i / PVA$								
Tank Construction (pick from drop down list)		Welded		Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25 $P_v X = \exp(\Delta P_v)$)	PvX	0.00270	psia	Eq. 40-4 $x_i = (Z_i M_i) / M_i$								
Tank Shell Color (pick from drop down list)		White		Vapor pressure at ave daily min liquid surface temp. (Eq. 1-25 $P_v N = \exp(-\Delta P_v)$)	PvN	0.00217	psia	hexane	0.00000	86.18	130	0.00051	0.000002	0.003	0.00077	
Tank Shell Condition (pick from drop down list)		Average		Average daily max. liquid surface temp.; Fig. 7.1-17 $TLX = TLA + 0.25 \Delta T_v$	TLX	494.39	°R	benzene	0.00000	78.11	130	0.00299	0.000013	0.003	0.00498	
Tank Interior Condition (pick from drop down list)		Light Rust		Average daily min. liquid surface temp.; Fig. 7.1-17 $TLN = TLA - 0.25 \Delta T_v$	TLN	488.87	°R	toluene	0.00001	92.14	130	0.02467	0.000091	0.003	0.03481	
Tank paint solar absorptance, dimensionless, Table 7.1-6	σ	0.25						ethylbenzene	0.00000	106.17	130	0.00282	0.000009	0.003	0.0345	
Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	-0.03	psi					xylene	0.0003	106.17	130	0.05436	0.000175	0.003	0.06656	
True Vapor Pressure; Eq. 1-25, $P_vA = \exp(A - (B/TLA))$								naphthalene	0.00000	128.17	130	2.82E-04	7.50E-07	0.003	2.86E-04	
Not Insulated	P _{vA}	0.0024228	psia	Partially Insulated - Equation 1-9: $\Delta P_v = P_v X - P_v N$	ΔPv	0.00047	psia	cumene	0.00000	120.19	130	0.00E+00	0.00E+00	0.003	0.00E+00	
Partially Insulated	P _{vA}	0.0024265	psia	Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25 us $P_v X$)	PvX	0.00267	psia	Component Vapor Pressure								
Fully Insulated	P _{vA}	0.0023756	psia	Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25 us $P_v N$)	PvN	0.002019	psia	Eq. 40-3 $PVA_i = (0.019337) / (PVA_i \cdot B / (TLA \cdot C))$								
Average Daily Ambient Temperature (TAA) Eq. 1-30 $TAA = ((TAX + TAN) / 2)$	TAA	490.50	°R					hexane	0.00000	188	86.18	0.00000	6.878	1171.5	224.37	0.8715
Average daily maximum ambient temperature, Table 7.1-7	TAX	496.90	°R					benzene	0.00001	188	78.11	0.00002	6.906	1211	220.79	0.5064
Average daily minimum ambient temperature, Table 7.1-7	TAN	484.10	°R					2,2,4 TMP	0.00000	188	114.23	0.00000	6.812	1257.8	220.74	0.2495
Liquid Bulk Temperature; Eq. 1-31: $TB = TAA + 0.003 \sigma I$	TB	490.92	°R					toluene	0.00032	188	92.14	0.00065	7.017	1377.6	222.64	0.1296
Average Daily Liquid Surface Temperature (TLA)				Vapor Space Volume (Eq. 1-3: $V_v = (PI / 4) D^2 Hvo$)	Vv	47.52	ft ³	ethylbenzene	0.00013	188	106.17	0.00023	6.95	1419.3	212.61	0.3361
Not Insulated; Eq. 1-28, $TLA = 0.4 \cdot TAA + 0.6 \cdot TB + 0.005 \cdot \sigma I$	TLA	491.45	°R	Effective Tank diameter	D _e	5.29	ft	xylene	0.00230	188	106.17	0.00514	7.009	1462.3	215.11	0.0312
Partially Insulated; Eq. 1-29, $TLA = 0.3 \cdot TAA + 0.7 \cdot TB + 0.005 \cdot \sigma R I$	TLA	491.49	°R	Effective Tank Height	H _e	4.32	ft	naphthalene	0.00076	188	128.17	0.00111	7.146	1831.6	211.82	0.0006
Fully Insulated; $TLA = TB$	TLA	490.9	°R	Vapor Space Outage $Hvo = 1/2 H$	Hvo	2.16	ft	cumene	0.00000	188	120.19	0.00000	6.929	1455.8	207.2	0.0153
Average Vapor Temperature (Tv)								Eq. 40-6 $ZV_i = y_i M_i / MV$								
Not Insulated; Eq. 1-33, $Tv = 0.7 \cdot TAA + 0.3 \cdot TB + 0.009 \cdot \sigma I$	Tv	491.89	°R					Eq. 40-5 $y_i = P_i / PVA$								
Partially Insulated; Eq. 1-34, $Tv = 0.6 \cdot TAA + 0.4 \cdot TB + 0.01 \cdot \sigma R I$	Tv	492.07	°R					Eq. 40-4 $x_i = (Z_i M_i) / M_i$								
Fully Insulated; $Tv = TB$	Tv	490.92	°R					hexane	0.00000	86.18	130	0.00052	0.000002	0.002	0.00078	
Stock Vapor Density; Eq. 1-22, $W_v = (M_v \cdot PVA) / (R \cdot Tv)$								benzene	0.00001	188	78.11	0.00002	6.906	1211	220.79	0.5064
Not Insulated	Wv	5.967E-05	lb/ft ³					2,2,4 TMP	0.00000	188	114.23	0.00000	6.812	1257.8	220.74	0.2495
Partially Insulated	Wv	5.974E-05	lb/ft ³					toluene	0.00032	188	92.14	0.00065	7.017	1377.6	222.64	0.1296
Fully Insulated	Wv	5.862E-05	lb/ft ³					ethylbenzene	0.00013	188	106.17	0.00023	6.95	1419.3	212.61	0.3361

Monthly Calculations (continued)

10460		BRIDGEPORT, CT		ROUTINE EMISSIONS CALCULATIONS		ROUTINE EMISSIONS CALCULATIONS		HAPS Speciation		Diesel						
Symbol	Units	Symbol	Units	Symbol	Units	Symbol	Units	Product	ib/month	Vapor Mole Fraction						
Total Losses (Eq. 1-1: LT = LS+LW)	LT	0.01	lb/month	Standing Losses: Eq. 1-2, $L_s = 365 (V_v \cdot W_v \cdot K_e \cdot K_s)$	Ls	0.00	lb/month	Total HAP Emissions =	0.000	Vapor Weight Concentration						
Daily total solar insolation on a horizontal surface, Table 7.1-7	I	847.0	Btu/ft ² -day	Vapor Space Volume	Vv	47.5	ft ³	Eq. 40-2 $L_i = Z_i(L_s)$		Vapor Mole Fraction						
Nearest US Location		Bridgeport, CT		Stock Vapor Density	Wv	0.0001	lb/ft ³			Eq. 40-5 $y_i = P_i / PVA$						
Absolute Pressure	P _a	14.69	psi	Vapor Space Expansion Factor (0 < K _e <= 1); Eq. 1-5	KE	0.023	per day	Individual HAPS	L_i (lb/month)	M_i	M_v	Z_{0i}	P_i = P_{v,i}(K_e)	P_{v,i}	y_i	
Ideal Gas Constant	R	10.73	psia ft ³ /lb-mole R	Vented Vapor Saturation Factor	Ks	1.00	NA	hexane	0.0000	86.18	130	0.00051	0.000002	0.003	0.00077	
Product Information				Working Losses: Eq. 1-35, $L_w = VQ \cdot KN \cdot K_p \cdot W_v \cdot KB$	Lw	0.00	lb/month	benzene	0.0000	78.11	130	0.00299	0.000013	0.003	0.00498	
Product Type	Distillate Fuel Oil No. 2			Net Working Loss Throughput (Eq. 1-39: $VQ=5.614 \cdot Q$)	VQ	55	ft ³ /month	toluene	0.0001	92.14	130	0.02467	0.000091	0.003	0.03481	
Vapor Molecular weight	Mv	130	lb/lb-mole	Working Loss Turnover Factor Eq. 1-35 $K_e=(180+N)/6N$ for N=36, else $K_e=KN$	KN	1.0000		ethylbenzene	0.0000	106.17	130	0.00282	0.000009	0.003	0.0345	
Average organic liquid density	WL	7.10	lb/gal	Stock Vapor Density	Wv	0.0001	lb/ft ³	xylene	0.0003	106.17	130	0.05436	0.000175	0.003	0.06656	
Average Reid Vapor Pressure	RVP	0.02	psi	Vent Setting Correction Factor	KB	1.00		naphthalene	0.0000	128.17	130	2.82E-04	7.50E-07	0.003	2.86E-04	
Product factor: 0.4 for crude oils or 1 for other organic liquids	Kc	1.00		Vented Vapor Saturation Factor; Eq. 1-21, $K_s = 1/(1+0.053 \cdot PVA \cdot Hvo)$	Ks	1.00		cumene	0.0000	120.19	130	0.00E+00	0.00E+00	0.003	0.00E+00	
Vapor Pressure Equation Constant A	A	12.10		Vapor Pressure at Avg Daily Liq Surface Temp	PvA	0.0026	psia	Liquid Mole Fraction								
Vapor Pressure Equation Constant B (Table 7.1-2)	B	8907.0	°R	Vapor Space Outage	Hvo	0.00	ft	Eq. 40-4 $x_i = (Z_i M_i) / M_i$								
Tank design data				Vapor Space Expansion Factor (Eq. 1-5: $(\Delta T_v / TLA) + (\Delta P_v - \Delta P_B) / (P_A - P_vA)$)	KE	0.0233	per day	Component Vapor Pressure								
Shell height	Hs	4.32	ft	Average Daily Vapor Temperature Range	ΔTv	13.48	°R	Eq. 40-3 $PVA_i = (0.019337) / (PVA_i \cdot B / (TLA \cdot C))$								
Diameter	D	5.29	ft	Average Daily Vapor Pressure Range	ΔPv	0.0008	psia	hexane	0.00000	188	86.18	0.00000	6.878	1171.5	224.37	0.8715
Throughput	Q	410	gal/month	Not Insulated - Equation 1-7 ($\Delta T_v = 0.7 \Delta T_A + 0.02 \sigma I$)	ΔTv	13.48	°R	benzene	0.00001	188	78.11	0.00002	6.906	1211	220.79	0.5064
Turnovers	N	7.52	per year													

Monthly Calculations (continued)

MARCH

Tank No.	ROUTINE EMISSIONS CALCULATIONS	Symbol	Units	ROUTINE EMISSIONS CALCULATIONS	Symbol	Units	HAPS Speciation	ib/month	Product	ib/month	Vapor Weight Concentration	Vapor Mole Fraction		
	Total Losses (Eq. 1-1: LT = LS+LW)	LT	0.01	Standing Losses; Eq. 1-2, $LS = 365 (Vv \cdot Wv \cdot KE \cdot Ks)$	LS	0.00	Total HAP Emissions =	0.001	Diesel					
			3.91E-06	Vapor Space Volume	Vv	47.5	Eq. 40-2 $Z_i = y_i / (L_i)$							
			ton/month	Stock Vapor Density	Wv	0.0001								
				Vapor Space Expansion Factor ($0 < KE \leq 1$); Eq. 1-5	KE	0.027								
				Vented Vapor Saturation Factor	Ks	1.00	Individual HAPS	L_i (lb/month)	M	M _v	Z _{0i}	$P_i = P_{v,i}(K)$	$P_{v,i}$	y_i
				Constant: Number of Daily Events in a Year	365	30	hexane	0.0000	86.18	130	0.00049	0.000003	0.003	0.00073
				Nearest US Location	Bridgeport, CT		benzene	0.0000	78.11	130	0.00288	0.000016	0.003	0.00479
				Daily total solar insolation on a horizontal surface; Table 7.1-7	I	1156.0	2,2,4 TMP	0.0000	114.23	130	0.00000	0.000000	0.003	0.00445
				Absolute Pressure	P _a	14.69	toluene	0.0000	92.14	130	0.02399	0.000168	0.005	0.03384
				Ideal Gas Constant	R	10.73	ethylbenzene	0.0000	106.17	130	0.00296	0.000018	0.005	0.03622
				Product Information			xylenes	0.0007	106.17	130	0.05737	0.000348	0.005	0.07024
				Product Type	Distillate Fuel Oil No. 2		naphthalene	0.0000	128.17	130	3.13E-04	1.08E-06	0.003	3.18E-04
				Vapor Molecular weight	Mv	130	cumene	0.0000	120.19	130	0.00E+00	0.00E+00	0.003	0.00E+00
				Average organic liquid density	WL	7.10								
				Average Reid Vapor Pressure	RVP	0.02								
				Product factor: 0.4 for crude oils or 1 for other organic liquids	Kc	1.00								
				Vapor Pressure Equation Constant A	A	12.10								
				Vapor Pressure Equation Constant B (Table 7.1-2)	B	8907.0								
				Tank design data										
				Shell height	Hs	4.32								
				Diameter	D	5.29								
				Throughput	Q	410								
				Turnovers	N	6.79								
				Roof Type:	0.00									
				Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625								
				Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA								
				Maximum Filling Height - use (Pi/4)D if unknown	HLX	3.32								
				Minimum Filling Height (use 0 if unknown)	HLN	1.00								
				Liquid height (assume 1/2 H)	HL	2.16								
				Tank insulation (pick from drop down list)	Not Insulated									
				Tank Construction (pick from drop down list)	Welded									
				Tank Shell Color (pick from drop down list)	White									
				Tank Shell Condition (pick from drop down list)	Average									
				Tank Interior Condition (pick from drop down list)	Light Rust									
				Tank paint solar absorptance, dimensionless; Table 7.1-6	α	0.25								
				Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	0.03								
				True Vapor Pressure; Eq. 1-25, $PvA = \exp(A-(B/TLA))$	P _{Va}	0.003406								
				Not Insulated	P _{Va}	0.003406								
				Partially Insulated	P _{Va}	0.0034165								
				Fully Insulated	P _{Va}	0.0032754								
				Average Daily Ambient Temperature (TAA) Eq. 1-30 $TAA = ((TAX+1)/N)$	TAA	498.90								
				Average daily maximum ambient temperature; Table 7.1-7	TAX	506.00								
				Average daily minimum ambient temperature; Table 7.1-7	TAN	491.80								
				Liquid Bulk Temperature; Eq. 1-31: $TB = TAA + 0.003 \text{ or } 1$	TB	499.77								
				Average Daily Liquid Surface Temperature (TLA)										
				Not Insulated; Eq. 1-28, $TLA = 0.4 \cdot TAA + 0.6 \cdot TB + 0.005 \cdot \alpha \cdot I$	TLA	500.87								
				Partially Insulated; Eq. 1-29, $TLA = 0.3 \cdot TAA + 0.7 \cdot TB + 0.005 \cdot \alpha \cdot R$	TLA	500.95								
				Fully Insulated; $TLA = TB$	TLA	499.8								
				Average Vapor Temperature (Tv)										
				Not Insulated; Eq. 1-33, $Tv = 0.7 \cdot TAA + 0.3 \cdot TB + 0.009 \cdot \alpha \cdot I$	Tv	501.76								
				Partially Insulated; Eq. 1-34, $Tv = 0.6 \cdot TAA + 0.4 \cdot TB + 0.01 \cdot \alpha \cdot R$	Tv	502.14								
				Fully Insulated; $Tv = TB$	Tv	499.77								
				Stock Vapor Density; Eq. 1-22, $Wv = (Mv \cdot PvA) / (R \cdot Tv)$	Wv	8.222E-05								
				Not Insulated	Wv	8.222E-05								
				Partially Insulated	Wv	8.242E-05								
				Fully Insulated	Wv	7.940E-05								

Monthly Calculations (continued)

APRIL

Tank No.	ROUTINE EMISSIONS CALCULATIONS	Symbol	Units	ROUTINE EMISSIONS CALCULATIONS	Symbol	Units	HAPS Speciation	ib/month	Product	ib/month	Vapor Weight Concentration	Vapor Mole Fraction		
	Total Losses (Eq. 1-1: LT = LS+LW)	LT	0.01	Standing Losses; Eq. 1-2, $LS = 365 (Vv \cdot Wv \cdot KE \cdot Ks)$	LS	0.01	Total HAP Emissions =	0.001	Diesel					
			5.84E-06	Vapor Space Volume	Vv	47.5	Eq. 40-2 $Z_i = y_i / (L_i)$							
			ton/month	Stock Vapor Density	Wv	0.0001								
				Vapor Space Expansion Factor ($0 < KE \leq 1$); Eq. 1-5	KE	0.032								
				Vented Vapor Saturation Factor	Ks	1.00	Individual HAPS	L_i (lb/month)	M	M _v	Z _{0i}	$P_i = P_{v,i}(K)$	$P_{v,i}$	y_i
				Constant: Number of Daily Events in a Year	365	30	hexane	0.0000	86.18	130	0.00045	0.000003	0.005	0.00068
				Nearest US Location	Bridgeport, CT		benzene	0.0000	78.11	130	0.00272	0.000022	0.005	0.00453
				Daily total solar insolation on a horizontal surface; Table 7.1-7	I	1490.0	2,2,4 TMP	0.0000	114.23	130	0.00000	0.000000	0.005	0.00453
				Absolute Pressure	P _a	14.69	toluene	0.0000	92.14	130	0.02399	0.000168	0.005	0.03384
				Ideal Gas Constant	R	10.73	ethylbenzene	0.0000	106.17	130	0.00296	0.000018	0.005	0.03622
				Product Information			xylenes	0.0007	106.17	130	0.05737	0.000348	0.005	0.07024
				Product Type	Distillate Fuel Oil No. 2		naphthalene	0.0000	128.17	130	3.13E-04	1.08E-06	0.003	3.18E-04
				Vapor Molecular weight	Mv	130	cumene	0.0000	120.19	130	0.00E+00	0.00E+00	0.003	0.00E+00
				Average organic liquid density	WL	7.10								
				Average Reid Vapor Pressure	RVP	0.02								
				Product factor: 0.4 for crude oils or 1 for other organic liquids	Kc	1.00								
				Vapor Pressure Equation Constant A	A	12.10								
				Vapor Pressure Equation Constant B (Table 7.1-2)	B	8907.0								
				Tank design data										
				Shell height	Hs	4.32								
				Diameter	D	5.29								
				Throughput	Q	410								
				Turnovers	N	7.02								
				Roof Type:	0.00									
				Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625								
				Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA								
				Maximum Filling Height - use (Pi/4)D if unknown	HLX	3.32								
				Minimum Filling Height (use 0 if unknown)	HLN	1.00								
				Liquid height (assume 1/2 H)	HL	2.16								
				Tank insulation (pick from drop down list)	Not Insulated									
				Tank Construction (pick from drop down list)	Welded									
				Tank Shell Color (pick from drop down list)	White									
				Tank Shell Condition (pick from drop down list)	Average									
				Tank Interior Condition (pick from drop down list)	Light Rust									
				Tank paint solar absorptance, dimensionless; Table 7.1-6	α	0.25								
				Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	0.03								
				True Vapor Pressure; Eq. 1-25, $PvA = \exp(A-(B/TLA))$	P _{Va}	0.0049604								
				Not Insulated	P _{Va}	0.0049604								
				Partially Insulated	P _{Va}	0.0049793								
				Fully Insulated	P _{Va}	0.0047266								
				Average Daily Ambient Temperature (TAA) Eq. 1-30 $TAA = ((TAX+1)/N)$	TAA	509.15								
				Average daily maximum ambient temperature; Table 7.1-7	TAX	516.80								
				Average daily minimum ambient temperature; Table 7.1-7	TAN	501.50								
				Liquid Bulk Temperature; Eq. 1-31: $TB = TAA + 0.003 \text{ or } 1$	TB	510.27								
				Average Daily Liquid Surface Temperature (TLA)										
				Not Insulated; Eq. 1-28, $TLA = 0.4 \cdot TAA + 0.6 \cdot TB + 0.005 \cdot \alpha \cdot I$	TLA	511.68								
				Partially Insulated; Eq. 1-29, $TLA = 0.3 \cdot TAA + 0.7 \cdot TB + 0.005 \cdot \alpha \cdot R$	TLA	511.79								
				Fully Insulated; $TLA = TB$	TLA	510.3								
				Average Vapor Temperature (Tv)										

Monthly Calculations (continued)

JULY

Tank No.	10460	Units		Units		Units		ib/month	
ROUTINE EMISSIONS CALCULATIONS		Symbol		ROUTINE EMISSIONS CALCULATIONS		Symbol		HAPS Speciation	
ROUTINE EMISSIONS CALCULATIONS		Symbol		ROUTINE EMISSIONS CALCULATIONS		Symbol		ib/month	
Total Losses (Eq. 1-1: LT = LS+LW)	LT	0.03	lb/month	Standing Losses; Eq. 1-2, $LS = 365 (Vv \cdot Wv \cdot KE \cdot Ks)$	LS	0.01	lb/month	Total HAP Emissions =	0.002
Time Period	July			Vapor Space Volume	Vv	47.5	ft ³	Eq. 40-6 $Zvi = yMi / MV$	
Nearest US Location	Bridgeport, CT			Stock Vapor Density	Wv	0.0003	lb/ft ³	Eq. 40-5 $yi = Pi / PVA$	
Daily total solar insolation on a horizontal surface; Table 7.1-7	I	1904.0	Btu/ft ² -day	Vapor Space Expansion Factor ($0 < KE \leq 1$); Eq. 1-5	KE	0.033	per day	Individual HAPS	
Absolute Pressure	PA	14.69	psia	Vented Vapor Saturation Factor	Ks	1.00	NA	hexane	0.0000
Ideal Gas Constant	R	10.73	psia ft ³ /lb-mole R	Constant: Number of Daily Events in a Year	365	31	days/month	benzene	0.0001
Product Information				Working Losses; Eq. 1-35, $Lw = VO \cdot KN \cdot Kp \cdot Wv \cdot KB$	LW	0.01	lb/month	toluene	0.0000
Product Type	Distillate Fuel Oil No. 2			Net Working Loss Throughput (Eq. 1-39: $VQ=5.614 \cdot Q$)	NV	55	ft ³ /month	ethylbenzene	0.0001
Vapor Molecular weight	Mv	130	lb/lb-mole	Working Loss Turnover Factor Eq. 1-35: $Kp=(180+N)/6N$ for N>36, else $Kp=1$	KN	1.0000		xylene	0.0016
Average organic liquid density	WL	7.10	lb/gal	Working Loss Product Factor	Kp	1.00		naphthalene	0.0000
Average Reid Vapor Pressure	RVP	0.02	psia	Stock Vapor Density	Wv	0.0003	lb/ft ³	cumene	0.0000
Product factor: 0.4 for crude oils or 1 for other organic liquids	Kc	1.00		Vent Setting Correction Factor	KB	1.00			
Vapor Pressure Equation Constant A	A	12.10		Vented Vapor Saturation Factor; Eq. 1-21, $Ks = 1/(1+0.053 \cdot PVA \cdot Hvo)$	Ks	1.00			
Vapor Pressure Equation Constant B (Table 7.1-2)	B	8907.0	°R	Vapor Pressure at Avg Daily Lq Surface Temp	PvA	0.0113	psia		
				Vapor Space Outage	Hvo	0.00	ft		
Tank design data				Vapor Space Expansion Factor (Eq. 1-5: $(\Delta T_v/TLA) + (\Delta P_v - \Delta P_b)/(PA - PVA)$)	KE	0.0326	per day		
Shell height	Hs	4.32	ft	Average Daily Vapor Temperature Range	ΔTv	19.69	°R		
Diameter	D	5.29	ft	Average Daily Vapor Pressure Range	ΔPv	0.0034	psia		
Throughput	Q	410	gal/month	Breather Vent Pressure Setting Range (Equation 1-10: $\Delta P_b = PBP - P_b$)	ΔPb	0.0600	psi		
Turnovers	N	6.79	per year	Vapor Pressure at Avg Daily Lq Surface Temp	PvA	0.0113	psia		
Roof Type:		0.00		Average Daily Liquid Surface Temperature	TLA	537.14	°R		
Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft	Atmospheric Pressure	PA	14.69	psia		
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA	ft						
Maximum Filling Height - use (Pi/4)D if unknown	HLX	3.32	ft						
Minimum Filling Height (use 0 if unknown)	HLN	1.00	ft						
Liquid height (assume 1/2 H)	HL	2.16	ft						
Tank insulation (pick from drop down list)		Not Insulated							
Tank Construction (pick from drop down list)		Welded							
Tank Shell Color (pick from drop down list)		White							
Tank Shell Condition (pick from drop down list)		Average							
Tank Interior Condition (pick from drop down list)		Light Rust							
Tank paint solar absorptance, dimensionless; Table 7.1-6	α	0.25							
Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	0.03	psi						
True Vapor Pressure; Eq. 1-25, $PvA = \exp(A - (B/TLA))$									
Not Insulated	PvA	0.0113179							
Partially Insulated	PvA	0.0113679							
Fully Insulated	PvA	0.0107012							
Average Daily Ambient Temperature (TAA) Eq. 1-30 $TAA = ((TAX+1) TAA)$	TAA	533.90	°R						
Average daily maximum ambient temperature; Table 7.1-7	TAX	541.10	°R						
Average daily minimum ambient temperature; Table 7.1-7	TAN	526.70	°R						
Liquid Bulk Temperature; Eq. 1-31: $TB = TAA + 0.003 \text{ or } 1$	TB	535.33	°R						
Average Daily Liquid Surface Temperature (TLA)									
Not Insulated; Eq. 1-28, $TLA = 0.4 \cdot TAA + 0.6 \cdot TB + 0.005 \cdot \alpha \cdot I$	TLA	537.14	°R						
Partially Insulated; Eq. 1-29, $TLA = 0.3 \cdot TAA + 0.7 \cdot TB + 0.005 \cdot \alpha \cdot R$	TLA	537.28	°R						
Fully Insulated; $TLA = TB$	TLA	535.3	°R						
Average Vapor Temperature (Tv)									
Not Insulated; Eq. 1-33, $Tv = 0.7 \cdot TAA + 0.3 \cdot TB + 0.009 \cdot \alpha \cdot I$	Tv	538.61	°R						
Partially Insulated; Eq. 1-34, $Tv = 0.6 \cdot TAA + 0.4 \cdot TB + 0.01 \cdot \alpha \cdot R$	Tv	539.23	°R						
Fully Insulated; $Tv = TB$	Tv	535.33	°R						
Stock Vapor Density; Eq. 1-22, $Wv = (Mv \cdot PvA)/(R \cdot Tv)$									
Not Insulated	Wv	2.546E-04							
Partially Insulated	Wv	2.554E-04							
Fully Insulated	Wv	2.422E-04							

Monthly Calculations (continued)

AUGUST

Tank No.	10460	Units		Units		Units		ib/month	
ROUTINE EMISSIONS CALCULATIONS		Symbol		ROUTINE EMISSIONS CALCULATIONS		Symbol		HAPS Speciation	
ROUTINE EMISSIONS CALCULATIONS		Symbol		ROUTINE EMISSIONS CALCULATIONS		Symbol		ib/month	
Total Losses (Eq. 1-1: LT = LS+LW)	LT	0.02	lb/month	Standing Losses; Eq. 1-2, $LS = 365 (Vv \cdot Wv \cdot KE \cdot Ks)$	LS	0.01	lb/month	Total HAP Emissions =	0.002
Time Period	August			Vapor Space Volume	Vv	47.5	ft ³	Eq. 40-6 $Zvi = yMi / MV$	
Nearest US Location	Bridgeport, CT			Stock Vapor Density	Wv	0.0002	lb/ft ³	Eq. 40-5 $yi = Pi / PVA$	
Daily total solar insolation on a horizontal surface; Table 7.1-7	I	1685.0	Btu/ft ² -day	Vapor Space Expansion Factor ($0 < KE \leq 1$); Eq. 1-5	KE	0.030	per day	Individual HAPS	
Absolute Pressure	PA	14.69	psia	Vented Vapor Saturation Factor	Ks	1.00	NA	hexane	0.0000
Ideal Gas Constant	R	10.73	psia ft ³ /lb-mole R	Constant: Number of Daily Events in a Year	365	31	days/month	benzene	0.0001
Product Information				Working Losses; Eq. 1-35, $Lw = VO \cdot KN \cdot Kp \cdot Wv \cdot KB$	LW	0.01	lb/month	toluene	0.0000
Product Type	Distillate Fuel Oil No. 2			Net Working Loss Throughput (Eq. 1-39: $VQ=5.614 \cdot Q$)	NV	55	ft ³ /month	ethylbenzene	0.0001
Vapor Molecular weight	Mv	130	lb/lb-mole	Working Loss Turnover Factor Eq. 1-35: $Kp=(180+N)/6N$ for N>36, else $Kp=1$	KN	1.0000		xylene	0.0015
Average organic liquid density	WL	7.10	lb/gal	Working Loss Product Factor	Kp	1.00		naphthalene	0.0000
Average Reid Vapor Pressure	RVP	0.02	psia	Stock Vapor Density	Wv	0.0002	lb/ft ³	cumene	0.0000
Product factor: 0.4 for crude oils or 1 for other organic liquids	Kc	1.00		Vent Setting Correction Factor	KB	1.00			
Vapor Pressure Equation Constant A	A	12.10		Vented Vapor Saturation Factor; Eq. 1-21, $Ks = 1/(1+0.053 \cdot PVA \cdot Hvo)$	Ks	1.00			
Vapor Pressure Equation Constant B (Table 7.1-2)	B	8907.0	°R	Vapor Pressure at Avg Daily Lq Surface Temp	PvA	0.0109	psia		
				Vapor Space Outage	Hvo	0.00	ft		
Tank design data				Vapor Space Expansion Factor (Eq. 1-5: $(\Delta T_v/TLA) + (\Delta P_v - \Delta P_b)/(PA - PVA)$)	KE	0.0299	per day		
Shell height	Hs	4.32	ft	Average Daily Vapor Temperature Range	ΔTv	18.09	°R		
Diameter	D	5.29	ft	Average Daily Vapor Pressure Range	ΔPv	0.0031	psia		
Throughput	Q	410	gal/month	Breather Vent Pressure Setting Range (Equation 1-10: $\Delta P_b = PBP - P_b$)	ΔPb	0.0600	psi		
Turnovers	N	6.79	per year	Vapor Pressure at Avg Daily Lq Surface Temp	PvA	0.0109	psia		
Roof Type:		0.00		Average Daily Liquid Surface Temperature	TLA	536.06	°R		
Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft	Atmospheric Pressure	PA	14.69	psia		
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA	ft						
Maximum Filling Height - use (Pi/4)D if unknown	HLX	3.32	ft						
Minimum Filling Height (use 0 if unknown)	HLN	1.00	ft						
Liquid height (assume 1/2 H)	HL	2.16	ft						
Tank insulation (pick from drop down list)		Not Insulated							
Tank Construction (pick from drop down list)		Welded							
Tank Shell Color (pick from drop down list)		White							
Tank Shell Condition (pick from drop down list)		Average							
Tank Interior Condition (pick from drop down list)		Light Rust							
Tank paint solar absorptance, dimensionless; Table 7.1-6	α	0.25							
Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	0.03	psi						
True Vapor Pressure; Eq. 1-25, $PvA = \exp(A - (B/TLA))$									
Not Insulated	PvA	0.0109487							
Partially Insulated	PvA	0.0109916							
Fully Insulated	PvA	0.0104171							
Average Daily Ambient Temperature (TAA) Eq. 1-30 $TAA = ((TAX+1) TAA)$	TAA	533.20	°R						
Average daily maximum ambient temperature; Table 7.1-7	TAX	540.10	°R						
Average daily minimum ambient temperature; Table 7.1-7	TAN	526.30	°R						
Liquid Bulk Temperature; Eq. 1-31: $TB = TAA + 0.003 \text{ or } 1$	TB	534.46	°R						
Average Daily Liquid Surface Temperature (TLA)									
Not Insulated; Eq. 1-28, $TLA = 0.4 \cdot TAA + 0.6 \cdot TB + 0.005 \cdot \alpha \cdot I$	TLA	536.06	°R						
Partially Insulated; Eq. 1-29, $TLA = 0.3 \cdot TAA + 0.7 \cdot TB + 0.005 \cdot \alpha \cdot R$	TLA	536.19	°R						
Fully Insulated; $TLA = TB$	TLA	534.5	°R						
Average Vapor Temperature (Tv)									
Not Insulated; Eq. 1-33, $Tv = 0.7 \cdot TAA + 0.3 \cdot TB + 0.009 \cdot \alpha \cdot I$	Tv	537.37	°R						
Partially Insulated; Eq. 1-34, $Tv = 0.6 \cdot TAA + 0.4 \cdot TB + 0.01 \cdot \alpha \cdot R$	Tv	537.92	°R						
Fully Insulated; $Tv = TB$	Tv	534.46	°R						
Stock Vapor Density; Eq. 1-22, $Wv = (Mv \cdot PvA)/(R \cdot Tv)$									
Not Insulated	Wv	2.488E-04							
Partially Insulated	Wv	2.475E-04							
Fully Insulated	Wv	2.361E-04							

Monthly Calculations (continued)

SEPTEMBER

Tank No.	10460	Symbol	Units	ROUTINE EMISSIONS CALCULATIONS	Symbol	Units	HAPS Speciation	ib/month
ROUTINE EMISSIONS CALCULATIONS								
Total Losses (Eq. 1-1: $LT = LS + LW$)	LT		0.02	ib/month	Vapor Space Volume	Vv	47.5	ft ³
Nearest US Location	Bridgeport, CT				Stock Vapor Density	Vw	0.0002	lb/ft ³
Daily total solar insolation on a horizontal surface; Table 7.1-7	I	1320.0	Btu/ft ² -day	Vapor Space Expansion Factor ($0 < KE \leq 1$); Eq. 1-5	KE	0.028	per day	
Absolute Pressure	Pa	14.69	psia	Vented Vapor Saturation Factor	Ks	1.00	NA	
Ideal Gas Constant	R	10.73	psia ft ³ /lb-mole R	Constant: Number of Daily Events in a Year	365	31	days/month	
Product Information								
Product Type	Distillate Fuel Oil No. 2			Working Losses; Eq. 1-35: $LW = VO \cdot KN \cdot Kp \cdot Wv \cdot KB$	Lw	0.01	lb/month	
Vapor Molecular weight	Mv	130	lb/lb-mole	Net Working Loss Throughput (Eq. 1-39: $VQ = 5.614 \cdot Q$)	VQ	55	ft ³ /month	
Average organic liquid density	WL	7.10	lb/gal	Working Loss Turnover Factor Eq. 1-35: $Kp = (180 + N) / (N + 36)$, else $Kp = 1$	Kp	1.0000		
Average Reid Vapor Pressure	RVP	0.02	psia	Working Loss Product Factor	Kp	1.00		
Product factor: 0.4 for crude oils or 1 for other organic liquids	Kc	1.00		Stock Vapor Density	Vw	0.0002	lb/ft ³	
Vapor Pressure Equation Constant A	A	12.10		Vent Setting Correction Factor	Kb	1.00		
Vapor Pressure Equation Constant B (Table 7.1-2)	B	8907.0	R	Vented Vapor Saturation Factor; Eq. 1-21: $Ks = 1 / (1 + 0.053 \cdot PVA \cdot Hvo)$	Ks	1.00		
Vapor Pressure at Avg Daily Liq Surface Temp	PvA	0.0058	psia	Vapor Space Volume (Eq. 1-3: $Vv = (PI / 4) \cdot D^2 \cdot Hvo$)	Vv	47.52	ft ³	
Vapor Space Outage	Hvo	0.00	ft	Effective Tank diameter	De	5.29	ft	
Tank design data				Effective Tank Height	He	4.32	ft	
Shell height	Hs	4.32	ft	Vapor Space Outage $Hvo = 1/2 H$	Hvo	2.16	ft	
Diameter	D	5.29	ft	Vapor Space Expansion Factor (Eq. 1-5: $(\Delta T_v / TLA) + (\Delta P_v - \Delta P_B) / (PA - PVA)$)				
Turnovers	N	7.02	per year	Average Daily Vapor Temperature Range	ΔTv	16.75	R	
Roof Type:		0.00		Average Daily Vapor Pressure Range	ΔPv	0.0023	psia	
Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft	Breather Vent Pressure Setting Range (Equation 1-10: $\Delta P_B = PBP - PBV$)	ΔPB	0.0600	psi	
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA	ft	Vapor Pressure at Avg Daily Liq Surface Temp	PvA	0.0058	psia	
Maximum Filling Height - use (Pi/4)D if unknown	HLX	3.32	ft	Average Daily Liquid Surface Temperature	TLA	528.39	R	
Minimum Filling Height (use 0 if unknown)	HLN	1.00	ft	Atmospheric Pressure	PA	14.69	psia	
Liquid height (assume 1/2 H)	HL	2.16	ft	Average Daily Vapor Temperature Range (ΔTv)				
Tank insulation (pick from drop down list)		Not Insulated		Average daily ambient temperature range - Equation 1-11 ($\Delta TA = TAX - TA$)	ΔTA	14.5	R	
Tank Construction (pick from drop down list)		Welded		Not Insulated - Equation 1-7 ($\Delta TV = 0.7 \Delta TA + 0.02 \sigma I$)	ΔTv	16.75	R	
Tank Shell Color (pick from drop down list)		White		Partially Insulated - Equation 1-8 ($\Delta TV = 0.6 \Delta TA + 0.02 \sigma R I$)	ΔTv	15.30	R	
Tank Shell Condition (pick from drop down list)		Average		Fully Insulated, constant temperature	ΔTv	0.00	R	
Tank Interior Condition (pick from drop down list)		Light Rust		Average Daily Vapor Pressure Range (ΔPv)				
Tank paint solar absorptance, dimensionless; Table 7.1-6	α	0.25		Not Insulated - Equation 1-9: $\Delta PV = PVX - PVN$	ΔPv	0.00230	psia	
Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	0.03	psi	Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25: $PvX = \exp(PvA)$)	PvX	0.00583	psia	
True Vapor Pressure; Eq. 1-25: $PvA = \exp(A - B/TLA)$				Vapor pressure at ave. daily min liquid surface temp. (Eq. 1-25: $PvN = \exp(PvA)$)	PvN	0.00752	psia	
Not Insulated	PvA	0.0086022		Average daily max. liquid surface temp.; Fig. 7.1-17: $TLX = TLA + 0.25 \Delta T$	TLX	532.58	R	
Partially Insulated	PvA	0.0086294		Average daily min. liquid surface temp.; Fig. 7.1-17: $TLN = TLA - 0.25 \Delta T$	TLN	524.21	R	
Fully Insulated	PvA	0.0082641		Partially Insulated - Equation 1-9: $\Delta PV = PVX - PVN$				
Average Daily Ambient Temperature (TAA) Eq. 1-30: $TAA = ((TAX + TAN) / 2)$				Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25: PvX)	PvX	0.00974	psia	
Average daily maximum ambient temperature; Table 7.1-7	TAX	533.40	R	Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25: PvN)	PvN	0.007617	psia	
Average daily minimum ambient temperature; Table 7.1-7	TAN	518.90	R	Average daily maximum liquid surface temperature, deg R ($TLX = TLA + TLX$)	TLX	532.32	R	
				Average daily minimum liquid surface temperature, deg R ($TLN = TLA - TLN$)	TLN	524.67	R	
Liquid Bulk Temperature; Eq. 1-31: $TB = TAA + 0.003 \sigma I$				Fully Insulated (ΔPv = 0)				
	TB	527.14	R	ΔPv	0.00	psia		
Average Daily Liquid Surface Temperature (TLA)				Vapor Space Volume (Eq. 1-3: $Vv = (PI / 4) \cdot D^2 \cdot Hvo$)				
Not Insulated; Eq. 1-28: $TLA = 0.4 \cdot TAA + 0.6 \cdot TB + 0.005 \sigma I$	TLA	528.39	R	Effective Tank diameter	De	5.29	ft	
Partially Insulated; Eq. 1-29: $TLA = 0.3 \cdot TAA + 0.7 \cdot TB + 0.005 \sigma R I$	TLA	528.49	R	Effective Tank Height	He	4.32	ft	
Fully Insulated; $TLA = TB$	TLA	527.1	R	Vapor Space Outage $Hvo = 1/2 H$	Hvo	2.16	ft	
Average Vapor Temperature (Tv)				Average Vapor Temperature (Tv)				
Not Insulated; Eq. 1-33: $Tv = 0.7 \cdot TAA + 0.3 \cdot TB + 0.009 \sigma I$	Tv	529.42	R					
Partially Insulated; Eq. 1-34: $Tv = 0.6 \cdot TAA + 0.4 \cdot TB + 0.01 \sigma R I$	Tv	529.85	R					
Fully Insulated; $Tv = TB$	Tv	527.14	R					
Stock Vapor Density; Eq. 1-22: $Wv = (Mv \cdot PVA) / (R \cdot Tv)$								
Not Insulated	Wv	1.968E-04						
Partially Insulated	Wv	1.973E-04						
Fully Insulated	Wv	1.899E-04						

Monthly Calculations (continued)

OCTOBER

Tank No.	10460	Symbol	Units	ROUTINE EMISSIONS CALCULATIONS	Symbol	Units	HAPS Speciation	ib/month
ROUTINE EMISSIONS CALCULATIONS								
Total Losses (Eq. 1-1: $LT = LS + LW$)	LT		0.01	ib/month	Vapor Space Volume	Vv	47.5	ft ³
Nearest US Location	Bridgeport, CT				Stock Vapor Density	Vw	0.0001	lb/ft ³
Daily total solar insolation on a horizontal surface; Table 7.1-7	I	948.0	Btu/ft ² -day	Vapor Space Expansion Factor ($0 < KE \leq 1$); Eq. 1-5	KE	0.028	per day	
Absolute Pressure	Pa	14.69	psia	Vented Vapor Saturation Factor	Ks	1.00	NA	
Ideal Gas Constant	R	10.73	psia ft ³ /lb-mole R	Constant: Number of Daily Events in a Year	365	31	days/month	
Product Information								
Product Type	Distillate Fuel Oil No. 2			Working Losses; Eq. 1-35: $LW = VO \cdot KN \cdot Kp \cdot Wv \cdot KB$	Lw	0.01	lb/month	
Vapor Molecular weight	Mv	130	lb/lb-mole	Net Working Loss Throughput (Eq. 1-39: $VQ = 5.614 \cdot Q$)	VQ	55	ft ³ /month	
Average organic liquid density	WL	7.10	lb/gal	Working Loss Turnover Factor Eq. 1-35: $Kp = (180 + N) / (N + 36)$, else $Kp = 1$	Kp	1.0000		
Average Reid Vapor Pressure	RVP	0.02	psia	Working Loss Product Factor	Kp	1.00		
Product factor: 0.4 for crude oils or 1 for other organic liquids	Kc	1.00		Stock Vapor Density	Vw	0.0001	lb/ft ³	
Vapor Pressure Equation Constant A	A	12.10		Vent Setting Correction Factor	Kb	1.00		
Vapor Pressure Equation Constant B (Table 7.1-2)	B	8907.0	R	Vented Vapor Saturation Factor; Eq. 1-21: $Ks = 1 / (1 + 0.053 \cdot PVA \cdot Hvo)$	Ks	1.00		
Vapor Pressure at Avg Daily Liq Surface Temp	PvA	0.0058	psia	Vapor Space Volume (Eq. 1-3: $Vv = (PI / 4) \cdot D^2 \cdot Hvo$)	Vv	47.52	ft ³	
Vapor Space Outage	Hvo	0.00	ft	Effective Tank diameter	De	5.29	ft	
Tank design data				Effective Tank Height	He	4.32	ft	
Shell height	Hs	4.32	ft	Vapor Space Outage $Hvo = 1/2 H$	Hvo	2.16	ft	
Diameter	D	5.29	ft	Vapor Space Expansion Factor (Eq. 1-5: $(\Delta T_v / TLA) + (\Delta P_v - \Delta P_B) / (PA - PVA)$)				
Turnovers	N	6.79	per year	Average Daily Vapor Temperature Range	ΔTv	15.45	R	
Roof Type:		0.00		Average Daily Vapor Pressure Range	ΔPv	0.0015	psia	
Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft	Breather Vent Pressure Setting Range (Equation 1-10: $\Delta P_B = PBP - PBV$)	ΔPB	0.0600	psi	
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA	ft	Vapor Pressure at Avg Daily Liq Surface Temp	PvA	0.0058	psia	
Maximum Filling Height - use (Pi/4)D if unknown	HLX	3.32	ft	Average Daily Liquid Surface Temperature	TLA	516.36	R	
Minimum Filling Height (use 0 if unknown)	HLN	1.00	ft	Atmospheric Pressure	PA	14.69	psia	
Liquid height (assume 1/2 H)	HL	2.16	ft	Average Daily Vapor Temperature Range (ΔTv)				
Tank insulation (pick from drop down list)		Not Insulated		Average daily ambient temperature range - Equation 1-11 ($\Delta TA = TAX - TA$)	ΔTA	15.3	R	
Tank Construction (pick from drop down list)		Welded		Not Insulated - Equation 1-7 ($\Delta TV = 0.7 \Delta TA + 0.02 \sigma I$)	ΔTv	16.75	R	
Tank Shell Color (pick from drop down list)		White		Partially Insulated - Equation 1-8 ($\Delta TV = 0.6 \Delta TA + 0.02 \sigma R I$)	ΔTv	13.32	R	
Tank Shell Condition (pick from drop down list)		Average		Fully Insulated, constant temperature	ΔTv	0.00	R	
Tank Interior Condition (pick from drop down list)		Light Rust		Average Daily Vapor Pressure Range (ΔPv)				
Tank paint solar absorptance, dimensionless; Table 7.1-6	α	0.25		Not Insulated - Equation 1-9: $\Delta PV = PVX - PVN$	ΔPv	0.00150	psia	
Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	0.03	psi	Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25: $PvX = \exp(PvA)$)	PvX	0.00580	psia	
True Vapor Pressure; Eq. 1-25: $PvA = \exp(A - B/TLA)$				Vapor pressure at ave. daily min liquid surface temp. (Eq. 1-25: $PvN = \exp(PvA)$)	PvN	0.00510	psia	
Not Insulated	PvA	0.0058079		Average daily max. liquid surface temp.; Fig. 7.1-17: $TLX = TLA + 0.25 \Delta T$	TLX	520.22	R	
Partially Insulated	PvA	0.0058217		Average daily min. liquid surface temp.; Fig. 7.1-17: $TLN = TLA - 0.25 \Delta T$	TLN	512.50	R	
Fully Insulated	PvA	0.0056355		Partially Insulated - Equation 1-9: $\Delta PV = PVX - PVN$				
Average Daily Ambient Temperature (TAA) Eq. 1-30: $TAA = ((TAX + TAN) / 2)$				Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25: PvX)	PvX	0.00653	psia	
Average daily maximum ambient temperature; Table 7.1-7	TAX	522.40	R	Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25: PvN)	PvN	0.0051788	psia	
Average daily minimum ambient temperature; Table 7.1-7	TAN	507.10	R	Average daily maximum liquid surface temperature, deg R ($TLX = TLA + TLX$)	TLX	519.91	R	
				Average daily minimum liquid surface temperature, deg R ($TLN = TLA - TLN$)	TLN	512.95	R	
Liquid Bulk Temperature; Eq. 1-31: $TB = TAA + 0.003 \sigma I$				Fully Insulated (ΔPv = 0)				
	TB	515.46	R	ΔPv	0.00	psia		
Average Daily Liquid Surface Temperature (TLA)				Vapor Space Volume (Eq. 1-3: $Vv = (PI / 4) \cdot D^2 \cdot Hvo$)				
Not Insulated; Eq. 1-28: $TLA = 0.4 \cdot TAA + 0.6 \cdot TB + 0.005 \sigma I$	TLA	516.36	R	Effective Tank diameter	De	5.29	ft	
Partially Insulated; Eq. 1-29: $TLA = 0.3 \cdot TAA + 0.7 \cdot TB + 0.005 \sigma R I$	TLA	516.43	R	Effective Tank Height	He	4.32	ft	
Fully Insulated; $TLA = TB$	TLA	515.5	R	Vapor Space Outage $Hvo = 1/2 H$	Hvo	2.16	ft	
Average Vapor Temperature (Tv)				Average Vapor Temperature (Tv)				
Not Insulated; Eq. 1-33: $Tv = 0.7 \cdot TAA + 0.3 \cdot TB + 0.009 \sigma I$	Tv	517.10	R					
Partially Insulated; Eq. 1-34: $Tv = 0.6 \cdot TAA + 0.4 \cdot TB + 0.01 \sigma R I$	Tv	517.40	R					
Fully Insulated; $Tv = TB$	Tv	515.46	R					
Stock Vapor Density; Eq. 1-22: $Wv = (Mv \cdot PVA) / (R \cdot Tv)$								
Not Insulated	Wv	1.361E-04						
Partially Insulated	Wv	1.363E-04						
Fully Insulated	Wv	1.324E-04						

Monthly Calculations (continued)

NOVEMBER

Tank No.	10460	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units
Total Losses (Eq. 1-1: $LT = LS + LW$)		LT	0.01	lb/month	Vapor Space Volume	Vv	47.5	ft ³	
Nearest US Location		Bridgeport, CT			Stock Vapor Density	Vv	0.0001	lb/ft ³	
Daily total solar insolation on a horizontal surface; Table 7.1-7		I	621.0	Btu/ft ² -day	Vapor Space Expansion Factor ($0 < KE \leq 1$); Eq. 1-5	KE	0.021	per day	
Absolute Pressure		P _A	14.69	psia	Vented Vapor Saturation Factor	Ks	1.00	NA	
Ideal Gas Constant		R	10.73	psia ft ³ /lb-mole R	Constant: Number of Daily Events in a Year	365	31	days/month	
Product Information					Working Losses; Eq. 1-35, $Lw = VO \cdot KN \cdot Kp \cdot Wv \cdot Kb$	Lw	0.01	lb/month	
Product Type		Distillate Fuel Oil No. 2			Net Working Loss Throughput (Eq. 1-39: $VQ = 5.614 \cdot Q$)	VQ	55	ft ³ /month	
Vapor Molecular weight		Mv	130	lb/lb-mole	Working Loss Turnover Factor Eq. 1-35 $Kw = (180 + N)/6N$ for N-36, else $Kw = 1$	KN	1.0000		
Average organic liquid density		WL	7.10	lb/gal	Working Loss Product Factor	Kp	1.00		
Average Reid Vapor Pressure		RVP	0.02	psia	Stock Vapor Density	Vv	0.0001	lb/ft ³	
Product factor: 0.4 for crude oils or 1 for other organic liquids		Kc	1.00		Vent Setting Correction Factor	KB	1.00		
Vapor Pressure Equation Constant A		A	12.10		Vented Vapor Saturation Factor; Eq. 1-21, $Ks = 1/(1+0.053 \cdot PVA \cdot Hvo)$	Ks	1.00		
Vapor Pressure Equation Constant B (Table 7.1-2)		B	8907.0	°R	Vapor Pressure at Avg Daily Liq Surface Temp	PvA	0.0041	psia	
Tank design data					Vapor Space Outage	Hvo	0.00	ft	
Shell height		Hs	4.32	ft	Vapor Space Expansion Factor (Eq. 1-5: $(\Delta Tv/TLA) + (\Delta Pv - \Delta Pb)/(PA - PvA)$)	KE	0.0208	per day	
Diameter		D	5.29	ft	Average Daily Vapor Temperature Range	ΔTv	12.56	°R	
Throughput		Q	410	gal/month	Average Daily Vapor Pressure Range	ΔPv	0.0020	psia	
Turnovers		N	7.02	per year	Breather Vent Pressure Setting Range (Equation 1-10: $\Delta Pb = PBP - PBV$)	ΔPb	0.0600	psia	
Roof Type:			0.00		Vapor Pressure at Avg Daily Liq Surface Temp	PvA	0.0041	psia	
Tank Cone Roof Slope (If unknown, use 0.0625)		SR	0.0625	ft/ft	Average Daily Liquid Surface Temperature	TLA	506.41	°R	
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))		RR	NA	ft	Atmospheric Pressure	PA	14.69	psia	
Maximum Filling Height - use (Pi/4)D if unknown		HLX	3.32	ft					
Minimum Filling Height (use 0 if unknown)		HLN	1.00	ft	Average Daily Vapor Temperature Range (ΔTv)				
Liquid height (assume 1/2 H)		HL	2.16	ft	Average daily ambient temperature range - Equation 1-11 ($\Delta TA = TAX - TA$)	ΔTA	13.5	°R	
Tank insulation (pick from drop down list)			Not Insulated		Not Insulated - Equation 1-7 ($\Delta TV = 0.7 \Delta TA + 0.02 \text{ or } I$)	ΔTv	12.56	°R	
Tank Construction (pick from drop down list)			Welded		Partially Insulated - Equation 1-8 ($\Delta TV = 0.6 \Delta TA + 0.02 \text{ or } I$)	ΔTv	11.21	°R	
Tank Shell Color (pick from drop down list)			White		Fully Insulated, constant temperature	ΔTv	0.00	°R	
Tank Shell Condition (pick from drop down list)			Average						
Tank Interior Condition (pick from drop down list)			Light Rust		Average Daily Vapor Pressure Range (ΔPv)				
Tank paint solar absorbance, dimensionless; Table 7.1-6		α	0.25		Not Insulated - Equation 1-9: $\Delta Pv = PVX - PVN$	ΔPv	0.00090	psia	
Breather Vent Setting Range (Default Assumption: +/- 0.03)		PBP	0.03	psia	Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25: $PvX = ex \cdot PVA$)	PvX	0.00461	psia	
True Vapor Pressure; Eq. 1-25, $PvA = \exp(A - (B/TLA))$					Vapor pressure at ave. daily min liquid surface temp. (Eq. 1-25: $PvN = ex \cdot PVA$)	PvN	0.00371	psia	
Not Insulated		PvA	0.0041375		Average daily max. liquid surface temp.; Fig. 7.1-17 $TLX = TLA + 0.25 \Delta T$	TLX	509.54	°R	
Partially Insulated		PvA	0.0041442		Average daily min. liquid surface temp.; Fig. 7.1-17 $TLN = TLA - 0.25 \Delta T$	TLN	503.27	°R	
Fully Insulated		PvA	0.0040535						
Average Daily Ambient Temperature (TAA) Eq. 1-30 $TAA = ((TAX + TA) / 2)$		TAA	505.35	°R	Partially Insulated - Equation 1-9: $\Delta Pv = PVX - PVN$	ΔPv	0.00081	psia	
Average daily maximum ambient temperature; Table 7.1-7		TAX	512.10	°R	Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25: PvX)	PvX	0.00457	psia	
Average daily minimum ambient temperature; Table 7.1-7		TAN	498.60	°R	Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25: PvN)	PvN	0.003750	psia	
Liquid Bulk Temperature; Eq. 1-31: $TB = TAA + 0.003 \text{ or } I$		TB	505.82	°R	Fully Insulated (ΔPv = 0)	ΔPv	0.00	psia	
Average Daily Liquid Surface Temperature (TLA)									
Not Insulated; Eq. 1-28, $TLA = 0.4 \cdot TAA + 0.6 \cdot TB + 0.005 \cdot \alpha \cdot I$		TLA	506.41	°R	Vapor Space Volume (Eq. 1-3: $Vv = (PI / 4) D^2 Hvo$)	Vv	47.52	ft ³	
Partially Insulated; Eq. 1-29, $TLA = 0.3 \cdot TAA + 0.7 \cdot TB + 0.005 \cdot \alpha \cdot I$		TLA	506.45	°R	Effective Tank diameter	De	5.29	ft	
Fully Insulated; $TLA = TB$		TLA	505.8	°R	Effective Tank Height	He	4.32	ft	
Average Vapor Temperature (Tv)					Vapor Space Outage $Hvo = 1/2 H$	Hvo	2.16	ft	
Not Insulated; Eq. 1-33, $Tv = 0.7 \cdot TAA + 0.3 \cdot TB + 0.009 \cdot \alpha \cdot I$		Tv	506.89	°R					
Partially Insulated; Eq. 1-34, $Tv = 0.6 \cdot TAA + 0.4 \cdot TB + 0.01 \cdot \alpha \cdot I$		Tv	507.09	°R					
Fully Insulated; $Tv = TB$		Tv	505.82	°R					
Stock Vapor Density; Eq. 1-22, $Wv = (Mv \cdot PVA) / (R \cdot Tv)$									
Not Insulated		Wv	9.88E-05						
Partially Insulated		Wv	9.90E-05						
Fully Insulated		Wv	9.70E-05						

HAPS Speciation	ib/month	Vapor Weight Concentration		Vapor Mole Fraction	
Product	Diesel	Eq. 40-6 $Zvi = yiMi / MV$	Eq. 40-5 $yi = Pi / PVA$		
Total HAP Emissions =	0.001				
Eq. 40-2 $L_i = Zvi(L_i)$					
Individual HAPS		L_i (lb/month)	M	M_v	Z_{vi}
hexane	0.0000	86.18	130	0.000047	0.000003
benzene	0.0000	78.11	130	0.00289	0.000014
2,2,4 TMP	0.0000	114.23	130	0.00000	0.000000
toluene	0.0002	92.14	130	0.02458	0.000100
ethylbenzene	0.0000	106.17	130	0.00284	0.000010
xylene	0.0003	106.17	130	0.05486	0.000195
naphthalene	0.0000	128.17	130	2.93E-04	8.62E-07
cumene	0.0000	120.19	130	0.00E+00	0.00E+00

Individual HAPS	Z_{vi}	M	M_v	X	A	B	C	P_{VA}
hexane	0.00000	188	86.18	0.00000	6.878	1171.5	224.37	1.3394
benzene	0.00001	188	78.11	0.00002	6.906	1211	220.79	0.8010
2,2,4 TMP	0.00000	188	114.23	0.00000	6.812	1257.8	220.74	0.4018
toluene	0.00032	188	92.14	0.00065	7.017	1377.6	222.64	0.2164
ethylbenzene	0.00013	188	106.17	0.00023	6.95	1419.3	212.61	0.0643
xylene	0.00299	188	106.17	0.00514	7.009	1462.3	215.11	0.0558
naphthalene	0.00078	188	128.17	0.00111	7.146	1831.6	211.82	0.0013
cumene	0.00000	188	120.19	0.00000	6.929	1455.8	207.2	0.0286

Monthly Calculations (continued)

DECEMBER

Tank No.	10460	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units	ROUTINE EMISSIONS CALCULATIONS		Symbol	Units
Total Losses (Eq. 1-1: $LT = LS + LW$)		LT	0.01	lb/month	Vapor Space Volume	Vv	47.5	ft ³	
Nearest US Location		Bridgeport, CT			Stock Vapor Density	Vv	0.0001	lb/ft ³	
Daily total solar insolation on a horizontal surface; Table 7.1-7		I	501.0	Btu/ft ² -day	Vapor Space Expansion Factor ($0 < KE \leq 1$); Eq. 1-5	KE	0.019	per day	
Absolute Pressure		P _A	14.69	psia	Vented Vapor Saturation Factor	Ks	1.00	NA	
Ideal Gas Constant		R	10.73	psia ft ³ /lb-mole R	Constant: Number of Daily Events in a Year	365	31	days/month	
Product Information					Working Losses; Eq. 1-35, $Lw = VO \cdot KN \cdot Kp \cdot Wv \cdot Kb$	Lw	0.00	lb/month	
Product Type		Distillate Fuel Oil No. 2			Net Working Loss Throughput (Eq. 1-39: $VQ = 5.614 \cdot Q$)	VQ	55	ft ³ /month	
Vapor Molecular weight		Mv	130	lb/lb-mole	Working Loss Turnover Factor Eq. 1-35 $Kw = (180 + N)/6N$ for N-36, else $Kw = 1$	KN	1.0000		
Average organic liquid density		WL	7.10	lb/gal	Working Loss Product Factor	Kp	1.00		
Average Reid Vapor Pressure		RVP	0.02	psia	Stock Vapor Density	Vv	0.0001	lb/ft ³	
Product factor: 0.4 for crude oils or 1 for other organic liquids		Kc	1.00		Vent Setting Correction Factor	KB	1.00		
Vapor Pressure Equation Constant A		A	12.10		Vented Vapor Saturation Factor; Eq. 1-21, $Ks = 1/(1+0.053 \cdot PVA \cdot Hvo)$	Ks	1.00		
Vapor Pressure Equation Constant B (Table 7.1-2)		B	8907.0	°R	Vapor Pressure at Avg Daily Liq Surface Temp	PvA	0.0029	psia	
Tank design data					Vapor Space Outage	Hvo	0.00	ft	
Shell height		Hs	4.32	ft	Vapor Space Expansion Factor (Eq. 1-5: $(\Delta Tv/TLA) + (\Delta Pv - \Delta Pb)/(PA - PvA)$)	KE	0.0188	per day	
Diameter		D	5.29	ft	Average Daily Vapor Temperature Range	ΔTv	11.33	°R	
Throughput		Q	410	gal/month	Average Daily Vapor Pressure Range	ΔPv	0.0006	psia	
Turnovers		N	6.79	per year	Breather Vent Pressure Setting Range (Equation 1-10: $\Delta Pb = PBP - PBV$)	ΔPb	0.0600	psia	
Roof Type:			0.00		Vapor Pressure at Avg Daily Liq Surface Temp	PvA	0.0029	psia	
Tank Cone Roof Slope (If unknown, use 0.0625)		SR	0.0625	ft/ft	Average Daily Liquid Surface Temperature	TLA	496.35	°R	
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))		RR	NA	ft	Atmospheric Pressure	PA	14.69	psia	
Maximum Filling Height - use (Pi/4)D if unknown		HLX	3.32	ft					
Minimum Filling Height (use 0 if unknown)		HLN	1.00	ft	Average Daily Vapor Temperature Range (ΔTv)				
Liquid height (assume 1/2 H)		HL	2.16	ft	Average daily ambient temperature range - Equation 1-11 ($\Delta TA = TAX - TA$)	ΔTA	12.6	°R	
Tank insulation (pick from drop down list)			Not Insulated		Not Insulated - Equation 1-7 ($\Delta TV = 0.7 \Delta TA + 0.02 \text{ or } I$)	ΔTv	11.33	°R	
Tank Construction (pick from drop down list)			Welded		Partially Insulated - Equation 1-8 ($\Delta TV = 0.6 \Delta TA + 0.02 \text{ or } I$)	ΔTv	10.07	°R	
Tank Shell Color (pick from drop down list)			White		Fully Insulated, constant temperature	ΔTv	0.00	°R	
Tank Shell Condition (pick from drop down list)			Average						
Tank Interior Condition (pick from drop down list)			Light Rust		Average Daily Vapor Pressure Range (ΔPv)				
Tank paint solar absorbance, dimensionless; Table 7.1-6		α	0.25		Not Insulated - Equation 1-9: $\Delta Pv = PVX - PVN$	ΔPv	0.00059	psia	
Breather Vent Setting Range (Default Assumption: +/- 0.03)		PBP	0.03	psia	Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25: $PvX = ex \cdot PVA$)	PvX	0.00321	psia	
True Vapor Pressure; Eq. 1-25, $PvA = \exp(A - (B/TLA))$					Vapor pressure at ave. daily min liquid surface temp. (Eq. 1-25: $PvN = ex \cdot PVA$)	PvN	0.00261	psia	
Not Insulated		PvA	0.0028974		Average daily max. liquid surface temp.; Fig. 7.1-17 $TLX = TLA + 0.25 \Delta T$	TLX	499.18	°R	
Partially Insulated		PvA	0.0029014		Average daily min. liquid surface temp.; Fig. 7.1-17 $TLN = TLA - 0.25 \Delta T$	TLN	493.52	°R	
Fully Insulated		PvA	0.0028479						
Average Daily Ambient Temperature (TAA) Eq. 1-30 $TAA = ((TAX + TA) / 2)$		TAA	495.50	°R	Partially Insulated - Equation 1-9: $\Delta Pv = PVX - PVN$	ΔPv	0.00053	psia	
Average daily maximum ambient temperature; Table 7.1-7		TAX	501.80	°R	Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25: PvX)	PvX	0.00318	psia	
Average daily minimum ambient temperature; Table 7.1-7		TAN	489.20	°R	Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25: PvN)	PvN	0.002479	psia	
Liquid Bulk Temperature; Eq. 1-31: $TB = TAA + 0.003 \text{ or } I$		TB	495.88	°R	Fully Insulated (ΔPv = 0)	ΔPv	0.00	psia	
Average Daily Liquid Surface Temperature (TLA)									
Not Insulated; Eq. 1-28, $TLA = 0.4 \cdot TAA + 0.6 \cdot TB + 0.005 \cdot \alpha \cdot I$		TLA	496.35	°R	Vapor Space Volume (Eq. 1-3: $Vv = (PI / 4) D^2 Hvo$)	Vv	47.52	ft ³	
Partially Insulated; Eq. 1-29, $TLA = 0.3 \cdot TAA + 0.7 \cdot TB + 0.005 \cdot \alpha \cdot I$		TLA	496.39	°R	Effective Tank diameter	De	5.29	ft	
Fully Insulated; $TLA = TB$		TLA	495.9	°R	Effective Tank Height	He	4.32	ft	
Average Vapor Temperature (Tv)					Vapor Space Outage $Hvo = 1/2 H$	Hvo	2.16	ft	
Not Insulated; Eq. 1-33, $Tv = 0.7 \cdot TAA + 0.3 \cdot TB + 0.009 \cdot \alpha \cdot I$		Tv	496.74	°R					
Partially Insulated; Eq. 1-34									

Monthly Calculations (continued)

MARCH

Tank No.	ROUTINE EMISSIONS CALCULATIONS			ROUTINE EMISSIONS CALCULATIONS			Symbol	Units	HAPS Speciation	lb/month	Product	Vapor Weight Concentration			Vapor Mole Fraction		
	Symbol	Units	Value	Symbol	Units	Value						Eq. 40-2	Eq. 40-5	Eq. 40-5	Eq. 40-5	Eq. 40-5	Eq. 40-5
	LT	1.37	lb/month	Standing Losses; Eq. 1-2, $L_s = 365 (Vv \cdot Wv \cdot Ke \cdot Ks)$	Ls	1.13	lb/month	Total HAP Emissions = 1.366	1.366	1.366	1.366	1.366	1.366	1.366	1.366	1.366	1.366
				Vapor Space Volume	Vv	441.8	ft ³										
				Stock Vapor Density	Wv	0.0014	lb/ft ³										
				Vapor Space Expansion Factor (0 < Ke <= 1); Eq. 1-5	Ke	0.060	per day										
				Vented Vapor Saturation Factor	Ks	1.00	NA										
				Constant; Number of Daily Events in a Year	365	31	days/month										
				Working Losses; Eq. 1-35, $L_w = VQ \cdot KN \cdot Kp \cdot Wv \cdot Kb$	Lw	0.23	lb/month	2,2,4 TMP	0.0000	114.23	130	0.00000	0.000000	0.058	-	-	-
				Net Working Loss Throughput (Eq. 1-39; $VO = 5.614 \cdot Q$)	VO	167	ft ³ /month										
				Working Loss Turnover Factor Eq. 1-35 $K_e = (180 + N) / 6N$ for N>36, else $K_e = 1.0000$	KN	1.0000											
				Working Loss Product Factor	Kp	1.00											
				Stock Vapor Density	Wv	0.0014	lb/ft ³										
				Vent Setting Correction Factor	KB	1.00											
				Vented Vapor Saturation Factor; Eq. 1-21, $K_s = 1 / (1 + 0.053 \cdot PVA \cdot Hvo)$	Ks	1.00		Liquid Mole Fraction	Eq. 40-4 $X_i = (Z_i \cdot M_i) / \sum M_i$	Z_i	M_i	X_i	A	B	C	P_{VA}	
				Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.0583	psia										
				Vapor Space Outage	Hvo	0.00	ft										
				Vapor Space Expansion Factor (Eq. 1-5); $(\Delta Tv / TLA) \cdot ((\Delta Pv - \Delta PB) / (PA - PVA))$	KE	0.0598	per day	Individual HAPS	Eq. 40-2 $L_{ij} = Z_{ij} \cdot (L_i) / \sum L_i$	L_{ij} (lb/month)	M_i	M_v	Z_{ij}	P_i = P_{VA}(X_i)	P_{VA}	y_i	
				Average Daily Vapor Temperature Range	ΔTv	32.37	°R										
				Average Daily Vapor Pressure Range	ΔPv	0.0000	psia										
				Breather Vent Pressure Setting Range (Equation 1-10; $APB = PBP - PVB$)	PBP	0.0600	psi										
				Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.0583	psia										
				Average Daily Liquid Surface Temperature	TLA	506.52	°R										
				Atmospheric Pressure	PA	14.69	psia										
				Average Daily Vapor Temperature Range (ΔTv)	ΔTv	14.2	°R	hexane	0.00000	130	86.18	0.00000	6.878	1171.5	224.37	1.3438	
				Average daily ambient temperature range - Equation 1-11 ($\Delta TA = TAX - TA$)	ΔTA	14.2	°R										
				Not Insulated - Equation 1-7 ($\Delta Tv = 0.7 \cdot \Delta TA + 0.02 \cdot \alpha$)	ΔTv	32.37	°R										
				Partially Insulated - Equation 1-8 ($\Delta Tv = 0.6 \cdot \Delta TA + 0.02 \cdot \alpha \cdot R$)	ΔTv	30.95	°R										
				Fully Insulated, constant temperature	ΔTv	0.00	°R										
				Average Daily Vapor Pressure Range (ΔPv)	ΔPv	0.00000	psia	benzene	0.00000	130	78.11	0.00000	6.906	1211	220.79	0.8038	
				Not Insulated - Equation 1-9; $\Delta Pv = Pvx - Pvn$	ΔPv	0.00000	psia										
				Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25 $Pvx = \exp(PVA)$)	Pvx	1.00000	psia										
				Vapor pressure at ave. daily min liquid surface temp. (Eq. 1-25 $Pvn = \exp(PVA)$)	Pvn	1.00000	psia										
				Average daily max. liquid surface temp.; Fig. 7.1-17 $TLX = TLA + 0.25 \Delta T$	TLX	514.62	°R										
				Average daily min. liquid surface temp.; Fig. 7.1-17 $TLN = TLA - 0.25 \Delta T$	TLN	498.43	°R										
				Partially Insulated - Equation 1-9; $\Delta Pv = Pvx - Pvn$	ΔPv	0.00000	psia										
				Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25 Pvx)	Pvx	1.00000	psia										
				Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25 Pvn)	Pvn	1.000000	psia										
				Average daily maximum ambient temperature, Table 7.1-7	TAX	506.00	°R										
				Average daily maximum liquid surface temperature, deg R ($TLX = TLA + TLX$)	TLX	514.60	°R										
				Average daily minimum ambient temperature, Table 7.1-7	TAN	491.80	°R										
				Average daily minimum liquid surface temperature, deg R ($TLN = TLA - TLN$)	TLN	499.12	°R										
				Fully Insulated (ΔPv = 0)	ΔPv	0.00	psia	toluene	0.00000	130	92.14	0.00000	7.017	1377.6	222.64	0.2173	
				Liquid Bulk Temperature; Eq. 1-31; $TB = TAA + 0.003 \cdot \alpha$	TB	502.26	°R										
				Vapor Space Volume (Eq. 1-3); $Vv = ((PI / 4) \cdot D^2 \cdot Hvo)$	Vv	441.79	ft³	2,2,4 TMP	0.00000	130	114.23	0.00000	6.812	1257.8	220.74	0.4033	
				Effective Tank diameter	D _e	9.77	ft										
				Effective Tank Height	H _e	11.78	ft										
				Vapor Space Outage $Hvo = 1/2 H$	Hvo	5.89	ft										
				Average Vapor Temperature (Tv)	Tv	510.00	°R	ethylbenzene	0.26400	130	106.17	0.32326	6.95	1419.3	212.61	0.0646	
				Not Insulated; Eq. 1-33, $Tv = 0.7 \cdot TAA + 0.3 \cdot TB + 0.009 \cdot \alpha$	Tv	510.00	°R										
				Partially Insulated; Eq. 1-34, $Tv = 0.6 \cdot TAA + 0.4 \cdot TB + 0.01 \cdot \alpha \cdot R$	Tv	511.46	°R										
				Fully Insulated; $Tv = TB$	Tv	502.26	°R										
				Stock Vapor Density; Eq. 1-22, $Wv = (Mv \cdot PVA) / (R \cdot Tv)$	Wv	2.120E-03		xylenes	0.73600	130	106.17	0.90120	7.009	1462.3	215.11	0.0561	
				Not Insulated	Wv	2.120E-03											
				Partially Insulated	Wv	1.399E-03											
				Fully Insulated	Wv	1.197E-03											

Monthly Calculations (continued)

APRIL

Tank No.	ROUTINE EMISSIONS CALCULATIONS			ROUTINE EMISSIONS CALCULATIONS			Symbol	Units	HAPS Speciation	lb/month	Product	Vapor Weight Concentration			Vapor Mole Fraction		
	Symbol	Units	Value	Symbol	Units	Value						Eq. 40-2	Eq. 40-5	Eq. 40-5	Eq. 40-5	Eq. 40-5	Eq. 40-5
	LT	2.38	lb/month	Standing Losses; Eq. 1-2, $L_s = 365 (Vv \cdot Wv \cdot Ke \cdot Ks)$	Ls	2.03	lb/month	Total HAP Emissions = 2.384	2.384	2.384	2.384	2.384	2.384	2.384	2.384	2.384	
				Vapor Space Volume	Vv	441.8	ft ³										
				Stock Vapor Density	Wv	0.0021	lb/ft ³										
				Vapor Space Expansion Factor (0 < Ke <= 1); Eq. 1-5	Ke	0.072	per day										
				Vented Vapor Saturation Factor	Ks	1.00	NA										
				Constant; Number of Daily Events in a Year	365	30	days/month										
				Working Losses; Eq. 1-35, $L_w = VQ \cdot KN \cdot Kp \cdot Wv \cdot Kb$	Lw	0.35	lb/month	2,2,4 TMP	0.0000	114.23	130	0.00000	0.000000	0.092	-	-	
				Net Working Loss Throughput (Eq. 1-39; $VO = 5.614 \cdot Q$)	VO	167	ft ³ /month										
				Working Loss Turnover Factor Eq. 1-35 $K_e = (180 + N) / 6N$ for N>36, else $K_e = 1.0000$	KN	1.0000											
				Working Loss Product Factor	Kp	1.00											
				Stock Vapor Density	Wv	0.0021	lb/ft ³										
				Vent Setting Correction Factor	KB	1.00											
				Vented Vapor Saturation Factor; Eq. 1-21, $K_s = 1 / (1 + 0.053 \cdot PVA \cdot Hvo)$	Ks	1.00		Liquid Mole Fraction	Eq. 40-4 $X_i = (Z_i \cdot M_i) / \sum M_i$	Z_i	M_i	X_i	A	B	C	P_{VA}	
				Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.0916	psia										
				Vapor Space Outage	Hvo	0.00	ft										
				Vapor Space Expansion Factor (Eq. 1-5); $(\Delta Tv / TLA) \cdot ((\Delta Pv - \Delta PB) / (PA - PVA))$	KE	0.0722	per day	Individual HAPS	Eq. 40-2 $L_{ij} = Z_{ij} \cdot (L_i) / \sum L_i$	L_{ij} (lb/month)	M_i	M_v	Z_{ij}	P_i = P_{VA}(X_i)	P_{VA}	y_i	
				Average Daily Vapor Temperature Range	ΔTv	39.62	°R										
				Average Daily Vapor Pressure Range	ΔPv	0.0000	psia										
				Breather Vent Pressure Setting Range (Equation 1-10; $APB = PBP - PVB$)	PBP	0.0600	psi										
				Vapor Pressure at Avg Daily Liq Surface Temp	PVA	0.0916	psia										
				Average Daily Liquid Surface Temperature	TLA	518.98	°R										
				Atmospheric Pressure	PA	14.69	psia										
				Average Daily Vapor Temperature Range (ΔTv)	ΔTv	15.3	°R	hexane	0.00000	130	86.18	0.00000	6.878	1171.5	224.37	1.8784	
				Average daily ambient temperature range - Equation 1-11 ($\Delta TA = TAX - TA$)	ΔTA	15.3											

Monthly Calculations (continued)

SEPTEMBER

Tank No.	ROUTINE EMISSIONS CALCULATIONS			ROUTINE EMISSIONS CALCULATIONS			HAPS Speciation		Vapor Mole Fraction	
	Symbol	Units	Value	Symbol	Units	Value	Product	Eq. 40-2	Eq. 40-5	
10470	LT	lb/month	3.52	LS	lb/month	2.93	hexane	0.0000	0.0000	
		ton/month	1.76E-03	VV	ft ³ /month	441.8	benzene	0.0000	0.0000	
				WV	lb/ft ³	0.0035	toluene	0.0000	0.0000	
				KE	per day	0.063	ethylbenzene	0.0000	0.0000	
				KS	per day	1.00	xylene	0.0000	0.0000	
				365	days/month	30	naphthalene	0.0000	0.0000	
				WV	lb/ft ³	0.0035	cumene	0.0000	0.0000	
				KB	per day	1.00				
				KN	per day	1.0000				
				KP	per day	1.00				
				WV	lb/ft ³	0.0035				
				KB	per day	1.00				
				KN	per day	1.0000				
				KP	per day	1.00				
				WV	lb/ft ³	0.0035				
				KB	per day	1.00				
				KN	per day	1.0000				
				KP	per day	1.00				
				WV	lb/ft ³	0.0035				
				KB	per day	1.00				
				KN	per day	1.0000				
				KP	per day	1.00				
				WV	lb/ft ³	0.0035				
				KB	per day	1.00				
				KN	per day	1.0000				
				KP	per day	1.00				
				WV	lb/ft ³	0.0035				
				KB	per day	1.00				
				KN	per day	1.0000				
				KP	per day	1.00				
				WV	lb/ft ³	0.0035				
				KB	per day	1.00				
				KN	per day	1.0000				
				KP	per day	1.00				
				WV	lb/ft ³	0.0035				
				KB	per day	1.00				
				KN	per day	1.0000				
				KP	per day	1.00				
				WV	lb/ft ³	0.0035				
				KB	per day	1.00				
				KN	per day	1.0000				
				KP	per day	1.00				
				WV	lb/ft ³	0.0035				
				KB	per day	1.00				
				KN	per day	1.0000				
				KP	per day	1.00				
				WV	lb/ft ³	0.0035				
				KB	per day	1.00				
				KN	per day	1.0000				
				KP	per day	1.00				
				WV	lb/ft ³	0.0035				
				KB	per day	1.00				
				KN	per day	1.0000				
				KP	per day	1.00				
				WV	lb/ft ³	0.0035				
				KB	per day	1.00				
				KN	per day	1.0000				
				KP	per day	1.00				
				WV	lb/ft ³	0.0035				
				KB	per day	1.00				
				KN	per day	1.0000				
				KP	per day	1.00				
				WV	lb/ft ³	0.0035				
				KB	per day	1.00				
				KN	per day	1.0000				
				KP	per day	1.00				
				WV	lb/ft ³	0.0035				
				KB	per day	1.00				
				KN	per day	1.0000				
				KP	per day	1.00				
				WV	lb/ft ³	0.0035				
				KB	per day	1.00				
				KN	per day	1.0000				
				KP	per day	1.00				
				WV	lb/ft ³	0.0035				
				KB	per day	1.00				
				KN	per day	1.0000				
				KP	per day	1.00				
				WV	lb/ft ³	0.0035				
				KB	per day	1.00				
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				KP	per day	1.00				
				WV	lb/ft ³	0.0035				
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				WV	lb/ft ³	0.0035				
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				WV	lb/ft ³	0.0035				
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				KP	per day	1.00				
				WV	lb/ft ³	0.0035				
				KB	per day	1.00				
				KN	per day	1.0000				
				KP	per day	1.00				
				WV	lb/ft ³	0.0035				
				KB	per day	1.00				
				KN	per day	1.0000				
				KP	per day	1.00				
				WV	lb/ft ³	0.0035				
				KB	per day	1.00				
				KN	per day	1.0000				
				KP	per day	1.00				
				WV	lb/ft ³	0.0035				
				KB	per day	1.00				
				KN	per day	1.0000				
				KP	per day	1.00				
				WV	lb/ft ³	0.0035				
				KB	per day	1.00				
				KN	per day	1.0000				
				KP	per day	1.00				
				WV	lb/ft ³	0.0035				
				KB	per day	1.00				
				KN	per day	1.0000				
				KP	per day	1.00				
				WV	lb/ft ³	0.0035				
				KB	per day	1.00				
				KN	per day	1.0000				
				KP	per day	1.00				
				WV	lb/ft ³	0.0035				
				KB	per day	1.00				
				KN	per day	1.0000				
				KP	per day	1.00				
				WV	lb/ft ³	0.0035				
				KB	per day	1.00				
				KN	per day	1.0000				
				KP	per day	1.00				
				WV	lb/ft ³	0.0035				
				KB	per day	1.00				
				KN	per day	1.0000				
				KP	per day	1.00				
				WV	lb/ft ³	0.0035				
				KB	per day	1.00				
				KN	per day	1.0000				
				KP	per day	1.00				
				WV	lb/ft ³	0.0035				
				KB	per day	1.00				
				KN	per day	1.0000				
				KP	per day	1.00				
				WV	lb/ft ³	0.0035				
				KB	per day	1.00				
				KN	per day	1.0000				
				KP	per day	1.00				
				WV	lb/ft ³	0.0035				
				KB	per day	1.00				
				KN	per day	1.0000				
				KP	per day	1.00				
				WV	lb/ft ³					

Monthly Calculations (continued)

MARCH

Task No.	10480	Symbol	Units	ROUTINE EMISSIONS CALCULATIONS	Symbol	Units
ROUTINE EMISSIONS CALCULATIONS						
Total Losses (Eq. 1-1: $LT = LS + LW$)	LT	0.79	lb/month	Standing Losses; Eq. 1-2, $LS = 365 (Vv \cdot Wv \cdot KE \cdot Ka)$	LS	0.64 lb/month
		3.96E-04	ton/month	Vapor Space Volume	Vv	250.5 ft ³
				Stock Vapor Density	Wv	0.0014 lb/ft ³
				Vapor Space Expansion Factor ($0 < KE \leq 1$); Eq. 1-5	KE	0.060 per day
				Vented Vapor Saturation Factor	Ks	1.00 NA
				Constant; Number of Daily Events in a Year	365	30 days/month
Nearest US Location		Bridgport, CT		Working Losses; Eq. 1-35, $LW = VQ \cdot KN \cdot Kp \cdot Wv \cdot KB$	LW	0.15 lb/month
Daily total solar insolation on a horizontal surface; Table 7.1-7	I	1156.0	Btu/ft ² -day	Net Working Loss Throughput (Eq. 1-39: $VQ = 5.614 \cdot Q$)	VQ	107 ft ³ /month
Absolute Pressure	PA	14.89	psia	Working Loss Turnover Factor Eq. 1-35: $Kp = (180 + N)/6N$ for $N \geq 36$, else $Kp = 1$	KN	1.0000
Ideal Gas Constant	R	10.73	psia ft ³ /lb-mole R	Working Loss Product Factor	Kp	1.00
Product Information						
Product Type		Diesel Additive		Stock Vapor Density	Wv	0.0014 lb/ft ³
Vapor Molecular weight	Mv	130	Lb/lb-mole	Vent Setting Correction Factor	KB	1.00
Average organic liquid density	WL	6.10	lb/gal	Vented Vapor Saturation Factor; Eq. 1-21, $Ks = 1/(1+0.053 \cdot PvA \cdot Hvo)$	Ks	1.00
Average Reid Vapor Pressure	RVP	0.00	psi	Vapor Pressure at Avg Daily Liq Surface Temp	PvA	0.0583 psia
Product factor; 0.4 for crude oils or 1 for other organic liquids	Kc	1.00		Vapor Space Outage	Hvo	0.00 ft
Vapor Pressure Equation Constant A	A	0.00				
Vapor Pressure Equation Constant B (Table 7.1-2)	B	0.0	°R			
Tank design data						
Shell height	Hs	10.60	ft	Vapor Space Expansion Factor (Eq. 1-5: $(\Delta T v / TLA) \cdot [(APv - \Delta P B) / (PA - PvA)]$)	KE	0.0598 per day
Diameter	D	7.76	ft	Average Daily Vapor Temperature Range	ΔTv	32.37 °R
Throughput	Q	800	gal/month	Average Daily Vapor Pressure Range	ΔPv	0.00000 psia
Turnovers	N	2.51	per year	Breather Vent Pressure Setting Range (Equation 1-10: $\Delta P B = P B P - P B V$)	PBP	0.0600 psi
Roof Type:		0.00		Vapor Pressure at Avg Daily Liq Surface Temp	PvA	0.0583 psia
Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft	Average Daily Liquid Surface Temperature	TLA	506.52 °R
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA	ft	Atmospheric Pressure	PA	14.69 psia
Maximum Filling Height - use (Pi/4)D if unknown	HLX	9.60	ft			
Minimum Filling Height (use 0 if unknown)	HLN	1.00	ft	Average Daily Vapor Temperature Range (ΔTv)		
Liquid height (assume 1/2 H)	HL	5.30	ft	Average daily ambient temperature range - Equation 1-11 ($\Delta TA = TAX - TA$)	ΔTA	14.2 °R
Tank insulation (pick from drop down list)		Not Insulated		Not Insulated - Equation 1-7 ($\Delta TV = 0.7 \cdot \Delta TA + 0.02 \cdot \alpha$)	ΔTV	32.37 °R
Tank Construction (pick from drop down list)		Welded		Partially Insulated - Equation 1-8 ($\Delta TV = 0.6 \cdot \Delta TA + 0.02 \cdot \alpha$)	ΔTV	30.95 °R
Tank Shell Color (pick from drop down list)		Black		Fully Insulated, constant temperature	ΔTV	0.00 °R
Tank Shell Condition (pick from drop down list)		Average				
Tank Interior Condition (pick from drop down list)		Light Rust		Average Daily Vapor Pressure Range (ΔPv)		
Tank paint solar absorptance, dimensionless; Table 7.1-6	α	0.97		Not Insulated - Equation 1-9: $\Delta PV = PVX - PVN$	ΔPv	0.00000 psia
Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	0.03	psi	Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25: $PvX = \alpha \cdot PvA$)	PvX	1.00000 psia
		-0.03		Vapor pressure at ave daily min liquid surface temp. (Eq. 1-25: $PvN = \alpha \cdot PvA$)	PvN	1.00000 psia
True Vapor Pressure; Eq. 1-25, $PvA = \exp(A \cdot (B/TLA))$						
Not Insulated	PvA	0.0583131		Average daily max. liquid surface temp.; Fig. 7.1-17: $TLX = TLA + 0.25 \Delta TV$	TLX	514.62 °R
Partially Insulated	PvA	0.059051		Average daily min. liquid surface temp.; Fig. 7.1-17: $TLN = TLA - 0.25 \Delta TV$	TLN	498.43 °R
Fully Insulated	PvA	0.0496349				
Average Daily Ambient Temperature (TAA) Eq. 1-30: $TAA = ((TAX + TAN) / 2) + (TAX - TAN) \cdot (TAA - TAA) / (TAX - TAN)$						
Average daily maximum ambient temperature; Table 7.1-7	TAX	506.00	°R	Partially Insulated - Equation 1-9: $\Delta PV = PVX - PVN$	ΔPv	0.00000 psia
Average daily minimum ambient temperature; Table 7.1-7	TAN	491.80	°R	Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25: $PvX = \alpha \cdot PvA$)	PvX	1.00000 psia
				Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25: $PvN = \alpha \cdot PvA$)	PvN	1.00000 psia
				Average daily maximum liquid surface temperature, deg R ($TLX = TLA + TLX$)	TLX	514.60 °R
				Average daily minimum liquid surface temperature, deg R ($TLN = TLA - TLN$)	TLN	498.12 °R
Liquid Bulk Temperature; Eq. 1-31: $TB = TAA + 0.003 \cdot \alpha$						
	TB	502.26	°R	Fully Insulated ($\Delta Pv = 0$)	ΔPv	0.00 psia
Average Daily Liquid Surface Temperature (TLA)						
Not Insulated; Eq. 1-28, $TLA = 0.4 \cdot TAA + 0.6 \cdot TB + 0.005 \cdot \alpha$	TLA	506.52	°R	Vapor Space Volume (Eq. 1-3: $Vv = (PI/4) \cdot D^2 \cdot Hvo$)	Vv	250.49 ft ³
Partially Insulated; Eq. 1-29, $TLA = 0.3 \cdot TAA + 0.7 \cdot TB + 0.005 \cdot \alpha$	TLA	506.86	°R	Effective Tank diameter	De	7.76 ft
Fully Insulated; $TLA = TB$	TLA	502.3	°R	Effective Tank Height	He	10.60 ft
				Vapor Space Outage Hvo = 1/2 H	Hvo	5.30 ft
Average Vapor Temperature (Tv)						
Not Insulated; Eq. 1-33, $Tv = 0.7 \cdot TAA + 0.3 \cdot TB + 0.009 \cdot \alpha$	Tv	510.00	°R			
Partially Insulated; Eq. 1-34, $Tv = 0.6 \cdot TAA + 0.4 \cdot TB + 0.01 \cdot \alpha$	Tv	511.46	°R			
Fully Insulated; $Tv = TB$	Tv	502.26	°R			
Stock Vapor Density; Eq. 1-22, $Wv = (Mv \cdot PvA) / (R \cdot Tv)$						
Not Insulated	Wv	1.385E-03				
Partially Insulated	Wv	1.399E-03				
Fully Insulated	Wv	1.197E-03				

HAPS Speciation	Product	ib/month	Vapor Weight Concentration	Vapor Mole Fraction
			Eq. 40-6 $Zvi = yMi / MV$	Eq. 40-5 $yi = Pi / PvA$
Total HAP Emissions = 0.791				
Eq. 40-2 $L_i = Zvi(L_i)$				
Individual HAPS				
			M_i	Z_{vi}
hexane	0.0000	86.18	130	0.00000
benzene	0.0000	78.11	130	0.00000
2,2,4 TMP	0.0000	114.23	130	0.00000
toluene	0.0000	92.14	130	0.00000
ethylbenzene	0.2314	106.17	130	0.29246
xylenes	0.5599	106.17	130	0.70754
naphthalene	0.0000	128.17	130	0.00E+00
cumene	0.0000	120.19	130	0.00E+00

Individual HAPS	Z _{vi}	M _i	M	X _i	A	B	C	P _{vi}
hexane	0.00000	130	86.18	0.00000	6.878	1171.5	224.37	1.3438
benzene	0.00000	130	78.11	0.00000	6.906	1211	220.79	0.8038
2,2,4 TMP	0.00000	130	114.23	0.00000	6.812	1257.8	220.74	0.4033
toluene	0.00000	130	92.14	0.00000	7.017	1377.6	222.64	0.2173
ethylbenzene	0.26400	130	106.17	0.32326	6.95	1419.3	212.61	0.0646
xylenes	0.73600	130	106.17	0.90120	7.009	1462.3	215.11	0.0561
naphthalene	0.00000	130	128.17	0.00000	7.146	1831.6	211.82	0.0013
cumene	0.00000	130	120.19	0.00000	6.929	1455.8	207.2	0.0287

Monthly Calculations (continued)

APRIL

Task No.	10480	Symbol	Units	ROUTINE EMISSIONS CALCULATIONS	Symbol	Units
ROUTINE EMISSIONS CALCULATIONS						
Total Losses (Eq. 1-1: $LT = LS + LW$)	LT	1.38	lb/month	Standing Losses; Eq. 1-2, $LS = 365 (Vv \cdot Wv \cdot KE \cdot Ka)$	LS	1.15 lb/month
		6.89E-04	ton/month	Vapor Space Volume	Vv	250.5 ft ³
				Stock Vapor Density	Wv	0.0021 lb/ft ³
				Vapor Space Expansion Factor ($0 < KE \leq 1$); Eq. 1-5	KE	0.072 per day
				Vented Vapor Saturation Factor	Ks	1.00 NA
				Constant; Number of Daily Events in a Year	365	30 days/month
Nearest US Location		Bridgport, CT		Working Losses; Eq. 1-35, $LW = VQ \cdot KN \cdot Kp \cdot Wv \cdot KB$	LW	0.23 lb/month
Daily total solar insolation on a horizontal surface; Table 7.1-7	I	1490.0	Btu/ft ² -day	Net Working Loss Throughput (Eq. 1-39: $VQ = 5.614 \cdot Q$)	VQ	107 ft ³ /month
Absolute Pressure	PA	14.89	psia	Working Loss Turnover Factor Eq. 1-35: $Kp = (180 + N)/6N$ for $N \geq 36$, else $Kp = 1$	KN	1.0000
Ideal Gas Constant	R	10.73	psia ft ³ /lb-mole R	Working Loss Product Factor	Kp	1.00
Product Information						
Product Type		Diesel Additive		Stock Vapor Density	Wv	0.0021 lb/ft ³
Vapor Molecular weight	Mv	130	Lb/lb-mole	Vent Setting Correction Factor	KB	1.00
Average organic liquid density	WL	6.10	lb/gal	Vented Vapor Saturation Factor; Eq. 1-21, $Ks = 1/(1+0.053 \cdot PvA \cdot Hvo)$	Ks	1.00
Average Reid Vapor Pressure	RVP	0.00	psi	Vapor Pressure at Avg Daily Liq Surface Temp	PvA	0.0916 psia
Product factor; 0.4 for crude oils or 1 for other organic liquids	Kc	1.00		Vapor Space Outage	Hvo	0.00 ft
Vapor Pressure Equation Constant A	A	0.00				
Vapor Pressure Equation Constant B (Table 7.1-2)	B	0.0	°R			
Tank design data						
Shell height	Hs	10.60	ft	Vapor Space Expansion Factor (Eq. 1-5: $(\Delta T v / TLA) \cdot [(APv - \Delta P B) / (PA - PvA)]$)	KE	0.0722 per day
Diameter	D	7.76	ft	Average Daily Vapor Temperature Range	ΔTv	39.62 °R
Throughput	Q	800	gal/month	Average Daily Vapor Pressure Range	ΔPv	0.00000 psia
Turnovers	N	2.60	per year	Breather Vent Pressure Setting Range (Equation 1-10: $\Delta P B = P B P - P B V$)	PBP	0.0600 psi
Roof Type:		0.00		Vapor Pressure at Avg Daily Liq Surface Temp	PvA	0.0916 psia
Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft	Average Daily Liquid Surface Temperature	TLA	518.98 °R
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA	ft	Atmospheric Pressure	PA	14.69 psia
Maximum Filling Height - use (Pi/4)D if unknown	HLX	9.60	ft			
Minimum Filling Height (use 0 if unknown)	HLN	1.00	ft	Average Daily Vapor Temperature Range (ΔTv)		
Liquid height (assume 1/2 H)	HL	5.30	ft	Average daily ambient temperature range - Equation 1-11 ($\Delta TA = TAX - TA$)	ΔTA	15.3 °R
Tank insulation (pick from drop down list)		Not Insulated		Not Insulated - Equation 1-7 ($\Delta TV = 0.7 \cdot \Delta TA + 0.02 \cdot \alpha$)	ΔTV	39.62 °R
Tank Construction (pick from drop down list)		Welded		Partially Insulated - Equation 1-8 ($\Delta TV = 0.6 \cdot \Delta TA + 0.02 \cdot \alpha$)	ΔTV	38.09 °R
Tank Shell Color (pick from drop down list)		Black		Fully Insulated, constant temperature	ΔTV	0.00 °R
Tank Shell Condition (pick from drop down list)		Average				
Tank Interior Condition (pick from drop down list)		Light Rust		Average Daily Vapor Pressure Range (ΔPv)		
Tank paint solar absorptance, dimensionless; Table 7.1-6	α	0.97		Not Insulated - Equation 1-9: $\Delta PV = PVX - PVN$	ΔPv	0.00000 psia
Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	0.03	psi	Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25: $PvX = \alpha \cdot PvA$)	PvX	1.00000 psia
		-0.03		Vapor pressure at ave daily min liquid surface temp. (Eq. 1-25: $PvN = \alpha \cdot PvA$)	PvN	1.00000 psia
True Vapor Pressure; Eq. 1-25, $PvA = \exp(A \cdot (B/TLA))$						
Not Insulated	PvA	0.0916245		Average daily max. liquid surface temp.; Fig. 7.1-17: $TLX = TLA + 0.25 \Delta TV$	TLX	528.88 °R
Partially Insulated	PvA	0.0930318		Average daily min. liquid surface temp.; Fig. 7.1-17: $TLN = TLA - 0.25 \Delta TV$	TLN	509.07 °R
Fully Insulated	PvA	0.0753251				
Average Daily Ambient Temperature (TAA) Eq. 1-30: $TAA = ((TAX + TAN) / 2) + (TAX - TAN) \cdot (TAA - TAA) / (TAX - TAN)$						
Average daily maximum ambient temperature; Table 7.1-7	TAX	516.80	°R	Partially Insulated - Equation 1-9: $\Delta PV = PVX - PVN$	ΔPv	0.00000 psia
Average daily minimum ambient temperature; Table 7.1-7	TAN	501.50	°R	Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25: $PvX = \alpha \cdot PvA$)	PvX	1.00000 psia
				Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25: $PvN = \alpha \cdot PvA$)	PvN	1.00000 psia
				Average daily maximum liquid surface temperature, deg R ($TLX = TLA + TLX$)	TLX	528.93 °R
				Average daily minimum liquid surface temperature, deg R ($TLN = TLA - TLN$)	TLN	509.89 °R
Liquid Bulk Temperature; Eq. 1-31: $TB = TAA + 0.003 \cdot \alpha$						
	TB	513.49	°R	Fully Insulated ($\Delta Pv = 0$)	ΔPv	0.00 psia
Average Daily Liquid Surface Temperature (TLA)						
Not Insulated; Eq. 1-28, $TLA = 0.4 \cdot TAA + 0.6 \cdot TB + 0.005 \cdot \alpha$	TLA	518.98	°R	Vapor Space Volume (Eq. 1-3: $Vv = (PI/4) \cdot D^2 \cdot Hvo$)	Vv	250.49 ft ³
Partially Insulated; Eq. 1-29, $TLA = 0.3 \cdot TAA + 0.7 \cdot TB + 0.005 \cdot \alpha$	TLA	519.41	°R	Effective Tank diameter	De	7.76 ft
Fully Insulated; $TLA = TB$	TLA	513.5	°R	Effective Tank Height	He	10.60 ft
				Vapor Space Outage Hvo = 1/2 H	Hvo	5.30 ft
Average Vapor Temperature (Tv)						
Not Insulated; Eq. 1-33, $Tv = 0.7 \cdot TAA + 0.3 \cdot TB + 0.009 \cdot \alpha$	Tv	523.46	°R			
Partially Insulated; Eq. 1-34, $Tv = 0.6 \cdot TAA + 0.4 \cdot TB + 0.01 \cdot \alpha$	Tv	525.34	°R			
Fully Insulated; $Tv = TB$	Tv	513.49	°R			
Stock Vapor Density; Eq. 1-22, $Wv = (Mv \cdot PvA) / (R \cdot Tv)$						
Not Insulated	Wv	2.120E-03				
Partially Insulated	Wv	2.145E-03				
Fully Insulated	Wv	1.777E-03				

HAPS Speciation	Product	ib/month	Vapor Weight Concentration	Vapor Mole Fraction
			Eq. 40-6 $Zvi = yMi / MV$	Eq. 40-5 $yi = Pi / PvA$

Monthly Calculations (continued)

SEPTEMBER

Tank No.	10480	Symbol	Units	ROUTINE EMISSIONS CALCULATIONS	Symbol	Units
ROUTINE EMISSIONS CALCULATIONS						
Total Losses (Eq. 1-1: $LT = LS + LW$)	LT	2.04	lb/month	Standing Losses; Eq. 1-2, $LS = 365 (Vv \cdot Wv \cdot KE \cdot Ka)$	LS	1.66 lb/month
		1.02E-03	ton/month	Vapor Space Volume	Vv	250.5 ft ³
				Stock Vapor Density	Wv	0.0035 lb/ft ³
				Vapor Space Expansion Factor ($0 < KE \leq 1$); Eq. 1-5	KE	0.063 per day
Nearest US Location				Vented Vapor Saturation Factor	Ks	1.00 NA
Daily total solar insolation on a horizontal surface; Table 7.1-7	I	1320.0	Btu/ft ² -day	Constant; Number of Daily Events in a Year	365	30 days/month
Absolute Pressure	PA	14.69	psia	Working Losses; Eq. 1-35, $Lw = VQ \cdot KN \cdot Kp \cdot Wv \cdot KB$	Lw	0.38 lb/month
Ideal Gas Constant	R	10.73	psia ft ³ /lb-mole R	Net Working Loss Throughput (Eq. 1-39: $VQ=5.614 \cdot Q$)	VQ	107 ft ³ /month
Product Information				Working Loss Turnover Factor Eq. 1-35: $Kp=(180+N)/6N$ for N=36, else $Kp=KN$	KN	1.0000
Product Type				Working Loss Product Factor	Kp	1.00
Vapor Molecular weight	Mv	130	Lb/lb-mole	Stock Vapor Density	Wv	0.0035 lb/ft ³
Average organic liquid density	WL	6.10	lb/gal	Vent Setting Correction Factor	KB	1.00
Average Reid Vapor Pressure	RVP	0.00	psi	Vented Vapor Saturation Factor; Eq. 1-21, $Ks = 1/(1+0.053 \cdot PvA \cdot Hvo)$	Ks	1.00
Product factor; 0.4 for crude oils or 1 for other organic liquids	Kc	1.00		Vapor Pressure at Avg Daily Liq Surface Temp	PvA	0.1569 psia
Vapor Pressure Equation Constant A	A	0.00		Vapor Space Outage	Hvo	0.00 ft
Vapor Pressure Equation Constant B (Table 7.1-2)	B	0.0	°R	Vapor Space Expansion Factor (Eq. 1-5: $(\Delta T v / TLA) \cdot [(APv - \Delta P B) / (PA - PvA)]$)	KE	0.0627 per day
Tank design data				Average Daily Vapor Temperature Range	ΔTv	35.76 °R
Shell height	Hs	10.60	ft	Average Daily Vapor Pressure Range	ΔPv	0.0000 psi
Diameter	D	7.76	ft	Breather Vent Pressure Setting Range (Equation 1-10: $\Delta P B = P B P - P B V$)	PBP	0.0600 psi
Throughput	Q	800	gal/month	Vapor Pressure at Avg Daily Liq Surface Temp	PvA	0.1569 psia
Turnovers	N	2.60	per year	Average Daily Liquid Surface Temperature	TLA	534.86 °R
Roof Type:				Atmospheric Pressure	PA	14.69 psia
Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft	Average Daily Vapor Temperature Range (ΔTv)		
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA	ft	Average daily ambient temperature range - Equation 1-11 ($\Delta TA = TAX - TAN$)	ΔTA	14.5 °R
Maximum Filling Height - use (Pi/4)D if unknown	HLX	9.60	ft	Not Insulated - Equation 1-7 ($\Delta TV = 0.7 \cdot \Delta TA + 0.02 \cdot \alpha$)	ΔTV	35.76 °R
Minimum Filling Height (use 0 if unknown)	HLN	1.00	ft	Partially Insulated - Equation 1-8 ($\Delta TV = 0.6 \cdot \Delta TA + 0.02 \cdot \alpha R$)	ΔTV	34.31 °R
Liquid height (assume 1/2 H)	HL	5.30	ft	Fully Insulated, constant temperature	ΔTV	0.00 °R
Tank insulation (pick from drop down list)				Average Daily Vapor Pressure Range (ΔPv)		
Tank Construction (pick from drop down list)				Not Insulated - Equation 1-9: $\Delta P V = P V X - P V N$	ΔPv	0.00000 psi
Tank Shell Color (pick from drop down list)				Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25: $P V X = \alpha P$)	PvX	1.00000 psi
Tank Shell Condition (pick from drop down list)				Vapor pressure at ave daily min liquid surface temp. (Eq. 1-25: $P V N = \alpha P$)	PvN	1.00000 psi
Tank Interior Condition (pick from drop down list)				Average daily max. liquid surface temp.; Fig. 7.1-17: $TLX = TLA + 0.25 \Delta TV$	TLX	543.80 °R
Tank paint solar absorptance, dimensionless; Table 7.1-6	α	0.97		Average daily min. liquid surface temp.; Fig. 7.1-17: $TLN = TLA - 0.25 \Delta TV$	TLN	525.92 °R
Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	0.03	psi	Partially Insulated - Equation 1-9: $\Delta P V = P V X - P V N$	ΔPv	0.00000 psi
True Vapor Pressure; Eq. 1-25, $PvA = \exp(A \cdot (B/TLA))$				Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25: PvX)	PvX	1.00000 psi
Not Insulated	PvA	0.1569349		Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25: PvN)	PvN	1.0000000 psi
Partially Insulated	PvA	0.1569129		Average daily maximum liquid surface temperature, deg R ($TLX = TLA + TLX$)	TLX	543.82 °R
Fully Insulated	PvA	0.1336491		Average daily minimum liquid surface temperature, deg R ($TLN = TLA - TLN$)	TLN	526.66 °R
Average Daily Ambient Temperature (TAA) Eq. 1-30 $TAA = ((TAX + TAN) / 2)$	TAA	526.15	°R	Fully Insulated (ΔPv = 0)	ΔPv	0.00 psi
Average daily maximum ambient temperature; Table 7.1-7	TAX	533.40	°R	Vapor Space Volume (Eq. 1-3: $Vv = (PI / 4) D^2 Hvo$)	Vv	250.49 ft ³
Average daily minimum ambient temperature; Table 7.1-7	TAN	518.90	°R	Effective Tank diameter	De	7.76 ft
Liquid Bulk Temperature; Eq. 1-31: $TB = TAA + 0.003 \alpha s$	TB	529.99	°R	Effective Tank Height	He	10.60 ft
				Vapor Space Outage Hvo = 1/2 H	Hvo	5.30 ft
Average Daily Liquid Surface Temperature (TLA)						
Not Insulated; Eq. 1-28, $TLA = 0.4 \cdot TAA + 0.6 \cdot TB + 0.005 \cdot \alpha \cdot I$	TLA	534.86	°R			
Partially Insulated; Eq. 1-29, $TLA = 0.3 \cdot TAA + 0.7 \cdot TB + 0.005 \cdot \alpha \cdot R$	TLA	535.24	°R			
Fully Insulated; $TLA = TB$	TLA	530.0	°R			
Average Vapor Temperature (Tv)						
Not Insulated; Eq. 1-33, $Tv = 0.7 \cdot TAA + 0.3 \cdot TB + 0.009 \cdot \alpha \cdot I$	Tv	538.83	°R			
Partially Insulated; Eq. 1-34, $Tv = 0.6 \cdot TAA + 0.4 \cdot TB + 0.01 \cdot \alpha \cdot R$	Tv	540.49	°R			
Fully Insulated; $Tv = TB$	Tv	529.99	°R			
Stock Vapor Density; Eq. 1-22, $Wv = (Mv \cdot PvA) / (R \cdot Tv)$						
Not Insulated	Wv	3.528E-03				
Partially Insulated	Wv	3.562E-03				
Fully Insulated	Wv	3.056E-03				

HAPS Speciation	lb/month	Product	Eq. 40-6 $Zvi = yMi / MV$	Vapor Weight Concentration	Vapor Mole Fraction
Total HAP Emissions =	2.040				
Individual HAPS					
hexane	0.0000	86.18	130	0.00000	0.00000
benzene	0.0000	78.11	130	0.00000	0.00000
2,2,4 TMP	0.0000	114.23	130	0.00000	0.00000
toluene	0.0000	92.14	130	0.00000	0.00000
ethylbenzene	0.5934	106.17	130	0.29081	0.055882
xylenes	1.4471	106.17	130	0.70919	0.136278
naphthalene	0.0000	128.17	130	0.00E+00	0.00E+00
cumene	0.0000	120.19	130	0.00E+00	0.00E+00

Individual HAPS	Zi	Mi	M	Xi	A	B	C	P _{vi}
hexane	0.00000	130	86.18	0.00000	6.878	1171.5	224.37	2.8022
benzene	0.00000	130	78.11	0.00000	6.906	1211	220.79	1.7585
2,2,4 TMP	0.00000	130	114.23	0.00000	6.812	1257.8	220.74	0.9097
toluene	0.00000	130	92.14	0.00000	7.017	1377.6	222.64	0.5221
ethylbenzene	0.26400	130	106.17	0.32326	6.95	1419.3	212.61	0.1729
xylenes	0.73600	130	106.17	0.90120	7.009	1462.3	215.11	0.1512
naphthalene	0.00000	130	128.17	0.00000	7.146	1831.6	211.82	0.0046
cumene	0.00000	130	120.19	0.00000	6.929	1455.8	207.2	0.0829

Monthly Calculations (continued)

OCTOBER

Tank No.	10480	Symbol	Units	ROUTINE EMISSIONS CALCULATIONS	Symbol	Units
ROUTINE EMISSIONS CALCULATIONS						
Total Losses (Eq. 1-1: $LT = LS + LW$)	LT	1.16	lb/month	Standing Losses; Eq. 1-2, $LS = 365 (Vv \cdot Wv \cdot KE \cdot Ka)$	LS	0.91 lb/month
		5.79E-04	ton/month	Vapor Space Volume	Vv	250.5 ft ³
				Stock Vapor Density	Wv	0.0023 lb/ft ³
				Vapor Space Expansion Factor ($0 < KE \leq 1$); Eq. 1-5	KE	0.052 per day
Nearest US Location				Vented Vapor Saturation Factor	Ks	1.00 NA
Daily total solar insolation on a horizontal surface; Table 7.1-7	I	948.0	Btu/ft ² -day	Constant; Number of Daily Events in a Year	365	31 days/month
Absolute Pressure	PA	14.69	psia	Working Losses; Eq. 1-35, $Lw = VQ \cdot KN \cdot Kp \cdot Wv \cdot KB$	Lw	0.24 lb/month
Ideal Gas Constant	R	10.73	psia ft ³ /lb-mole R	Net Working Loss Throughput (Eq. 1-39: $VQ=5.614 \cdot Q$)	VQ	107 ft ³ /month
Product Information				Working Loss Turnover Factor Eq. 1-35: $Kp=(180+N)/6N$ for N=36, else $Kp=KN$	KN	1.0000
Product Type				Working Loss Product Factor	Kp	1.00
Vapor Molecular weight	Mv	130	Lb/lb-mole	Stock Vapor Density	Wv	0.0023 lb/ft ³
Average organic liquid density	WL	6.10	lb/gal	Vent Setting Correction Factor	KB	1.00
Average Reid Vapor Pressure	RVP	0.00	psi	Vented Vapor Saturation Factor; Eq. 1-21, $Ks = 1/(1+0.053 \cdot PvA \cdot Hvo)$	Ks	1.00
Product factor; 0.4 for crude oils or 1 for other organic liquids	Kc	1.00		Vapor Pressure at Avg Daily Liq Surface Temp	PvA	0.0984 psia
Vapor Pressure Equation Constant A	A	0.00		Vapor Space Outage	Hvo	0.00 ft
Vapor Pressure Equation Constant B (Table 7.1-2)	B	0.0	°R	Vapor Space Expansion Factor (Eq. 1-5: $(\Delta T v / TLA) \cdot [(APv - \Delta P B) / (PA - PvA)]$)	KE	0.0517 per day
Tank design data				Average Daily Vapor Temperature Range	ΔTv	29.10 °R
Shell height	Hs	10.60	ft	Average Daily Vapor Pressure Range	ΔPv	0.0000 psi
Diameter	D	7.76	ft	Breather Vent Pressure Setting Range (Equation 1-10: $\Delta P B = P B P - P B V$)	PBP	0.0600 psi
Throughput	Q	800	gal/month	Vapor Pressure at Avg Daily Liq Surface Temp	PvA	0.0984 psia
Turnovers	N	2.51	per year	Average Daily Liquid Surface Temperature	TLA	521.00 °R
Roof Type:				Atmospheric Pressure	PA	14.69 psia
Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft	Average Daily Vapor Temperature Range (ΔTv)		
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA	ft	Average daily ambient temperature range - Equation 1-11 ($\Delta TA = TAX - TAN$)	ΔTA	15.3 °R
Maximum Filling Height - use (Pi/4)D if unknown	HLX	9.60	ft	Not Insulated - Equation 1-7 ($\Delta TV = 0.7 \cdot \Delta TA + 0.02 \cdot \alpha$)	ΔTV	29.10 °R
Minimum Filling Height (use 0 if unknown)	HLN	1.00	ft	Partially Insulated - Equation 1-8 ($\Delta TV = 0.6 \cdot \Delta TA + 0.02 \cdot \alpha R$)	ΔTV	27.57 °R
Liquid height (assume 1/2 H)	HL	5.30	ft	Fully Insulated, constant temperature	ΔTV	0.00 °R
Tank insulation (pick from drop down list)				Average Daily Vapor Pressure Range (ΔPv)		
Tank Construction (pick from drop down list)				Not Insulated - Equation 1-9: $\Delta P V = P V X - P V N$	ΔPv	0.00000 psi
Tank Shell Color (pick from drop down list)				Vapor pressure at ave. daily max liquid surface temp. (Eq. 1-25: $P V X = \alpha P$)	PvX	1.00000 psi
Tank Shell Condition (pick from drop down list)				Vapor pressure at ave daily min liquid surface temp. (Eq. 1-25: $P V N = \alpha P$)	PvN	1.00000 psi
Tank Interior Condition (pick from drop down list)				Average daily max. liquid surface temp.; Fig. 7.1-17: $TLX = TLA + 0.25 \Delta TV$	TLX	528.28 °R
Tank paint solar absorptance, dimensionless; Table 7.1-6	α	0.97		Average daily min. liquid surface temp.; Fig. 7.1-17: $TLN = TLA - 0.25 \Delta TV$	TLN	513.73 °R
Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	0.03	psi	Partially Insulated - Equation 1-9: $\Delta P V = P V X - P V N$	ΔPv	0.00000 psi
True Vapor Pressure; Eq. 1-25, $PvA = \exp(A \cdot (B/TLA))$				Vapor pressure at the average daily max liquid surface temp. (Eq. 1-25: PvX)	PvX	1.00000 psi
Not Insulated	PvA	0.0983581		Vapor pressure at the average daily min liquid surface temp. (Eq. 1-25: PvN)	PvN	1.0000000 psi
Partially Insulated	PvA	0.0993076		Average daily maximum liquid surface temperature, deg R ($TLX = TLA + TLX$)	TLX	528.17 °R
Fully Insulated	PvA	0.0869909		Average daily minimum liquid surface temperature, deg R ($TLN = TLA - TLN$)	TLN	514.39 °R
Average Daily Ambient Temperature (TAA) Eq. 1-30 $TAA = ((TAX + TAN) / 2)$	TAA	514.75	°R	Fully Insulated (ΔPv = 0)	ΔPv	0.00 psi
Average daily maximum ambient temperature; Table 7.1-7	TAX	522.40	°R	Vapor Space Volume (Eq. 1-3: $Vv = (PI / 4) D^2 Hvo$)	Vv	250.49 ft ³
Average daily minimum ambient temperature; Table 7.1-7	TAN	507.10	°R	Effective Tank diameter	De	7.76 ft
Liquid Bulk Temperature; Eq. 1-31: $TB = TAA + 0.003 \alpha s$	TB	517.51	°R	Effective Tank Height	He	10.60 ft
				Vapor Space Outage Hvo = 1/2 H	Hvo	5.30 ft
Average Daily Liquid Surface Temperature (TLA)						
Not Insulated; Eq. 1-28, $TLA = 0.4 \cdot TAA + 0.6 \cdot TB + 0.005 \cdot \alpha \cdot I$	TLA	521.00	°R			
Partially Insulated; Eq. 1-29, $TLA = 0.3 \cdot TAA + 0.7 \cdot TB + 0.005 \cdot \alpha \cdot R$	TLA	521.28	°R			
Fully Insulated; $TLA = TB$	TLA	517.5	°R			
Average Vapor Temperature (Tv)						
Not Insulated; Eq. 1-33, $Tv = 0.7 \cdot TAA + 0.3 \cdot TB + 0.009 \cdot \alpha \cdot I$	Tv	523.85	°R			
Partially Insulated; Eq. 1-34, $Tv = 0.6 \cdot TAA + 0.4 \cdot TB + 0.01 \cdot \alpha \cdot R$	Tv	525.05	°R			
Fully Insulated; $Tv = TB$	Tv	517.51	°R			
Stock Vapor Density; Eq. 1-22, $Wv = (Mv \cdot PvA) / (R \cdot Tv)$						
Not Insulated	Wv	2.275E-03				
Partially Insulated	Wv	2.291E-03				
Fully Insulated	Wv	2.036E-03				

HAPS Speciation	lb/month	Product	Eq. 40-6 $Zvi = yMi / MV$	Vapor Weight Concentration	Vapor Mole Fraction
Total HAP Emissions =	1.157				
Individual HAPS					
hexane	0.0000	86.18	130	0.00000	0.00000
benzene	0.0000	78.11	130	0.00000	0.00000
2,2,4 TMP	0.0000	114.23	130	0.00000	0.00000
toluene	0.0000	92.			

Monthly Calculations (continued)

NOVEMBER

Tank No.	10480	Symbol	Units	ROUTINE EMISSIONS CALCULATIONS	Symbol	Units
ROUTINE EMISSIONS CALCULATIONS						
Total Losses (Eq. 1-1: $LT = LS + LW$)	LT	0.61	lb/month	Standing Losses; Eq. 1-2, $LS = 365 (Vv \cdot Wv \cdot KE \cdot Ka)$	LS	0.44 lb/month
		3.03E-04	ton/month	Vapor Space Volume	Vv	250.5 ft ³
				Stock Vapor Density	Wv	0.0015 lb/ft ³
				Vapor Space Expansion Factor ($0 < KE \leq 1$); Eq. 1-5	KE	0.038 per day
Nearest US Location				Vented Vapor Saturation Factor	Ks	1.00 NA
Daily total solar insolation on a horizontal surface; Table 7.1-7	I	621.0	Btu/ft ² -day	Constant; Number of Daily Events in a Year	365	31 days/month
Absolute Pressure	PA	14.69	psia	Working Losses; Eq. 1-35, $LW = VQ \cdot KN \cdot Kp \cdot Wv \cdot KB$	LW	0.16 lb/month
Ideal Gas Constant	R	10.73	psia ft ³ /lb-mole R	Net Working Loss Throughput (Eq. 1-39: $VQ = 5.614 \cdot Q$)	VQ	107 ft ³ /month
Product Information				Working Loss Turnover Factor Eq. 1-35: $Kp = (180 + N)/6N$ for $N \geq 36$, else $Kp = KN$	KN	1.0000
Product Type				Working Loss Product Factor	Kp	1.00
Vapor Molecular weight	Mv	130	Lb/lb-mole	Stock Vapor Density	Wv	0.0015 lb/ft ³
Average organic liquid density	WL	6.10	lb/gal	Vent Setting Correction Factor	KB	1.00
Average Reid Vapor Pressure	RVP	0.00	psi	Vented Vapor Saturation Factor; Eq. 1-21, $Ks = 1/(1+0.053 \cdot PvA \cdot Hvo)$	Ks	1.00
Product factor; 0.4 for crude oils or 1 for other organic liquids	Kc	1.00		Vapor Pressure at Avg Daily Liq Surface Temp	PvA	0.0650 psia
Vapor Pressure Equation Constant A	A	0.00		Vapor Space Outage	Hvo	0.00 ft
Vapor Pressure Equation Constant B (Table 7.1-2)	B	0.0	"R	Vapor Space Expansion Factor (Eq. 1-5: $(\Delta T v / TLA) \cdot [(APv - \Delta P B) / (PA - PvA)]$)	KE	0.0381 per day
Tank design data				Average Daily Vapor Temperature Range	$\Delta T v$	21.50 "R
Shell height	Hs	10.60	ft	Average Daily Vapor Pressure Range	$\Delta P v$	0.00000 psia
Diameter	D	7.76	ft	Breather Vent Pressure Setting Range (Equation 1-10: $\Delta P B = P B P - P B V$)	PBP	0.0600 psi
Throughput	Q	800	gal/month	Vapor Pressure at Avg Daily Liq Surface Temp	PvA	0.0650 psia
Turnovers	N	2.60	per year	Average Daily Liquid Surface Temperature	TLA	509.45 "R
Roof Type:				Atmospheric Pressure	PA	14.69 psia
Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft			
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA	ft			
Maximum Filling Height - use (Pi/4)D if unknown	HLX	9.60	ft			
Minimum Filling Height (use 0 if unknown)	HLN	1.00	ft			
Liquid height (assume 1/2 H)	HL	5.30	ft			
Tank insulation (pick from drop down list)						
Tank Construction (pick from drop down list)						
Tank Shell Color (pick from drop down list)						
Tank Shell Condition (pick from drop down list)						
Tank Interior Condition (pick from drop down list)						
Tank paint solar absorptance, dimensionless; Table 7.1-6	α	0.97				
Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	0.03	psi			
True Vapor Pressure; Eq. 1-25, $PvA = \exp(A \cdot (B/TLA))$						
Not Insulated	PvA	0.064996	psi			
Partially Insulated	PvA	0.0654304	psi			
Fully Insulated	PvA	0.0597064	psi			
Average Daily Ambient Temperature (TAA) Eq. 1-30 $TAA = ((TAX + 1) \cdot TAA) / (TAX + 1)$	TAA	505.35	"R			
Average daily maximum ambient temperature; Table 7.1-7	TAX	512.10	"R			
Average daily minimum ambient temperature; Table 7.1-7	TAN	498.60	"R			
Liquid Bulk Temperature; Eq. 1-31: $TB = TAA + 0.003 \cdot \alpha \cdot I$	TB	507.16	"R			
Average Daily Liquid Surface Temperature (TLA)						
Not Insulated; Eq. 1-28, $TLA = 0.4 \cdot TAA + 0.6 \cdot TB + 0.005 \cdot \alpha \cdot I$	TLA	509.45	"R			
Partially Insulated; Eq. 1-29, $TLA = 0.3 \cdot TAA + 0.7 \cdot TB + 0.005 \cdot \alpha \cdot I$	TLA	509.63	"R			
Fully Insulated; $TLA = TB$	TLA	507.2	"R			
Average Vapor Temperature (Tv)						
Not Insulated; Eq. 1-33, $Tv = 0.7 \cdot TAA + 0.3 \cdot TB + 0.009 \cdot \alpha \cdot I$	Tv	511.31	"R			
Partially Insulated; Eq. 1-34, $Tv = 0.6 \cdot TAA + 0.4 \cdot TB + 0.01 \cdot \alpha \cdot I$	Tv	512.10	"R			
Fully Insulated; $Tv = TB$	Tv	507.16	"R			
Stock Vapor Density; Eq. 1-22, $Wv = (Mv \cdot PvA) / (R \cdot Tv)$						
Not Insulated	Wv	1.540E-03				
Partially Insulated	Wv	1.548E-03				
Fully Insulated	Wv	1.426E-03				

HAPS Speciation	Product	ib/month	Vapor Weight Concentration	Vapor Mole Fraction
Total HAP Emissions = 0.606				
Eq. 40-6 $Zvi = y_i M_i / M_v$ Eq. 40-5 $y_i = P_i / PVA$				
Individual HAPS				
		L_{Ti} (lb/month)	M_i	M_v
hexane	0.0000	86.18	130	0.00000
benzene	0.0000	78.11	130	0.00000
2,2,4 TMP	0.0000	114.23	130	0.00000
toluene	0.0000	92.14	130	0.00000
ethylbenzene	0.1770	106.17	130	0.29229
xylenes	0.4285	106.17	130	0.70771
naphthalene	0.0000	128.17	130	0.00E+00
cumene	0.0000	120.19	130	0.00E+00

Individual HAPS	Z _i	M _i	M _v	X _i	A	B	C	P _{ij}
hexane	0.00000	130	86.18	0.00000	6.878	1171.5	224.37	1.4562
benzene	0.00000	130	78.11	0.00000	6.906	1211	220.79	0.8757
2,2,4 TMP	0.00000	130	114.23	0.00000	6.812	1257.8	220.74	0.4409
toluene	0.00000	130	92.14	0.00000	7.017	1377.6	222.64	0.2391
ethylbenzene	0.26400	130	106.17	0.32326	6.95	1419.3	212.61	0.0720
xylenes	0.73600	130	106.17	0.90120	7.009	1462.3	215.11	0.0625
naphthalene	0.00000	130	128.17	0.00000	7.146	1831.6	211.82	0.0015
cumene	0.00000	130	120.19	0.00000	6.929	1455.8	207.2	0.0323

Monthly Calculations (continued)

DECEMBER

Tank No.	10480	Symbol	Units	ROUTINE EMISSIONS CALCULATIONS	Symbol	Units
ROUTINE EMISSIONS CALCULATIONS						
Total Losses (Eq. 1-1: $LT = LS + LW$)	LT	0.38	lb/month	Standing Losses; Eq. 1-2, $LS = 365 (Vv \cdot Wv \cdot KE \cdot Ka)$	LS	0.27 lb/month
		1.91E-04	ton/month	Vapor Space Volume	Vv	250.5 ft ³
				Stock Vapor Density	Wv	0.0011 lb/ft ³
				Vapor Space Expansion Factor ($0 < KE \leq 1$); Eq. 1-5	KE	0.033 per day
Nearest US Location				Vented Vapor Saturation Factor	Ks	1.00 NA
Daily total solar insolation on a horizontal surface; Table 7.1-7	I	501.0	Btu/ft ² -day	Constant; Number of Daily Events in a Year	365	31 days/month
Absolute Pressure	PA	14.69	psia	Working Losses; Eq. 1-35, $LW = VQ \cdot KN \cdot Kp \cdot Wv \cdot KB$	LW	0.11 lb/month
Ideal Gas Constant	R	10.73	psia ft ³ /lb-mole R	Net Working Loss Throughput (Eq. 1-39: $VQ = 5.614 \cdot Q$)	VQ	107 ft ³ /month
Product Information				Working Loss Turnover Factor Eq. 1-35: $Kp = (180 + N)/6N$ for $N \geq 36$, else $Kp = KN$	KN	1.0000
Product Type				Working Loss Product Factor	Kp	1.00
Vapor Molecular weight	Mv	130	Lb/lb-mole	Stock Vapor Density	Wv	0.0011 lb/ft ³
Average organic liquid density	WL	6.10	lb/gal	Vent Setting Correction Factor	KB	1.00
Average Reid Vapor Pressure	RVP	0.00	psi	Vented Vapor Saturation Factor; Eq. 1-21, $Ks = 1/(1+0.053 \cdot PvA \cdot Hvo)$	Ks	1.00
Product factor; 0.4 for crude oils or 1 for other organic liquids	Kc	1.00		Vapor Pressure at Avg Daily Liq Surface Temp	PvA	0.0434 psia
Vapor Pressure Equation Constant A	A	0.00		Vapor Space Outage	Hvo	0.00 ft
Vapor Pressure Equation Constant B (Table 7.1-2)	B	0.0	"R	Vapor Space Expansion Factor (Eq. 1-5: $(\Delta T v / TLA) \cdot [(APv - \Delta P B) / (PA - PvA)]$)	KE	0.0331 per day
Tank design data				Average Daily Vapor Temperature Range	$\Delta T v$	18.54 "R
Shell height	Hs	10.60	ft	Average Daily Vapor Pressure Range	$\Delta P v$	0.00000 psia
Diameter	D	7.76	ft	Breather Vent Pressure Setting Range (Equation 1-10: $\Delta P B = P B P - P B V$)	PBP	0.0600 psi
Throughput	Q	800	gal/month	Vapor Pressure at Avg Daily Liq Surface Temp	PvA	0.0434 psia
Turnovers	N	2.51	per year	Average Daily Liquid Surface Temperature	TLA	498.80 "R
Roof Type:				Atmospheric Pressure	PA	14.69 psia
Tank Cone Roof Slope (If unknown, use 0.0625)	SR	0.0625	ft/ft			
Dome Roof Radius (If unknown, use tank diameter (D) or (2Rs))	RR	NA	ft			
Maximum Filling Height - use (Pi/4)D if unknown	HLX	9.60	ft			
Minimum Filling Height (use 0 if unknown)	HLN	1.00	ft			
Liquid height (assume 1/2 H)	HL	5.30	ft			
Tank insulation (pick from drop down list)						
Tank Construction (pick from drop down list)						
Tank Shell Color (pick from drop down list)						
Tank Shell Condition (pick from drop down list)						
Tank Interior Condition (pick from drop down list)						
Tank paint solar absorptance, dimensionless; Table 7.1-6	α	0.97				
Breather Vent Setting Range (Default Assumption: +/- 0.03)	PBP	0.03	psi			
True Vapor Pressure; Eq. 1-25, $PvA = \exp(A \cdot (B/TLA))$						
Not Insulated	PvA	0.0434368	psi			
Partially Insulated	PvA	0.0436837	psi			
Fully Insulated	PvA	0.0404123	psi			
Average Daily Ambient Temperature (TAA) Eq. 1-30 $TAA = ((TAX + 1) \cdot TAA) / (TAX + 1)$	TAA	495.50	"R			
Average daily maximum ambient temperature; Table 7.1-7	TAX	501.80	"R			
Average daily minimum ambient temperature; Table 7.1-7	TAN	489.20	"R			
Liquid Bulk Temperature; Eq. 1-31: $TB = TAA + 0.003 \cdot \alpha \cdot I$	TB	496.96	"R			
Average Daily Liquid Surface Temperature (TLA)						
Not Insulated; Eq. 1-28, $TLA = 0.4 \cdot TAA + 0.6 \cdot TB + 0.005 \cdot \alpha \cdot I$	TLA	498.80	"R			
Partially Insulated; Eq. 1-29, $TLA = 0.3 \cdot TAA + 0.7 \cdot TB + 0.005 \cdot \alpha \cdot I$	TLA	498.95	"R			
Fully Insulated; $TLA = TB$	TLA	497.0	"R			
Average Vapor Temperature (Tv)						
Not Insulated; Eq. 1-33, $Tv = 0.7 \cdot TAA + 0.3 \cdot TB + 0.009 \cdot \alpha \cdot I$	Tv	500.31	"R			
Partially Insulated; Eq. 1-34, $Tv = 0.6 \cdot TAA + 0.4 \cdot TB + 0.01 \cdot \alpha \cdot I$	Tv	500.94	"R			
Fully Insulated; $Tv = TB$	Tv	496.96	"R			
Stock Vapor Density; Eq. 1-22, $Wv = (Mv \cdot PvA) / (R \cdot Tv)$						
Not Insulated	Wv	1.052E-03				
Partially Insulated	Wv	1.056E-03				
Fully Insulated	Wv	9.851E-04				

HAPS Speciation	Product	ib/month	Vapor Weight Concentration	Vapor Mole Fraction
Total HAP Emissions = 0.383				
Eq. 40-6 $Zvi = y_i M_i / M_v$ Eq. 40-5 $y_i = P_i / PVA$				
Individual HAPS				
		L_{Ti} (lb/month)	M_i	M_v
hexane	0.0000	86.18	130	0.00000
benzene	0.0000	78.11	130	0.00000
2,2,4 TMP	0.0000	114.23	130	0.00000
toluene	0.0000	92.14	130	0.00000
ethylbenzene	0.1121	106.17	130	0.29289
xylenes	0.2705	106.17	130	0.70711
naphthalene	0.0000	128.17	130	0.00E+00
cumene	0.0000	120.19	130	0.00E+00

Individual HAPS	Z _i	M _i	M _v	X _i	A	B	C	P _{ij}
hexane	0.00000	130	86.18	0.00000	6.878	1171.5	224.37	1.0808
benzene	0.00000	130	78.11	0.00000	6.906	1211	220.79	0.6372
2,2,4 TMP	0.00000	130	114.23	0.00000	6.812	1257.8	220.74	0.3168
toluene	0.00000	130	92.14	0.00000	7.017	1377.6	222.64	0.1675
ethylbenzene	0.26400	130	106.17	0.32326	6.95	1419.3	212.61	0.0482
xylenes	0.73600	130	106.17	0.90120	7.009	1462.3	215.11	0.0417
naphthalene	0.00000	130	128.17	0.00000	7.146	1831.6	211.82	0.0009
cumene	0.00000	130	120.19	0.00000	6.929	1455.8	207.2	0.0210

Attachment C
Upstream GHG Calculations

Upstream GHG Calculations - Before Project

Propane Source

Product	Unit	Gal/yr (Liquid)	MMBTU/yr*
Propane	Flares	17,575	1,599

* MMBTU/yr based on default high heat values from 40 CFR 98 Subpart C Table C-1.

Pollutant	CH4	N2O	CO2	GHG**
Emission Factor (lb/MMBTU)**	0.27	0.0006	38.13	(CH4*84)+(N2O*264)+(CO2*1)
lb/yr	426.635	0.952	60,980.580	97,069.24
tons/yr	0.213	0.0005	30.490	48.535

** Source is Table A1 in Appendix A. Emission Factors for Use by State Agencies and Applicants, converted from g/MMBTU to lb/MMBTU

Upstream GHG Calculations - After Project

Propane Source

Product	Unit	Gal/yr (Liquid)	MMBTU/yr*
Propane	Flares	500	46

* MMBTU/yr based on default high heat values from 40 CFR 98 Subpart C Table C-1.

Pollutant	CH4	N2O	CO2	GHG**
Emission Factor (lb/MMBTU)**	0.27	0.0006	38.13	(CH4*84)+(N2O*264)+(CO2*1)
lb/yr	12.138	0.027	1,734.867	2,761.57
tons/yr	0.006	0.00001	0.867	1.381

** Source is Table A1 in Appendix A. Emission Factors for Use by State Agencies and Applicants, converted from g/MMBTU to lb/MMBTU